



Engineering Assessment Report

Strategic Housing Development in Kilnahue, Gorey, Co. Wexford

March 2022

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Client Name: Gerard Gannon Properties
Document Reference: 13-119r.012 Engineering Assessment Report
Project Number: 13-119

Quality Assurance . Approval Status

This document has been prepared and checked in accordance with
Waterman Group's IMS (BS EN ISO 9001: 2015 and BS EN ISO 14001: 2015)

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- B. GDSDS Attenuation Calculations
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1. Introduction

1.1 Background of Report

This Engineering Assessment Report has been prepared by Waterman Moylan as part of the documentation in support of a revised planning application for a proposed residential development at a site off Kilnahue Lane, Gorey, Co. Wexford.

An application was previously submitted for planning permission in June 2016 (Planning Reg. Ref. 20160623). This submission received a decision to approve for planning by Wexford County Council on 20 February 2017, but the application was subsequently refused by An Bord Pleanála on 18 July 2017 (Reference PL26.248159). Refer to the accompanying report titled 'Response to Previous Reasons for Refusal' for a summary of the reasons for refusal and a review of how these items have been addressed in the subject application.

This report assesses wastewater and surface water drainage, water supply infrastructure and the road and transportation network in the vicinity of the site, and details the criteria used to design the proposed wastewater and surface water drainage, water supply and transport networks.

1.2 Site Location and Description

The subject site is located at the west of Gorey, Co. Wexford, with access to the site at the north from Gorey Hill/Kilnahue Lane and at the south-west from Carnew Road (R725). The site is bounded by agricultural lands to the west, by Carnew Road (R725), residential properties and agricultural lands to the south and east, and by Gorey Hill / Kilnahue Lane to the north. The site location is indicated in the Figure below:

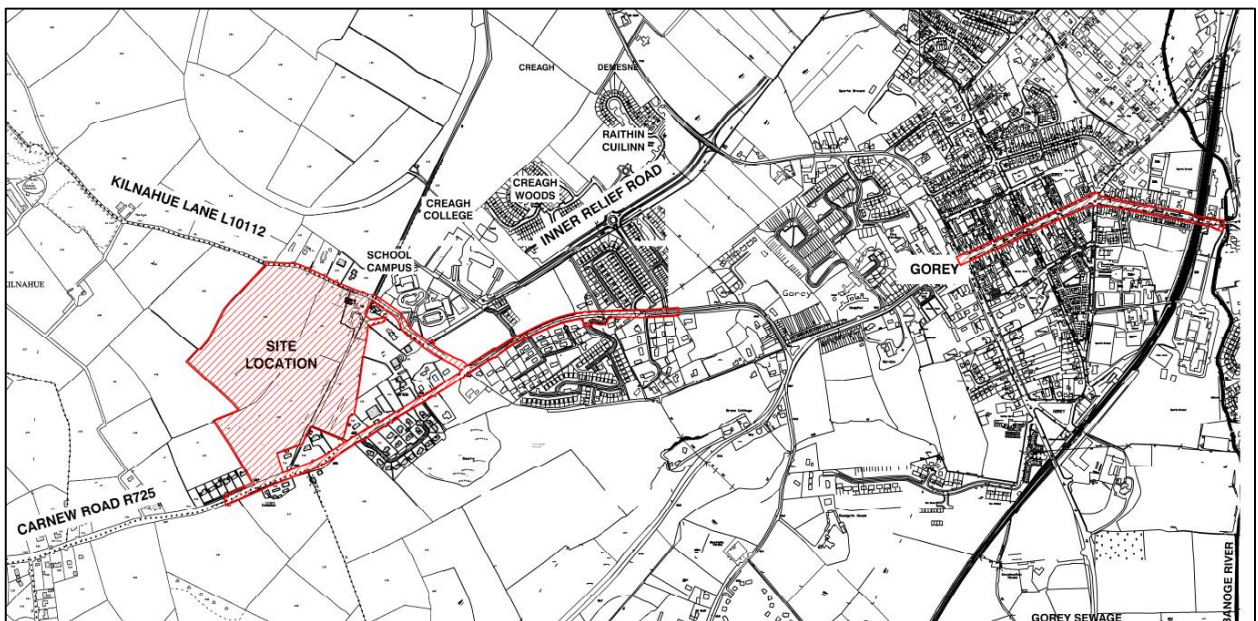


Figure 1 | Site Location (Image Source: Google Maps)

The subject site is a greenfield site, currently used for agricultural purposes. Topographic survey data shows that the site falls generally from west to the east, from a high point of approximately 133.5m OD Malin at the west of the site to a low point of approximately 101.5m OD Malin at the east. There is a surface water ditch at approximately 97.50m OD Malin to the east of the site which drains the site to the Banogue River.

1.3 Gorey Town and Environs Local Area Plan 2017-2023

The proposed development falls within the Gorey Town and Environs Local Area Plan 2017-2023. The majority of the site is zoned for new urban blocks, with a portion of the site at the west zoned as a neighbourhood park. One of the reasons for refusal of the previous planning application was inadequate provision of open amenity space in accordance with the Local Area Plan.

The proposed site layout has been revised significantly since the previous application, and now includes a large public open space at the north-west of the site, to serve as a neighbourhood park in accordance with the Environs Local Area Plan 2017-2023.

The Figure below shows an extract of the Place Concept for Gorey, taken from the Gorey Town and Environs Local Area Plan 2017-2023, with the proposed development inset. As can be seen, the proposed road alignments now closely follow the Local Area Plan, with a large neighbourhood park proposed in the same location as set out in the LAP.

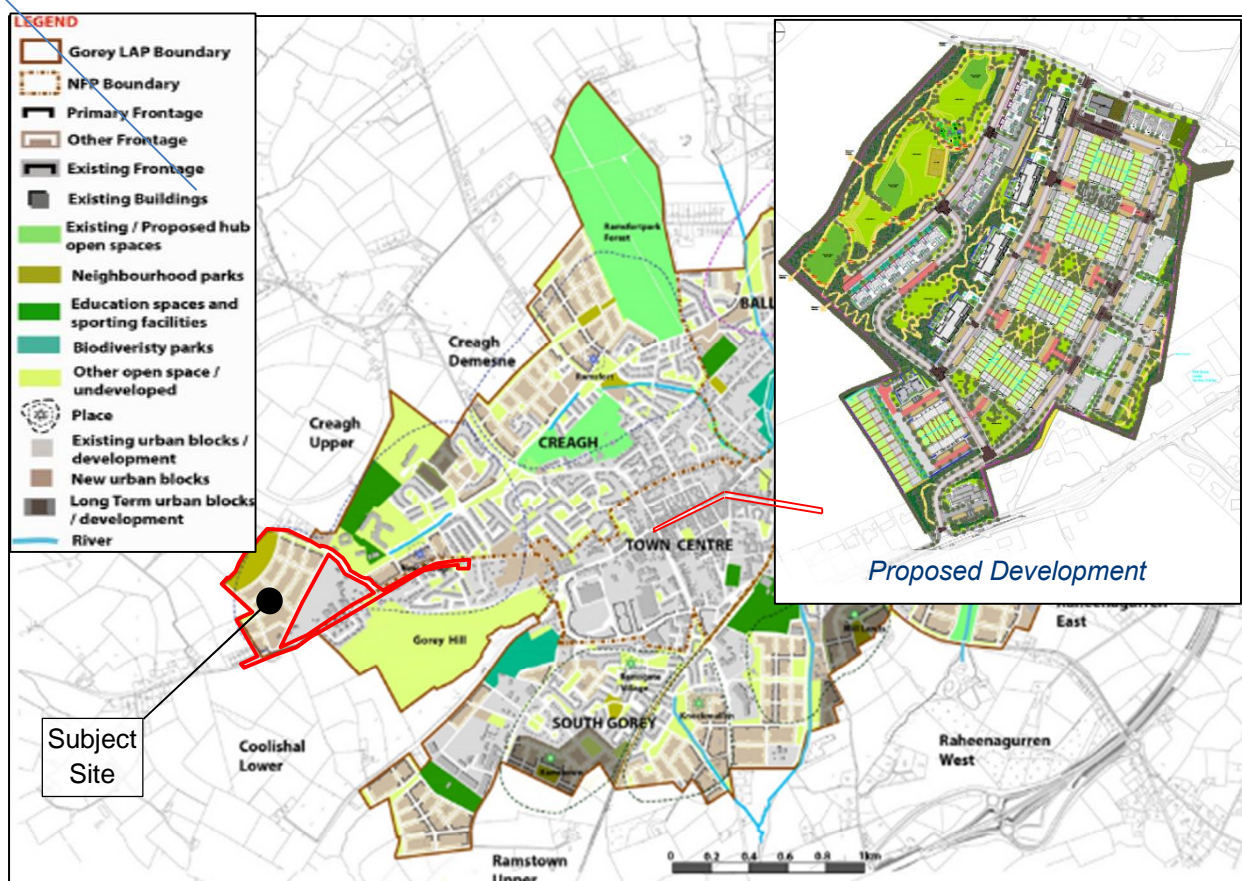


Figure 2 | Place Concept for Gorey, Extracted from Gorey Town and Environs LAP 2017-2023, with Proposed Development Inset

1.4 Proposed Development

The proposed development consists of a total of 421 residential units, comprising of 133 houses, 228 apartment units and 60 duplex units, a crèche, two retail units and community rooms. The schedule of accommodation is set out in the Table below:

Description	1-Bed	2-Bed	3-Bed	4-Bed	Total
Houses	-	-	115	18	133
Apartments	76	145	7	-	228
Duplexes	4	26	30	-	60
Crèche	565m ²				-
Retail	210m ²				-
Total	80	171	152	18	421

Table 1 | Schedule of Accommodation

1.5 Previous Refusal

As noted above, an application was previously submitted for planning permission at the subject site in June 2016 (Planning Reg. Ref. 20160623). That submission received a decision to approve for planning by Wexford County Council on 20 February 2017, but the application was subsequently refused by An Bord Pleanála on 18 July 2017 (Reference PL26.248159).

The proposed development has been designed to specifically address the deficiencies identified in An Bord Pleanála's refusal. The reasons for refusal included inadequate provision of open amenity space in accordance with the Local Area Plan, insufficient residential density and uncertainty regarding road and junction upgrade works at the adjacent Kilnahue Lane and Carnew Road.

Refer to the accompanying report titled "Response to Previous Reasons for Refusal" for a summary of the reasons for refusal and a review of how these items have been addressed in the subject application.

2. Foul Water Network

2.1 Existing Foul Water Network

Irish Water records for the surrounding area have been consulted as part of this assessment and are extracted below:

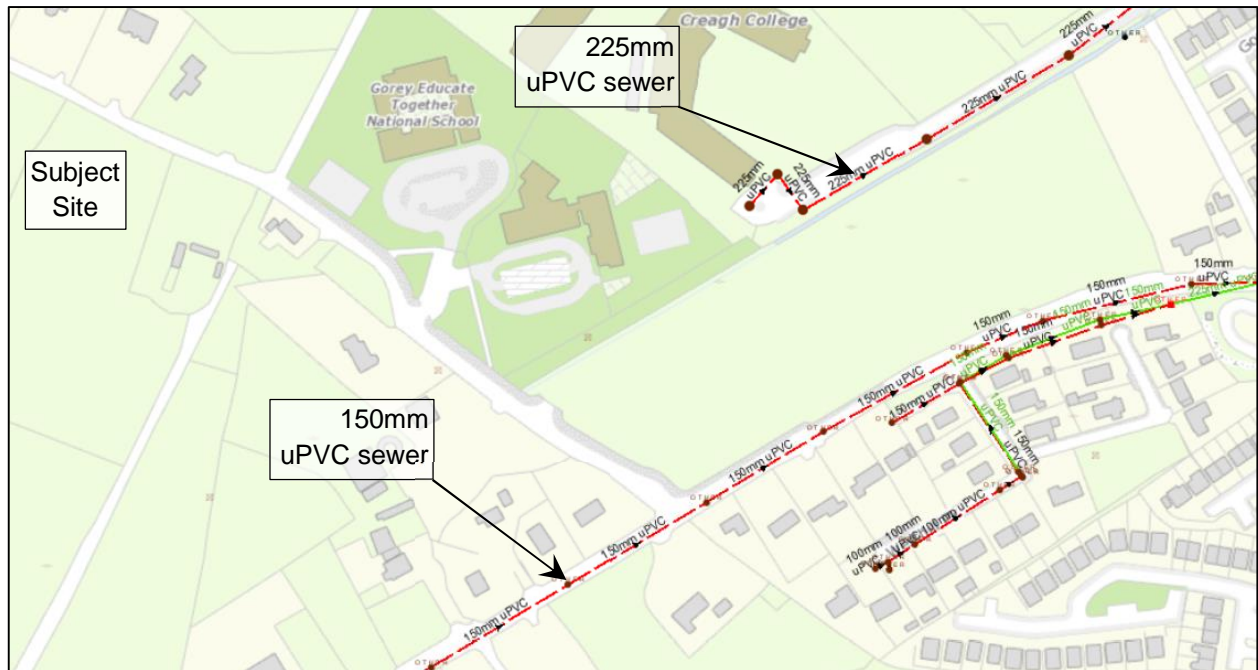


Figure 3 | Extract of Irish Water's Wastewater Drainage Records

There is an existing 150mm diameter public foul water sewer in Carnew Road, south-east of the site. This sewer increases in diameter to 225mm approximately 800m east of the site entrance, at Westhill Park.

There is a 225mm diameter foul sewer draining eastwards from Creagh College. There is a new 2m wide pedestrian access along the southern boundary of Gaelscoil Moshíológ, providing a pedestrian connection between Kilnahue Lane, approximately 120m north of the junction with Carnew Road, and the Creagh College roundabout. A new 150mm diameter sewer has been laid along this pedestrian link, connecting to the 225mm Creagh College sewer.

2.2 Proposed Foul Water Network

The majority of the site will drain foul water in a north-easterly direction, via a series of 150mm and 225mm sewers, towards Gorey Hill/Kilnahue Lane. From there, a new wastewater sewer will be laid discharging in a south-easterly direction towards Carnew Road and continuing in a north-easterly direction along Carnew Road, discharging via a new connection to the existing portion of 225mm sewer at Ardmore Water Boosting Station. Please refer to the accompanying drainage drawings 13-119-P4200 to P4205 for the drainage layout and details.

The entrance apartment building at the south of the site will discharge directly to the existing 150mm foul water sewer in Carnew Road. This apartment building is proposed to include 10 no. residential units.

The sewer in Carnew Road continues through to the Main Street of Gorey, and onto Esmonde Street, ultimately discharging to the Courtown Wastewater Treatment Plant. Irish Water have confirmed that the Courtown Wastewater Treatment Plant has capacity to cater for the proposed development.

A pre-connection enquiry for the development was submitted to Irish Water in February 2021 and a Confirmation of Feasibility Letter was issued by Irish Water in August 2021 – refer to Appendix A for a copy of this letter. This letter notes that to facilitate the proposed development, off-site foul sewer upgrades are required on Main Street and Esmonde Street in Gorey town. The required upgrades involve upgrading approximately 550m of 225mm diameter sewer to 375mm diameter.

The upgrades required by Irish Water, based on their 2018 model assessment issued to Waterman Moylan, are indicated in the Figure below:

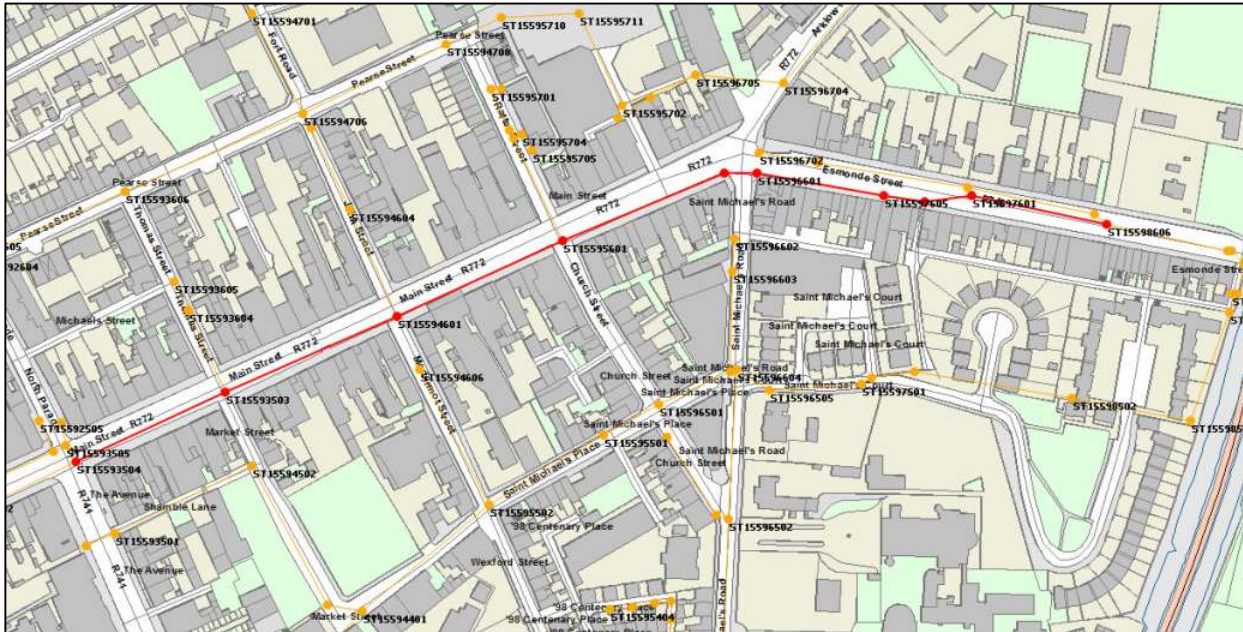


Figure 4 | Foul Sewer Upgrade on Main Street / Esmonde Street as Required by Irish Water

A Statement of Design Acceptance has also been received from Irish Water for the proposed development and is also included in Appendix A.

2.3 Foul Water Drainage Calculations

The calculated foul water flows at the subject development are set out in the Table below. Domestic wastewater loads have been calculated based on 2.7 persons per unit with a per capita wastewater flow of 150 litres per head per day along with a 10% unit consumption allowance, in line with Section 3.6 of the Irish Water Code of Practice for Wastewater Infrastructure. Note that the Irish Water Code of Practice assumes 2.7 residents per unit regardless of the unit type.

Per capita wastewater flows for the commercial area (the crèche/childcare facility and retail units) have been based on the flow rates set out in Appendix C of the Code of Practice, and a peak flow multiplier of 6 has been used, as per Section 2.2.5 of Appendix B of the Code of Practice.

Description	Total Population	Load per Capita	Daily Load	Total DWF	Peak Flow
	No. People	l/hd/day	l/day	l/s	l/s
133 Houses	359 Residents	150	53,850	0.623	3.740
228 Apartments	616 Residents	150	92,400	1.069	6.417
60 Duplexes	162 Residents	150	24,300	0.281	1.688
Crèche	89 Children	50	4,450	0.052	0.309
	11 Staff	45	1,170	0.014	0.081
Retail & Community	25 Customers	50	1,250	0.014	0.087
	8 Staff	45	360	0.004	0.025
Total	-	-	177,780	2.058	12.346

Table 2 | Calculation of Total Foul Water Flow from the Development

The total dry weather flow from the development is 2.058 l/s, with a peak flow of 12.346 l/s.

2.4 Foul Water Drainage – General

Foul water sewers will be constructed strictly in accordance with Irish Water requirements. No private drainage will be located within public areas.

Drains will be laid to comply with the requirements of the latest Building Regulations, and in accordance with the recommendations contained in the Technical Guidance Document H.

3. Surface Water Network

3.1 Existing Surface Water Network

The proposed development site is a greenfield site. Topographic survey data shows that the site falls generally from west to the east, from a high point of approximately 133.5m at the west of the site to a low point of approximately 101.5m at the east.

There is a surface water ditch at the eastern boundary of the site, at approximately 97.50m OD Malin. This ditch drains in a northerly direction, discharging to the Banogue River.

3.2 Proposed Surface Water Network

It is proposed to drain surface water through the site via a series of sewers, ranging in size from 225mm diameter to 450mm diameter. For storm water management purposes, the site has been divided into eight sub-catchments. Seven of these will be attenuated separately but will ultimately combine to outfall to the stream at Kilnahue Lane, north-east of the site. The eighth catchment, at the south of the site, will be attenuated separately and will have a separate outfall to the existing ditch on Carnew Road. The proposed sub-catchments are shown in the Figure below:

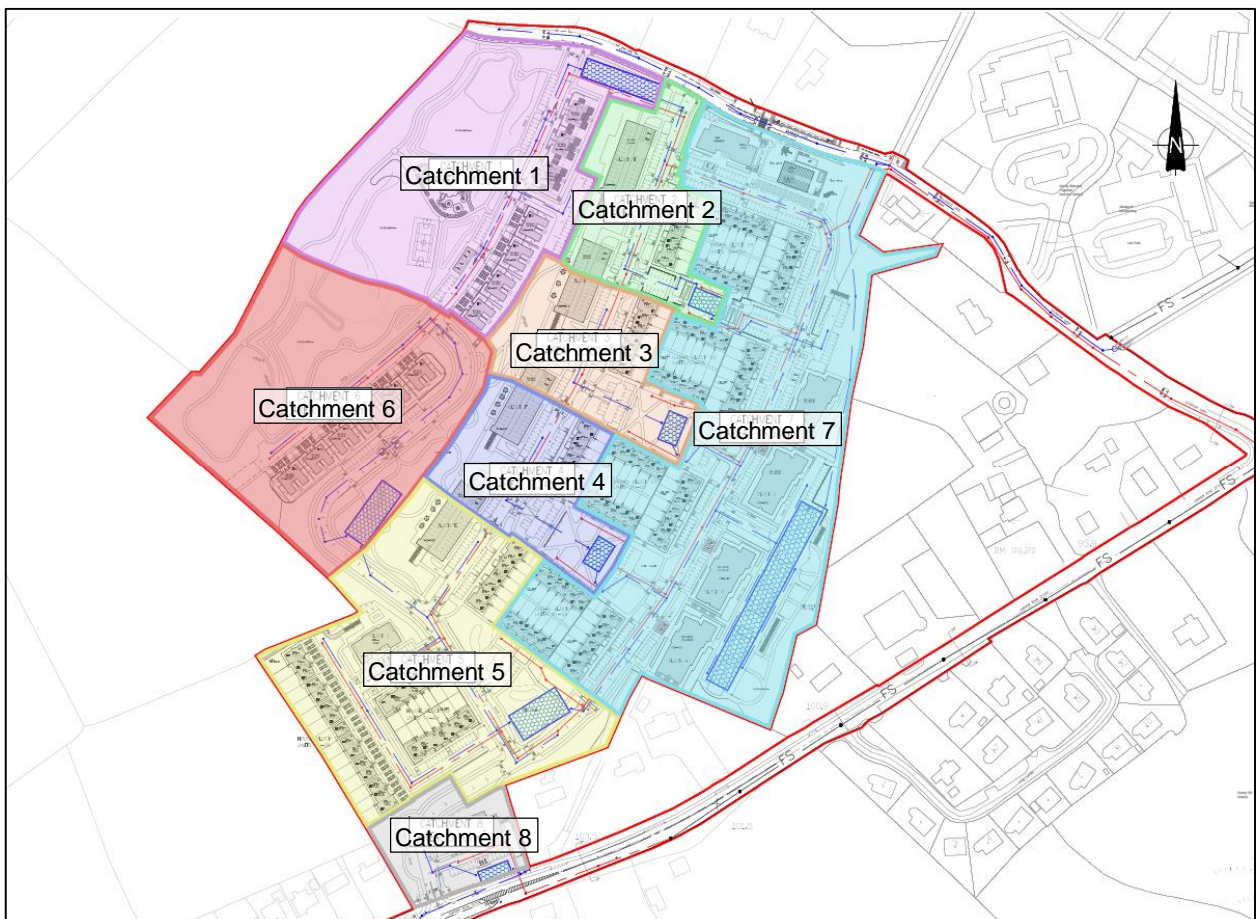


Figure 5 | Proposed Surface Water Drainage Catchments

Catchments 1 to 6 will each drain to below ground attenuation with a permeable base to allow for infiltration/soakaway. Each of these attenuation areas will discharge via a Hydrobrake or similar approved flow control device, joining a network which flows to the Catchment 7 attenuation tank. From here, surface

water will discharge at a controlled rate to Kilnahue Lane, continuing east down Kilnahue Lane before outfalling to the stream via a new headwall.

It is proposed to restrict the discharge rate to 75% of the greenfield equivalent rate (as calculated in Section 3.4 below), in order to alleviate downstream capacity constraints. The attenuation storage provided on site for each catchment has been upsized accordingly. The attenuation provided is sufficient to accommodate the 1-in-100 year storm, accounting for a 20% increase due to climate change and accounting for a discharge rate restricted to 75% of the greenfield equivalent rate.

During Site Investigations, a full 1,000l water bowser was added to trial pits following excavations. At the north-western portions of the site, the water did not remain in the pits sufficiently long enough to measure the infiltration rates. Although the attenuation areas have been designed to permit infiltration, it has nonetheless been conservatively assumed that all surface water will discharge to the drainage network rather than infiltrating the soil.

3.3 Proposed SuDS Strategy

The proposed development has been designed to incorporate best drainage practice. Section 3.4, below, sets out the methodology used in determining the existing greenfield runoff rates and calculating attenuation storage requirements for each catchment. The relevant calculations are included in full in Appendix B.

It is proposed to incorporate a Storm Water Management Plan through the use of various SuDS techniques to treat and minimise surface water runoff from the site. The methodology involved in developing a Storm Water Management Plan for the subject site is based on recommendations set out in the Greater Dublin Strategic Drainage Study (GDSDS) and in the SuDS Manual (Ciria C753). Based on three key elements . Water Quantity, Water Quality and Amenity . the targets of the SuDS train concept have been implemented in the design, providing SuDS devices for each of the following:

- Source Control
- Site Control
- Regional Control

3.3.1 Source Control

Permeable Paving:

It is proposed to introduce permeable paving in private parking spaces and courtyard areas throughout the development. Downpipes from the roofs of the blocks will drain to filter drains beneath the permeable paving to facilitate maximum infiltration of surface water from paved and roof areas. The goal of permeable paving is to control stormwater at the source to reduce runoff. In addition to reducing surface runoff, permeable paving has the dual benefit of improving water quality by trapping suspended solids and filtering pollutants in the substrata layers.

Green Roof:

It is proposed to introduce green roofing as a source control device. Each block will have green roofing introduced on at least 60% of the roof area.

The substrate and the plant layers in a green roof absorb large amounts of rainwater and release it back into the atmosphere by transpiration and evaporation. They also filter water as it passes through the layers, so the run-off, when it is produced, has fewer pollutants. Rainfall not retained by green roofs is detained, effectively increasing the time to peak and slowing peak flows.

A green roof can reduce annual percentage runoff by between 40% and 80% through this retention and evapotranspiration, with the impact dependent on a range of factors including the depth of substrate, the

saturation of substrate at the onset of a rain event, the angle of the roof, the range of vegetation growing, intensity of rainfall and the time of year.

Planted Areas:

It is proposed to provide open grassed areas with low level planting in various open spaces throughout the site. These will act as soft scape and will significantly slow down and reduce the amount of surface water runoff from the open spaces. Planter boxes and planted areas will also take surface water runoff from the downpipes from apartment buildings before draining to the surface water sewer network.

3.3.2 Site Control

Bioretention Tree Pits:

The proposed development includes significant tree planting throughout the development, with bioretention tree pits included at strategic locations through the site. Trees can help control storm water runoff because their leaves, stems, and roots slow rain from reaching the ground and capture and store rainfall to be released later. Trees help to attenuate flows, trap silts and pollutants, promote infiltration and prevent erosion. Incorporating tree planting offers multiple benefits, including attractive planting features, improved air quality and increased biodiversity whilst helping to ensure adaptation to climate change.

3.3.3 Regional Control

Attenuation Tanks/Soakaways:

It is proposed to provide below ground attenuation for each catchment in the form of pluvial cubes with a permeable membrane at the bottom to allow for infiltration into the ground. This will help control and treat storm water runoff by trapping silts and pollutants and promoting infiltration, while still providing sufficient attenuation storage for extreme storm events.

Regional Flow Control:

A new hydrobrake or similar approved flow control device will be provided at the outfall from each catchment to regulate the discharge rate, limiting flows to 75% of the greenfield equivalent runoff rate.

Downstream Defender:

A downstream defender (trade name for a large chamber that retains solids and hydrocarbons) is intended at the combined outfall from Catchments 1 to 7. This will treat the flows that are to be stored in the attenuation tank before discharging to the public above-ground network.

3.4 Interception or Treatment Storage and Attenuation Storage

As noted above, the methodology involved in developing the Storm Water Management Plan for the subject site is based on recommendations set out in the Greater Dublin Strategic Drainage Study (GSDSDS) and in the SuDS Manual. Appendix E of the Greater Dublin Strategic Drainage Study (GSDSDS) sets out criteria for determining the provision of interception or treatment storage, attenuation storage and long term storage at a development site. These calculations are included in full in Appendix B and are summarised below:

3.4.1 Criterion 1: River Water Quality Protection

Criterion 1.1: Interception

The Greater Dublin Strategic Drainage Study (GSDSDS) states that approximately 30% to 40% of rainfall events are sufficiently small that there is no measurable runoff from greenfield areas into the receiving

waters. These events are generally considered as the first 5mm of rainfall. Assuming 80% runoff from paved surfaces and 0% from pervious surfaces for the first 5mm of rainfall yields the following:

Paved surfaces connected to drainage system	$148625m^2 \times 0.5 \times 0.75 =$ $55,734.38m^2$	<i>148,625m² site area</i> <i>50% of the site is paved</i> <i>75% of the paved area</i>
Volume of Interception Storage	$55734.375m^2 \times 5mm \times 0.8 =$ 222.94m³	<i>Paved area directly drained</i> <i>5mm rainfall depth</i> <i>80% paved runoff factor</i>

Table 3 | Interception Storage

The required interception volume is 222.94m³.

Criterion 1.2: Treatment Volume

For events larger than 5mm, and in situations where interception storage cannot be provided, surface water runoff treatment is provided in accordance with the CIRIA design manual C521.

Assuming 80% runoff from paved surfaces and 0% from pervious surfaces for the first 15mm of rainfall:

Paved surfaces draining to river	$148625m^2 \times 0.5 \times 0.75 =$ $55,734.38m^2$	<i>148,625m² site area</i> <i>50% of the site is paved</i> <i>75% of the paved area</i>
Volume of Treatment Storage	$55734.375m^2 \times 15mm \times 0.8 =$ 668.81m³	<i>Paved area directly drained</i> <i>15mm rainfall depth</i> <i>80% runoff from paved surfaces</i>

Table 4 | Treatment Volume

The required treatment storage volume is 668.81m³. The required interception and treatment volumes are provided through the use of SuDS devices as described in Section 3.3 above.

3.4.2 Criterion 2: River Regime Protection

Attenuation storage is provided to limit the discharge rate from the site into receiving waters. As per the GSDSDS, the required attenuation volume is calculated assuming 100% runoff from paved areas, and has been calculated for the 1-year, 30-year and 100-year return periods, identifying the critical storm for each . refer to the calculations included in Appendix B.

The discharge rate has been limited to 75% of the greenfield equivalent runoff rate, to alleviate existing capacity constraints in the stream downstream of the subject site. This results in an increased storage volume requirement. Catchments 1 to 7 all outfall together to the existing stream, and as such have been considered together in the design and in the attenuation calculations. The greenfield equivalent runoff rate for these catchments is 120l/s, and the proposed flow restrictions will limit the outfall to 75% of this rate at 90l/s.

The attenuation volume requirement for this area, as calculated in Appendix B, is 6,794m³. As noted above, this portion of the site has been divided into 7 catchments, each of which will be attenuated separately, with the attenuation volume and the discharge rate proportional to the area of the catchment.

The proposed attenuation volumes and discharge rates for Catchments 1 to 7 are tabulated below:

Description	Attenuation			Catchment Area	Discharge Rate
	Area	Depth	Volume		
Catchment 1	591m ²	2.0m	1,181m ³	24,384m ²	14.8l/s
Catchment 2	221m ²	2.0m	442m ³	9,120m ²	5.5l/s
Catchment 3	227m ²	2.0m	454m ³	9,380m ²	5.7l/s
Catchment 4	224m ²	2.0m	448m ³	9,245m ²	5.6l/s
Catchment 5	612m ²	2.0m	1,224m ³	25,256m ²	15.3l/s
Catchment 6	598m ²	2.0m	1,197m ³	24,700m ²	15.0l/s
Catchment 7	1,879m ²	1.2m	2,255m ³	46,540m ²	28.2l/s
Total	4,352m²	1.655m	7,200m³	148,625m²	90.0l/s

Table 5 | Attenuation Volumes for Catchments 1-7

It is proposed to provide 7,200m³ of attenuation, which exceeds the required 6,794m³.

The required storage volume for Catchment 8, as calculated in Appendix B, is 280m³. It is proposed to provide a 280m³ tank at the south of the site to accommodate this volume.

3.4.3 Criterion 3: Levels of Service

There are four criteria for levels of service. These are:

- Criterion 3.1: No external flooding except where specifically planned (30-year high intensity rainfall event).
- Criterion 3.2: No internal flooding (100-year high intensity rainfall event).
- Criterion 3.3: No internal flooding (100-year river event and critical duration for site storage).
- Criterion 3.4: No flood routing off site except where specifically planned (100-year high intensity rainfall event).

Both internal and external flooding have been assessed in the Flood Risk Assessment report which accompanies this Engineering Assessment report. The Flood Risk Assessment has been carried out in accordance with the *DEHLG/OPW Guidelines on the Planning Process and Flood Risk Management* published in November 2009.

The assessment identifies the risk of both internal and external flooding at the site from various sources and sets out mitigation measures against the potential risks of flooding. The sources of possible flooding assessed in the report include coastal, fluvial, pluvial (direct heavy rain), groundwater and human/mechanical errors.

As a result of the flood risk management and mitigation measures proposed, the residual risk of internal or external flooding for the 30-year and 100-year flood events is low, and accordingly all four of the above criteria have been met. Please refer to the accompanying Flood Risk Assessment report for the full analysis of the flood risk at the subject site.

3.4.4 Criterion 4: River Flood Protection

The long term storage volume is a comparison of pre- and post-development runoff volumes. The objective is to limit the runoff discharged after development to the same as that which occurred prior to development.

Of the three methods described in the GSDSDS for establishing River Flood Protection by comparison of the pre- and post-development runoff volumes, (Criteria 4.1, 4.2 and 4.3 respectively), Criteria 4.3 is selected for use as the most practical criteria at this stage in the design.

The Criteria 4.3 approach is for all runoff to be limited to either Q_{BAR} or to 2 l/s/Ha, whichever is the greater. The proposed drainage system includes a flow control device to ensure that the discharge rate is limited to the greenfield equivalent and ample attenuation is provided for the 1-in-100 year storm, accounting for a 20% increase due to climate change.

The extra runoff volume of the development runoff over greenfield runoff, Vol_{XS} , as calculated in Appendix B is 1,037m³ for Catchments 1-7 and 95.36m³ for Catchment 8. Note that as stated in the GSDSDS, this volume is not additional to the attenuation storage volume but is effectively an element of it.

3.5 Water Environment Potential Impact Appraisal

A Water Environment Potential Impact Appraisal has been carried out by Hydro-G to assess the potential impact of the proposed development on the local Hydrology & Hydrogeology, and the full report by Hydro-G accompanies this submission under separate cover.

The assessment notes that agriculture is the main pressure in all catchments across Ireland. Therefore, any land taken out of agricultural use will aid efforts to improve water quality and the aims of the Water Framework Directive.

The assessment concludes that the proposal presents potential for improvement in the catchment as compared to the current scenario, noting that the SuDS proposals for the development are extensive and provide in excess of the attenuation capacity required, which is deemed to adequately provide protection for the receiving waters.

3.6 Surface Water – General

Surface water sewers will generally consist of PVC (to IS 123) or concrete socket and spigot pipes (to IS 6) and laid strictly in accordance with Wexford County Council requirements for taking in charge. It is intended that all sewers within the public domain will be handed over to the relevant Local Authority for taking in charge.

All private outfall manholes will be built in accordance with the Greater Dublin Regional Code of Practice for Drainage Works. No private drainage will be located within public areas.

Drains will be laid in accordance with the requirements of the Building Regulations, Technical Guidance Document H.

3.7 Flood Risk Assessment

A site-specific Flood Risk Assessment has been carried out for the proposed development and accompanies this submission under separate cover. The Flood Risk Assessment analyses the subject lands for risks from tidal flooding, fluvial flooding, pluvial flooding, ground water and failures of mechanical systems. Where risks were identified, mitigation measures have been proposed. As a result of the proposed mitigation measures, the residual risk of flooding from any source is low.

4. Water Supply Network

4.1 Existing Water Supply Network

Irish Water records for the surrounding area have been reviewed as part of this assessment, and are extracted below:

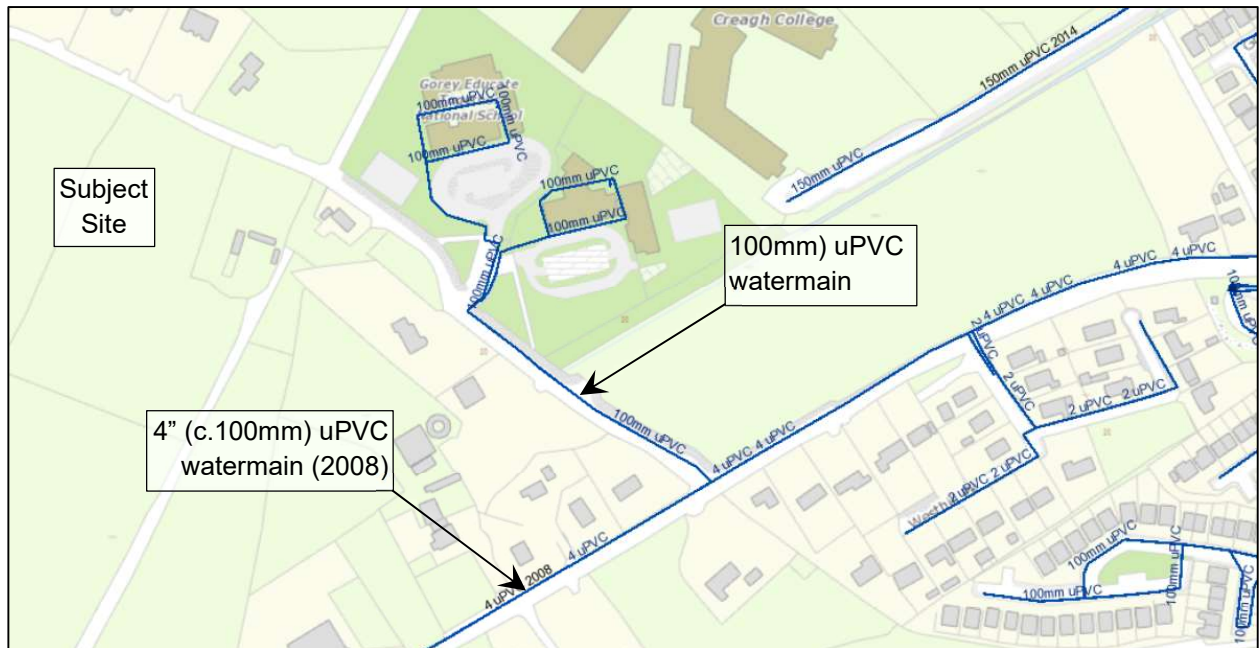


Figure 6 | Extract of Irish Water's Water Supply Service Records

There is an existing 100mm watermain in Gorey Hill/Kilnahue Lane, serving the school on the northern side of the road, and there is a 4" (c.100mm) watermain in Carnew Road.

4.2 Proposed Water Supply Network

It is proposed to provide two new connections to the existing public network, one to the existing watermain in Carnew Road and the other to the existing watermain in Gorey Hill/Kilnahue Lane.

A pre-connection enquiry for the development was submitted to Irish Water in February 2021, with a Confirmation of Feasibility Letter issued at the end of August 2021 and included in Appendix A. The letter stipulates that some watermain upgrades are required to facilitate the development.

As such, some off-site watermain upgrades are proposed in accordance with the requirements set out by Irish Water in the Confirmation of Feasibility Letter. These upgrades involve laying a new 150mm main from the Kilnahue Lane access to Ardmore water pumping station on Carnew Road, continuing as far as the 200mm main crossing just east of the pumping station. Additionally, a new booster station is to be included in the development site. Please refer to the accompanying engineering drawings.

A Statement of Design Acceptance has also been received from Irish Water for the proposed development and is also included in Appendix A.

4.3 Water Supply Calculations

The calculated water demand at the subject development is set out in the below table. The average domestic demand has been established based on an average occupancy ratio of 2.7 persons per dwelling

with a daily domestic per capita consumption of 150 litres per head per day and with a 10% allowance factor. Note that the Irish Water Code of Practice assumes 2.7 residents per unit regardless of the unit type.

The average day/peak week demand has been taken as 1.25 times the average daily domestic demand, while the peak demand has been taken as 5 times the average day/peak week demand, as per Section 3.7.2 of the Irish Water Code of Practice for Water Infrastructure.

Description	Total Population	Demand per Capita	Water Demand	Average Demand	Average Peak Demand	Peak Demand
	No. People	l/hd/day	l/day	l/s	l/s	l/s
133 Houses	359 Residents	150	53,850	0.623	0.779	3.740
228 Apartments	616 Residents	150	92,400	1.069	1.337	6.417
60 Duplexes	162 Residents	150	24,300	0.281	0.352	1.688
Crèche	89 Children	50	4,450	0.052	0.064	0.309
	11 Staff	45	1,170	0.014	0.017	0.081
Retail	25 Customers	50	1,250	0.014	0.018	0.087
	8 Staff	45	360	0.004	0.005	0.025
Total	-	-	177,780	2.058	2.572	12.346

Table 6 | Calculation of Water Demand for the Development

The average demand for the development is 2.058 l/s, with a peak demand of 12.346 l/s.

4.4 Water Supply – General

All watermains will be laid strictly in accordance with Irish Water requirements for taking in charge.

Valves, hydrants, scour and sluice valves and bulk water meters will be provided in accordance with the requirements of Irish Water.

5. Road and Transport Network

This section provides an overview of the existing and proposed road and transportation network in the vicinity of the site. A comprehensive Traffic and Transport Assessment and a Travel Plan have also been prepared by Waterman Moylan and accompanies this planning application under separate cover

5.1 Existing Transport Network

5.1.1 Existing Road Infrastructure

The subject site is bounded by two roads, Carnew Road (R725) to the south and Gorey Hill/Kilnahue Lane to the north. There is vehicular access to the site from both of these roads.

Carnew Road is the name of this stretch of the R725 Regional Road. The R725 is approximately 53km in length and runs in an east-west direction from Gorey through Carnew and Shillelagh to Carlow. The speed limit along the R725 adjacent to the proposed site access is 60km/hr, increasing to 80km/hr west of the site and reducing to 50km/hr east of the junction with Gorey Hill/Kilnahue Lane. To the west of the junction with Gorey Hill/Kilnahue Road, the R725 carriageway is 6m wide. To the east of the junction, the R725 is also a 6m carriageway and includes a cycle lane, layby parking and a footpath along the northern side. The layby parking and the cycle path end after 80m, while the footpath continues.

Gorey Hill is a single carriageway road running north-south at the east and north of the subject site from its junction with R725. The eastern portion of the road is known as Gorey Hill, while the portion of the road west of the site is known as Kilnahue Lane. It is generally 6m wide and provides local access to a small number of houses, to two primary schools and to a motor service commercial unit.

The existing primary junctions in the area surrounding the proposed development site are:

- R725 Carnew Road / Kilnahue Lane: an existing priority-controlled T-junction
- Kilnahue Lane / Access Road to School Site: an existing priority-controlled T-junction

5.1.2 Existing Pedestrian & Cycle Infrastructure

The R725 includes a footpath on the northern side of the carriageway to the west of the junction with Gorey Hill/Kilnahue Road, continuing for approximately 240m up to the petrol service station.

To the east of the junction, the R725 includes a cycle lane, layby parking and a footpath along the northern side of the carriageway. The layby parking and the cycle path end after 80m, while the footpath continues.

Gorey Hill/Kilnahue Lane includes a two-way cycle path (5m wide) and a footpath on the north-eastern side of the carriageway, extending for 300m from the junction with Carnew Road (R725). These pedestrian and cycle facilities currently facilitate access to the school site. A pedestrian crossing is provided on Gorey Hill/Kilnahue Lane approaching the intersection with R725.

5.1.3 Existing Public Transport Network

Gorey town is served by several public bus routes. The closest bus stops to the subject site are located in Gorey town centre, approximately 1.60km to 2.25km to the east (18 to 26-minute walk). The routes serving these bus stops are outlined below:

- Route 2 (Expressway): Dublin Airport. Wexford Station
Towards Wexford, this route operates at a frequency of 1 to 2 hours during the whole day, with the first bus departing from Gorey at 01:50 and the last at 23:46. In the opposite direction, to Dublin

Airport, this route also operates at a 1- to 2-hour frequency during the whole day, with the first bus departing from Gorey at 02:45 and the last at 21:20.

- Route 133X (Bus Éireann): Gorey (Main Street). Busáras
This route operates one service from Gorey to Busáras in Dublin City. The bus leaves Gorey at 06:50 and arrives in Busáras at 08:15. No service is provided in the opposite direction.
- Route 379 (Bus Éireann): Rosslare Harbour. Ballycanew. Wexford Station
This route operates only one service on Mondays and one service on Saturdays. On Mondays, the bus arrives in Gorey at 14:45 and leaves the town at 15:30. On Saturdays, the bus arrives in Gorey at 09:40 and leaves the town at 12:05 towards Wexford.
- Route 740 (Wexford Bus): Redmond Square. Dublin Airport
From Monday to Friday (excluding bank holidays), this route operates at a frequency between 30 minutes to two hours during the whole day. First bus leaves Gorey at 02:25 in the morning and the last at 20:20. In the opposite direction, this route operates at a 20 minute to 1.5 hour frequency during the whole day, with the first bus leaving Gorey at 07:10 and the last at 00:35.
- Route 740A (Wexford Bus): Gorey. Dublin Airport
On weekdays, this route operates 9 services throughout the day. The frequency is generally hourly with the first bus leaving Gorey at 06:00 and the last at 17:40. On weekends, the service reduces to 6 no., with the first at 07:10 and the last at 17:40.
- NUM11 (Wexford Bus): Gorey (Main Street). Whitmore Jewe. Maynooth University
This route only operates on weekdays, with the only bus leaving Gorey at 07:00 towards Maynooth, and the only return service arriving in Gorey at 19:00 from Monday to Thursday and at 18:55 on Fridays.
- Route X2 (Expressway): Wexford Station. Dublin Airport
Only one service per direction is operated by this route. The bus leaves Gorey town on a daily basis at 06:40 towards Dublin Airport and at 18:00 towards Wexford.
- Route 879 (Gorey Bus Links): Gorey. Courtown. Ballygarrett. Ballycanew
This is a local route linking Gorey to the surrounding towns. From Monday to Friday, it operates three services, leaving Gorey at 09:15, 13:10 and 17:10.
- Route ITC07 (Dunnes Coaches): Gorey Main Street. Carlow College
This route operates one single service. It leaves Gorey at 07:20 and arrives back at 18:23.
- Route 389 (Local Link Wexford): Gorey Main Street. Knockmullen. Pollshone
From Monday to Friday, this route operates four services, leaving Gorey towards Ardamine at 08:09, 18:40, 19:40 and 20:40. On Saturdays, the bus leaving at 08:09 is substituted by a service at 12:19. On Sundays, two services are provided, one leaving Gorey at 11:19 and the other at 18:49.

These listed bus routes provide frequent service to various locations, including local towns, Dublin City, Dublin Airport, Wexford town and Carlow town. The bus journey time to Dublin City Centre is approximately 2 hours, to Dublin Airport is approximately 2.5 hours and to Wexford town is approximately 1 hour.

5.2 Proposed Road Network

5.2.1 Internal Road Network

Direct vehicular access to the subject development is proposed from Carnew Road to the south and Kilnahue Lane to the north, with one access junction proposed at Carnew Road and two access junctions proposed at Kilnahue Lane. All three junctions will be priority controlled. Refer to Waterman Moylan's Proposed Road Layout drawing no. 13-119-P4100 to P4103 which accompany this application.

In addition to these vehicular access points, which will be accessible by all modes of transport, there are two pedestrian/cyclist links proposed. These are located to the north of the site, onto Gorey Hill/Kilnahue Lane, and to the south-east of the site, to the existing petrol station, which will lead out to the existing facilities along Carnew Road.

All internal roads in the proposed development are designed for a speed limit of 30km/hr, with generally a 5.5m wide carriageway, 1.5m on-road cycle lanes and minimum 1.8m footpaths along both sides. On-street parking intermixed with soft verges will separate footpaths from the main carriageway. All road intersections within the development itself will be priority controlled with raised tables where appropriate. The low design speeds and traffic calming measures will ensure the safe operation of these junctions.

5.2.2 External Road Upgrades

Several upgrades are proposed to the existing road network. At the request of Wexford County Council, it is proposed to upgrade the Carnew Road/Kilnahue Lane junction to a signalised junction. Refer to Waterman Moylan Drawing No. 13-119-P4131, which accompanies this submission. Appropriate speed limit signage is to be added as part of the junction upgrade.

Road improvements are proposed at Kilnahue Lane, including widening of the carriageway as far as the north-western boundary of the site, introduction of new footpaths and cycle lanes along the road, introduction of new traffic calming measures and introduction of a new unsignalized raised priority controlled zebra crossing with flashing amber beacons. The proposed upgrade works to Kilnahue Lane are shown on Waterman Moylan Drawing No. 13-119-P4130 and 13-119-P4131.

At Carnew Road, it is proposed to extend the existing footpath as far as the proposed site entrance, and continuing south-west beyond the entrance approximately 140m to the existing residential/agricultural access. It is also proposed to introduce a new cycle lane adjacent to the site entrance on Carnew Road, with the roadway to be widened into the verge to accommodate the new cycle lane, and to provide new street lighting and signage. The proposed upgrade works to Carnew Road are shown on Waterman Moylan Drawing No. 13-119-P4110.

These proposed upgrade works have been discussed and agreed with Wexford County Council. All of the proposed road upgrade works are to be carried out during the first phase of construction, and all of the proposed upgrade works are to be fully completed prior to any of the units in the development being occupied.

5.3 Design Manual for Urban Roads and Streets

5.3.1 Background

The stated objective of the Design Manual for Urban Roads and Streets (DMURS) is to achieve better street design in urban areas. This will encourage more people to choose to walk, cycle or use public transport by making the experience safer and more pleasant. It will lower traffic speeds, reduce unnecessary car use and create a built environment that promotes healthy lifestyles and responds more

sympathetically to the distinctive nature of individual communities and places. The implementation of DMURS is intended to enhance how we go about our business, enhance how we interact with each other, and have a positive impact on our enjoyment of the places to and through which we travel.

The proposed development has been designed to meet the objectives of DMURS, and the Design Team considers that the proposed road and street design is consistent with the principles and guidance outlined in DMURS. Outlined below are some of the specific design features that have been incorporated within the proposed scheme with the objective of delivering a design that is in compliance with DMURS.

5.3.2 Creating a Sense of Place

DMURS sets out four characteristics which represent the basic measures that should be established in order to create people friendly streets that facilitate more sustainable neighbourhoods. These characteristics are connectivity, enclosure, active edge and pedestrian activities/facilities.

Connectivity:

“The creation of vibrant and active places requires pedestrian activity. This in turn requires walkable street networks that can be easily navigated and are well connected.”

In order of importance, DMURS prioritises pedestrians, cyclists, public transport and private cars.

The proposed development has been designed with pedestrians and cyclists taking precedence over other modes of transport. In this regard, footpaths are provided throughout the development with regular pedestrian crossings along anticipated desire lines.

There are two access points provided to exclusively serve pedestrians and cyclists; one to the north of the site, onto Gorey Hill/Kilnahue Lane, and the other to the south-east of the site, to the existing petrol station, which will lead out to the existing facilities along Carnew Road.

Pedestrian crossings have been designed to allow pedestrians to cross the street at grade. The proposal includes excellent provision for cyclists, with new cycle lanes proposed on each side of the carriageway throughout the development. This provides a safe space for cyclists with the dominance of cars reduced.

Enclosure:

“A sense of enclosure spatially defines streets and creates a more intimate and supervised environment. A sense of enclosure is achieved by orientating buildings towards the street and placing them along its edge. The use of street trees can also enhance the feeling of enclosure.”

The proposed development has been designed with residential units overlooking streets and pedestrian routes. High quality landscaping and extensive tree planting are proposed throughout the scheme which creates a definitive sense of place. Road widths of generally 5.5m throughout the development ensure that a strong sense of enclosure is achieved on residential roads.

Active Edge:

“An active frontage enlivens the edge of the street creating a more interesting and engaging environment. An active frontage is achieved with frequent entrances and openings that ensure the street is overlooked and generate pedestrian activity as people come and go from buildings.”

As stated in Section 2.2.1 of DMURS, an active frontage enlivens the edge of the street, creating a more interesting and engaging environment. An active frontage is achieved with frequent entrances and openings. Section 3.4.1 of DMURS further notes that designers should avoid the creation of Dendritic networks, which place heavy restrictions on movement.

The provision of pedestrian crossings and cycle lanes will encourage and facilitate pedestrian and cyclist activity. The proposal includes strategically placed pedestrian crossings with raised tables, which will promote lower design speeds while enabling pedestrians to cross the street at grade, in accordance with Section 4.4.7 of DMURS.

On-street parking is provided throughout much of the development. On-street parking separates pedestrians from the vehicle carriageway and, as per DMURS Section 4.4.9, can calm traffic by increasing driver caution, contribute to pedestrian comfort by providing a buffer between the vehicular carriageway and footpath and provide good levels of passive security.

Pedestrian Activities/Facilities:

“The sense of intimacy, interest and overlooking that is created by a street that is enclosed and lined with active frontages enhances a pedestrian’s feeling of security and well-being. Good pedestrian facilities (such as wide footpaths and well-designed crossings) also makes walking a more convenient and pleasurable experience that will further encourage pedestrian activity.”

As outlined in the items above, the proposed development has been designed to provide excellent pedestrian connectivity, with a network of inter-connecting footpaths providing permeability throughout the site and to the surrounding area.

Throughout the site, pedestrian routes are 1.8m wide or greater which provides adequate space for two wheelchairs to pass one another. The proposal includes strategically placed pedestrian crossings with raised tables, which will promote lower design speeds while enabling pedestrians to cross the street at grade, in accordance with Section 4.4.7 of DMURS.

A shared surface zone is provided adjacent to the proposed crèche. Shared surface zones are streets designed primarily to meet the needs of pedestrians, cyclists, children and residents, where the speeds and dominance of cars is reduced.

5.3.3 Key Design Principles

DMURS sets out four core design principles which designers must have regard to when designing roads and streets. These four core principles are set out below together with a commentary establishing how these design principles have been incorporated into the design of the proposed development.

Design Principle 1: Pedestrian Activity/Facilities:

“To support the creation of integrated street networks which promote higher levels of permeability and legibility for all users and in particular more sustainable forms of transport.”

Streets have been designed in accordance with the alignment and curvature recommendations set out in DMURS Section 4.4.6. The road layout is generally orthogonal. Section 3.3.1 of DMURS notes that street networks that are generally orthogonal in nature are the most effective in terms of permeability (and legibility). Regular junctions along with raised pedestrian tables/crossings at main pedestrian desire lines will encourage reduced driving speeds.

Design Principle 2: Multi-Functional Streets:

“The promotion of multi-functional, place-based streets that balance the needs of all users within a self-regulating environment.”

The road hierarchy includes Local Access roads and home-zone / shared surfaces. The local access streets generally comprise of 5.5m wide carriageways (i.e. 2.75m wide vehicle lanes) with 1.5m wide cycle lanes and 1.8m wide footpaths on either side of the carriageway. Footpaths are often separated from the

carriageway by verges and by on-street parking bays. The inclusion of cycle lanes and footpaths throughout the development will encourage active modes of transport and promote multi-functional streets.

The proposed shared surface zone is designed primarily to meet the needs of pedestrians, cyclists, children and residents, where the speeds and dominance of cars is reduced. It is stated in Section 4.3.4 of DMURS that shared surface streets are highly desirable where movement priorities are low and there is a high place value in promoting more liveable streets, such as on Local streets within Neighbourhood and Suburbs.

The shared surface zone comprises of an 8m wide shared-surface carriageway. This will inform a clear hierarchy within the public realm, reducing the speed and dominance of cars. It is proposed to utilise a buff coloured chipping / macadam or similar approved surfacing at the shared surface zone, subject to Wexford County Council Roads and Transportation approval. Use of a shared-surface buff coloured chipping/macadam indicates to both drivers and pedestrians/cyclists that the road is a shared space. As stated in Section 4.4.2 of DMURS, paving materials can encourage a low vehicle speed shared environment. Entry treatment to the shared surface zone is provided in the form of a ramp up, which helps announce that a driver is entering into a shared surface zone.

Design Principle 3: Pedestrian Focus:

“The quality of the street is measured by the quality of the pedestrian environment.”

The design of the scheme has placed a particular focus on the pedestrian. Connectivity throughout the scheme is heavily weighted towards the pedestrian. There are excellent pedestrian links to the surrounding road networks, public transport services and amenities for both residents of the development and the wider public.

Raised tables are provided at crossing points, which allow pedestrians to continue at grade. The raised tables also promote lower vehicle speeds.

Design Principle 4: Multi-Disciplinary Approach:

“Greater communication and co-operation between design professionals through promotion plan led multidisciplinary approach to design.”

The design of the proposed scheme has been developed through the design team working closely together. The proposed development design is led by Connolly Architects working together with multiple disciplines including Waterman Moylan Consulting Engineers, Downey Planning and Rónán MacDiarmada & Associates Landscape Architects.

Public areas fronting and within the proposed development will be designed by a multidisciplinary design team to accommodate pedestrians and cyclists in accordance with the appropriate principles and guidelines set out in DMURS. In particular the vehicular access and public footways within the remit of the development will incorporate the relevant DMURS requirements and guidelines as set out above.

5.3.4 External Quality Audit

An external Quality Audit has been carried out by Bruton Consulting Engineers in accordance with Section 5.4.2 of DMURS. The audit includes a Road Safety Audit, Access Audit, Cycle Audit and Walking Audit.

The Quality Audit identified several specific issues with the design, and these issues have been remedied accordingly as per the table below:

Item	Problem Identified	Remedy
1	Limited forward visibility/stopping sight distance for drivers travelling westbound on Kilnahue Lane after the school access.	Reduce speed on Kilnahue Lane to 30kph from Junction with Carnew Road to Northern extent of proposed works so SSD = design speed.

2	There is a short section along Kilnahue Lane where the segregated cycle and pedestrian facilities are merged into a shared facility and the cross-sectional width (2.1m) is less than the segregated widths.	Reduce road width locally from 6m to 5.5m increasing shared footpath width to 2.6m.
3	No refuge area on the southern verge of the R725 for dismounted cyclists or pedestrians to wait at uncontrolled pedestrian crossing, may lead to cyclists being squeezed by passing vehicles.	Keep 1 island, remove pedestrian link from north to south of road. Provide cycleways locally through the entry gate. Provide Gateway signage, lighting and markings to make clear.
4	Corner radii at the proposed access on the R725 are 10m.	Entry radii reduced to 6m.
5	The internal junctions within the development are shown to be yield control junctions.	Stop control to be used instead of yield control.
6	The uncontrolled crossing on Road 1, chainage 142 approx is located at the base of the raised table.	The raised table has been extended to include the pedestrian crossing.
7	The topography of the site leads to many steps throughout the footpath network.	Alternative access to the adjacent open spaces is available with gradients that are in accordance with the Technical Guidance Document Part M of the Building Regulations without steps and without excessively long routes.
8	The topography of the site leads to many steps between parking spaces and residential units.	Suitable pedestrian provision with gradients in accordance with the Technical Guidance Document of Part M of the Building Regulations without steps be provided from dedicated car parking spaces to the associated residential units.
9	Trees at the corners of internal junctions could lead to a lack of visibility for drivers.	Tree types and locations are chosen such that the girth, clear stem and canopies will not interfere with visibility both when planted and when mature.
10	There is a notional pedestrian/cycle link to the Circle K Garage on the R725 but is discontinuous and the access point at the service station may not be suitable.	The link to the Topaz garage will not form part of this application.
11	The zebra crossing on Kilnahue Lane is missing tactile paving.	L-shaped red coloured tactile paving is to be provided at the crossing.

Table 7 | Quality Audit Issues and Remedies

Refer to Appendix C for the full Quality Audit report.

5.3.5 DMURS Statement of Design Consistency

As set out above, the development has been specifically designed to meet the objectives of DMURS. The Design Team considers that the proposed road and street design is consistent with the principles and guidance outlined in the Design Manual for Urban Roads and Streets (DMURS).

5.4 Traffic and Transport Assessment & Travel Plan

As noted above, a comprehensive Traffic and Transport Assessment and Travel Plan have also been prepared by Waterman Moylan and accompany this pre-planning submission under separate cover.

6. Liaison with Third Parties

This section summarises liaison undertaken with the various bodies in preparation of the SJHD submission:

Name	Party	Discussion
Joanne Kehoe & Tim O'Sullivan	WCC Roads & Drainage	Issued Roads and Surface Water drainage proposals, Quality Audit, comments issued by WCC and updated into proposals.
Nick West,	Irish Rail	Issued foul drainage proposals at Esmonde Street overpass for comment. Recommendations updated into proposals.
PJ Murphy	Irish Water	Proposals for foul and water were submitted. Confirmation of Feasibility and Statement of Design Acceptance have been issued by IW.
Norman Bruton	Bruton Engineering	Quality audit provided for on and off-site proposals and was sent onto WCC Joanne Kehoe.
WCC Meeting	Wexford County Council	Interdepartmental meeting with the Applicant to review proposals.

Appendices

A. Irish Water Confirmation of Feasibility Letter and Statement of Design Acceptance

Darragh Aiken
 Waterman Moylan
 Block S,
 EastPoint Business Park,
 Alfie Byrne Road,
 Dublin
 D03 H3F4

Uisce Éireann
 Bosca OP 448
 Oifig Sheachadta na
 Cathrach Theas
 Cathair Chorcaí

Irish Water
 PO Box 448,
 South City
 Delivery Office,
 Cork City.

www.water.ie

30 August 2021

Re: CDS21001761 pre-connection enquiry - Subject to contract | Contract denied

Connection for Multi/Mixed Use Development of 450 unit(s) at Lands at Kilanhue Lane, Gorey, Co. Wexford

Dear Sir/Madam,

Irish Water has reviewed your pre-connection enquiry in relation to a Water & Wastewater connection at Lands at Kilanhue Lane, Gorey, Co. Wexford (the **Premises**). Based upon the details you have provided with your pre-connection enquiry and on our desk top analysis of the capacity currently available in the Irish Water network(s) as assessed by Irish Water, we wish to advise you that your proposed connection to the Irish Water network(s) can be facilitated at this moment in time.

SERVICE	<p style="text-align: center;">OUTCOME OF PRE-CONNECTION ENQUIRY</p> <p style="text-align: center;"><u>THIS IS NOT A CONNECTION OFFER. YOU MUST APPLY FOR A CONNECTION(S) TO THE IRISH WATER NETWORK(S) IF YOU WISH TO PROCEED.</u></p>
Water Treatment	Feasible without infrastructure upgrade by Irish Water
Wastewater Treatment	Feasible without infrastructure upgrade by Irish Water
Water Network	<p>Upgrades as per modelling report for 350 houses in pervious PCE apply to this PCE. Modelling report in Appendix A. Existing pump capacity at Gorey Hill Booster PS to be confirmed and reviewed at the time of connection application.</p> <p>However please note Irish Water have issued a large volume of COF's for Gorey. Should a sufficient number of these developments connect to the network in the interim prior to you receiving a connection offer, additional upgrade to the water network may be required.</p>

Wastewater Network

The nearest foul sewer is approximately 310m from the proposed development. A sewer extension would be required to service the proposed development with the costs borne fully by the developer. A further 325m approx. of existing DN150 sewer on R725 will need to be upsized.

IW have undertaken a review of the impact this development will have on the wastewater network downstream. 611m approx. of sewer in Gorey town centre would need to be upsized to cater for this new development.

- 345m approx. of DN225 to be upsized to DN375 in Main Street
- 189m approx. of DN225 to be upsized to DN375 in Esmonde Street
- 77m approx. of DN525 to be upsized to DN750 in Courtown Road

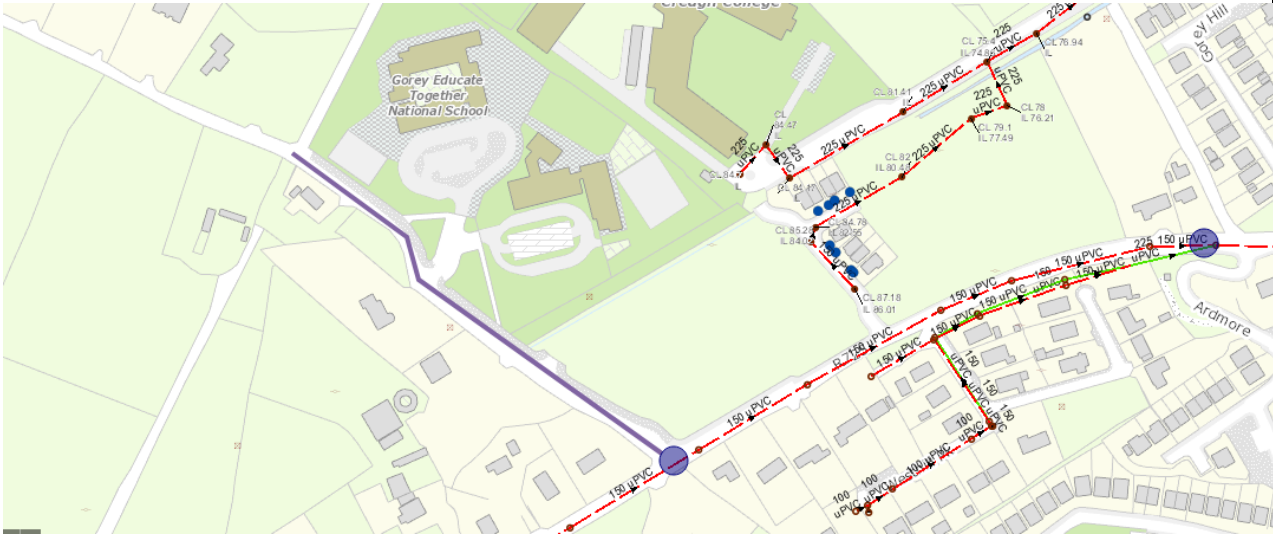
Irish Water will require you to provide a contribution of the relevant portion of the costs for the required upgrades, please contact Irish Water to discuss this further.

However please note Irish Water have issued a large volume of COF's for Gorey. In order to support these developments Irish Water is to undertake a Drainage Area Plan (DAP) for Gorey. This DAP is to commence end 2021 but it will be 2023-2024 before a verified model is available – subject to change.

Should these studies find additional constraints in the foul network using the verified DAP model, Irish Water may require you to provide a contribution of the relevant portion of the costs for the required upgrades. Any additional works on the wastewater network are within the public realm which should not require planning permission. All upgrades to be confirmed at Connection Application stage.

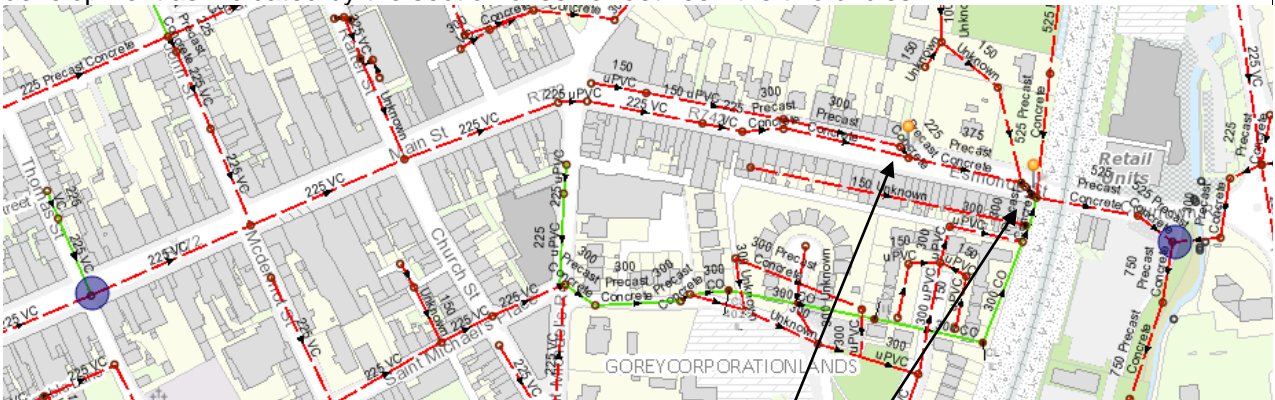
The design and construction of the Water & Wastewater pipes and related infrastructure to be installed in this development shall comply with the Irish Water Connections and Developer Services Standard Details and Codes of Practice that are available on the Irish Water website. Irish Water reserves the right to supplement these requirements with Codes of Practice and these will be issued with the connection agreement.

The map included below outlines the current Irish Water infrastructure adjacent to your site:



Sewer network adjacent to the site. 310m approx. sewer extension and 325m approx. of upsizing the existing DN150 on the F725 indicated by the section between the two circles.

611m approx. of sewer in Gorey town centre would need to be upsized to cater for this new development as indicated by the section of sewer between the two circles.



The 70m of existing DN375 sewer to the eastern end of Esmond Street does not need to be upsized

Reproduced from the Ordnance Survey of Ireland by Permission of the Government. License No. 3-3-34


Whilst every care has been taken in its compilation Irish Water gives this information as to the position of its underground network as a general guide only on the strict understanding that it is based on the best available information provided by each Local Authority in Ireland to Irish Water. Irish Water can assume no responsibility for and give no guarantees, undertakings or warranties concerning the accuracy, completeness or up to date nature of the information provided and does not accept any liability whatsoever arising from any errors or omissions. This information should not be relied upon in the event of excavations or any other works being carried out in the vicinity of the Irish Water underground network. The onus is on the parties carrying out excavations or any other works to ensure the exact location of the Irish Water underground network is identified prior to excavations or any other works being carried out. Service connection pipes are not generally shown but their presence should be anticipated.

General Notes:

- 1) The initial assessment referred to above is carried out taking into account water demand and wastewater discharge volumes and infrastructure details on the date of the assessment. **The availability of capacity may change at any date after this assessment.**
- 2) This feedback does not constitute a contract in whole or in part to provide a connection to any Irish Water infrastructure. All feasibility assessments are subject to the constraints of the Irish Water Capital Investment Plan.
- 3) The feedback provided is subject to a Connection Agreement/contract being signed at a later date.
- 4) A Connection Agreement will be required to commencing the connection works associated with the enquiry this can be applied for at <https://www.water.ie/connections/get-connected/>
- 5) A Connection Agreement cannot be issued until all statutory approvals are successfully in place.
- 6) Irish Water Connection Policy/ Charges can be found at <https://www.water.ie/connections/information/connection-charges/>
- 7) Please note the Confirmation of Feasibility does not extend to your fire flow requirements.
- 8) Irish Water is not responsible for the management or disposal of storm water or ground waters. You are advised to contact the relevant Local Authority to discuss the management or disposal of proposed storm water or ground water discharges
- 9) To access Irish Water Maps email datarequests@water.ie
- 10) All works to the Irish Water infrastructure, including works in the Public Space, shall have to be carried out by Irish Water.

If you have any further questions, please contact PJ Murphy from the design team on 022 52267 or email pjmurphy@water.ie For further information, visit **www.water.ie/connections**.

Yours sincerely,



Yvonne Harris

Head of Customer Operations

Appendix A
Water Modelling Report

Irish Water Blank Form IW-AMT-FM-024	Revision: 1.0	Approved By: Lar Spain
	Hydraulic Model Network Assessment	

Enquiry Type: Pre Connection Enquiry

General Information

Project Number (AI):	AI-2018-0099	NCE Ref:	N/A
Prepared by:	L. Seminario	Checked by:	M. Conn
Date:	27/06/2018		
Water Supply Scheme:	Gorey Regional Creagh (SZPUB1972)		
WTP Name:	Creagh WTP	DMA Ref:	Gorey Main Street (MA03820)
Development Location:	Lands at Kilnahue Lane, Gorey, Co. Wexford.		
Description of the Development:	Housing development (350 units). New water connection(s) required.		

Model Data

Model Used (File Name):	3300_FF04_AST_Q016_Hydraulic Models_Gorey Courttown Design Model.	Software:	EPANET
Year of Last Calibration:	2012	Model Type:	Detailed
Development Flow:	Average (l/s)	Peak (l/s)	
	2.08	6.59	

Option 1. Model-GIS Screenshot of Preferred Solution: Upsizing of Existing Gorey Hill Booster Station

NOTE-1: Creagh WTP: Yield = n/a. Design Capacity = 2.5 MLD. Current Production = 2.8 MLD (07/2018); 2.1 MLD (04/2018). TWL = 110 mAOD. **CHECK and CONFIRM maximum production capacity and clean water storage capacity.** **NOTE-2:** There are developments in the area for approx. other 576 housing units (AS) (approx. +354 m³/d). Supply to the town from nearby wells in the South should be considered so production capacity in the plant is made available for developments.

UPSIZING OF EXISTING GOREY HILL BOOSTER STATION: 84 mAOD.

- EXISTING SET OF PUMPS to supply the same areas as now and a small part of the development (sector below 110 mAOD). **CHECK** existing maximum capacity.
- A NEW SET OF PUMPS is required to supply most of the development (sub-sector above 110 mAOD). A new 150 mm NB rising main is required for that purpose. **CHECK availability of space for this expansion.** Otherwise, an alternative solution is provided in Page 2.

Model Outputs

Does development adversely impact existing customers?	YES. Pressures below are model-based pressures. Values between brackets correspond to pressures without the development. Values outside of the brackets correspond to the situation whether the development would be supplied through the existing network.		
Min. Press. at Connection Point (CP)	CP-1: n/a	CP-2: 14 m (32 m)	
Minimum Pressure at CMP	CMP-1: 10 m (12 m)	CMP-2: 9 m (27 m)	CMP-3: n/a
Maximum Headloss Supply Main	Between 7 and 10 m/km along the 2''/4'' uPVC shown above.		
Is Development Feasible?	Network Upgrades Required		

Model Assumptions and Disclaimers

- 1) Model Calibrated (2012). Model flows checked with Data Book. Telemetry data not available at the time.
- 2) DMA and/or supply zone boundaries not confirmed with LA.
- 3) Fireflows (Class A1: 8 l/s). Upgrades and upsizings mentioned above are required to meet fireflow requirements.
- 4) Existing customers located at highest ground elevation in model, assumed to be CMP (CMP: Critical Monitoring Point).
- 5) If network upgrades required, they will be analysed on request from New Connections

NOTE-1: CREAGH WTP: Yield = n/a. Design Capacity = 2.5 MLD. Current Production = 2.8 MLD (07/2018); 2.1 MLD (04/2018). TWL = 110 mAOD. CHECK and CONFIRM maximum production capacity and clean water storage capacity.

NOTE-2: There are developments in the area for approx. other 576 housing units (AS) (approx. +354 m³/d). Supply to the town from nearby wells in the South should be considered so production capacity in the plant is

Proposed upgrade of approx. 0.2 km of existing 100 mm uPVC main to new 150 mm NB

Proposed upgrade of approx. 0.5 km of existing 4" uPVC main downstream Gorey Hill to new 150 mm NB

PROPOSED NEW KILNAHUE LANE BOOSTER REQUIRED (Supply to sector above 110 mAOD)

CP-1: 110 mAOD (Supply to sector)

Proposed approx. 0.2 km of NEW 150 mm NB

From Creagh WTP

CHECK and CONFIRM the diameter and the status (OPEN) of any existing isolation valve along this 250mm uPVC main

CMP-3: 135

DEVELOPMENT SITE
Sector above 110 mAOD
Sector below 110 mAOD

Proposed upgrade of approx. 0.3 km of existing 4"/2" uPVC main upstream Gorey Hill Booster Pump Station to new 200 mm NB

CMP-2: 110 mAOD

CP-2: 105 mAOD (Supply to sector below 110 mAOD)

EXISTING GOREY HILL BOOSTER STATION: 84 mAOD. CHECK existing capacity. Upsizing may be required to meet the demand increase linked to the development (+ 54 m³/h are required). Pressures downstream are valid to supply any property below or around 110 mAOD but insufficient to supply any zone above approx. 110 mAOD. A new booster is required downstream in the network for that purpose ("NEW KILNAHUE LANE BOOSTER STATION").

Notes and Comments

Darragh Aiken

29 October 2021

Uisce Éireann
Bosca OP 448
Oifig Sheachadta na
Cathrach Theas
Cathair Chorcaí

Irish Water
PO Box 448,
South City
Delivery Office,
Cork City.

www.water.ie

**Re: Design Submission for Lands at Kilanhue Lane, Gorey, Co. Wexford (the “Development”)
(the “Design Submission”) / Connection Reference No: CDS21001761**

Dear Darragh Aiken,

Many thanks for your recent Design Submission.

We have reviewed your proposal for the connection(s) at the Development. Based on the information provided, which included the documents outlined in Appendix A to this letter, Irish Water has no objection to your proposals.

This letter does not constitute an offer, in whole or in part, to provide a connection to any Irish Water infrastructure. Before you can connect to our network you must sign a connection agreement with Irish Water. This can be applied for by completing the connection application form at www.water.ie/connections. Irish Water’s current charges for water and wastewater connections are set out in the Water Charges Plan as approved by the Commission for Regulation of Utilities (CRU)(https://www.cru.ie/document_group/irish-waters-water-charges-plan-2018/).

You the Customer (including any designers/contractors or other related parties appointed by you) is entirely responsible for the design and construction of all water and/or wastewater infrastructure within the Development which is necessary to facilitate connection(s) from the boundary of the Development to Irish Water’s network(s) (the “**Self-Lay Works**”), as reflected in your Design Submission. Acceptance of the Design Submission by Irish Water does not, in any way, render Irish Water liable for any elements of the design and/or construction of the Self-Lay Works.

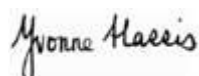
If you have any further questions, please contact your Irish Water representative:

Name: Pj Murphy

Phone: 022 52267

Email: pjmurphy@water.ie

Yours sincerely,



Yvonne Harris
Head of Customer Operations

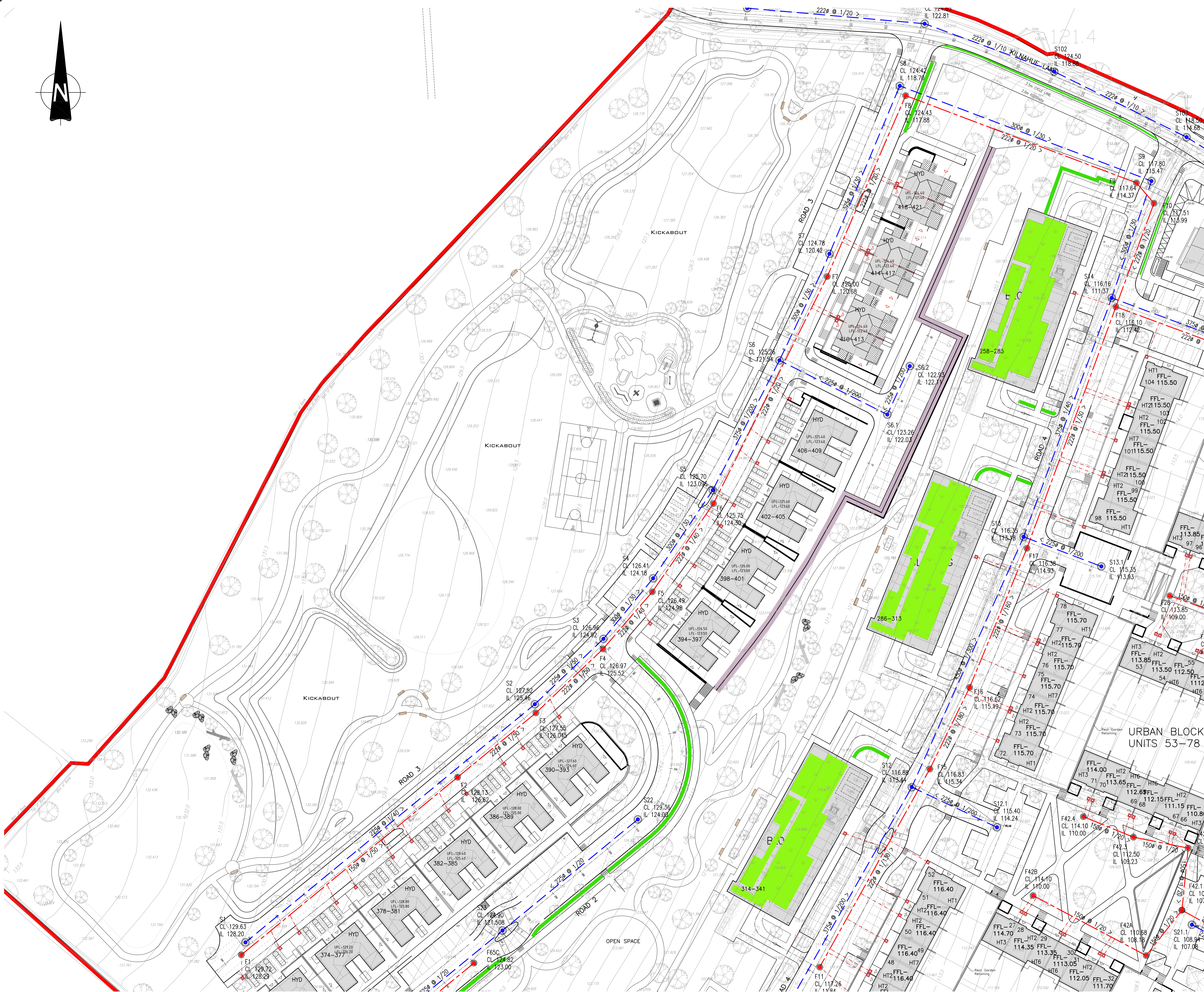
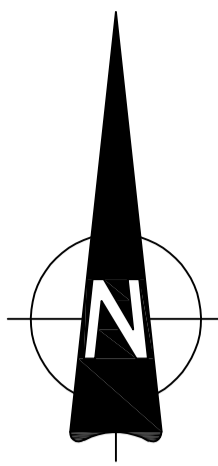
Appendix A

Document Title & Revision

- [13-119-P4201/2/3/4/5 Drainage Layout Sheets 1 to 5 inclusive, 13-119-P4220 Foul Long Sections Sheet 1 to 2 inclusive]
- [13-119-P4301/2/3/4/5/6 Watermain Layouts Sheets 1 to 6 inclusive]

For further information, visit www.water.ie/connections

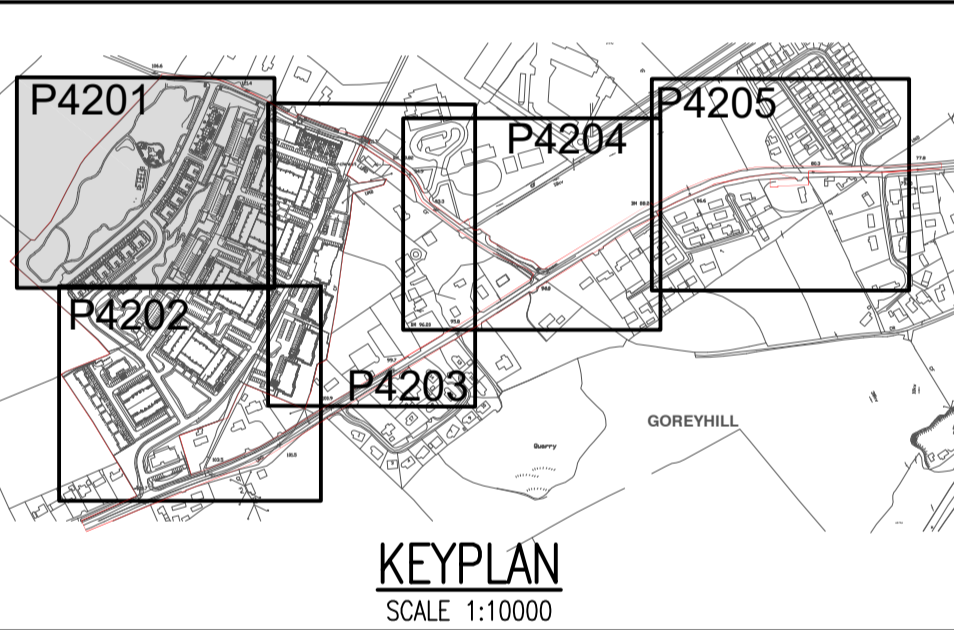
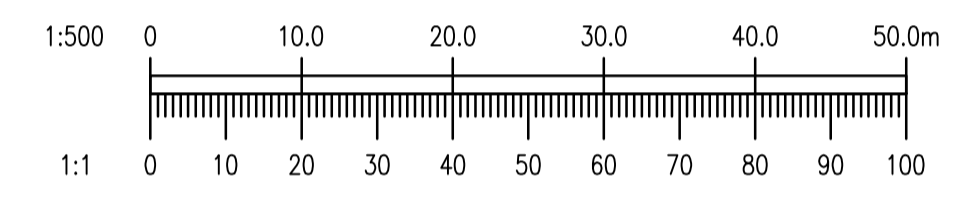
Notwithstanding any matters listed above, the Customer (including any appointed designers/contractors, etc.) is entirely responsible for the design and construction of the Self-Lay Works. Acceptance of the Design Submission by Irish Water will not, in any way, render Irish Water liable for any elements of the design and/or construction of the Self-Lay Works.



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LEGEND:

- EXF CL X IL X EXISTING FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- EXS CL X IL X EXISTING SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- XXXmm @ 1/XXX uPVC SN8 FX CL X IL X PROPOSED FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- XXXmm @ 1/XXX SX CL X IL X PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- PROPOSED FOUL INSPECTION CHAMBER AND CONNECTION
- PROPOSED SURFACE WATER INSPECTION CHAMBER AND CONNECTION
- PROPOSED PERFORATED PIPE
- PROPOSED GULLY AND CONNECTION
- PROPOSED SOAK PIT
- PROPOSED UNDERGROUND ATTENUATION STORAGE



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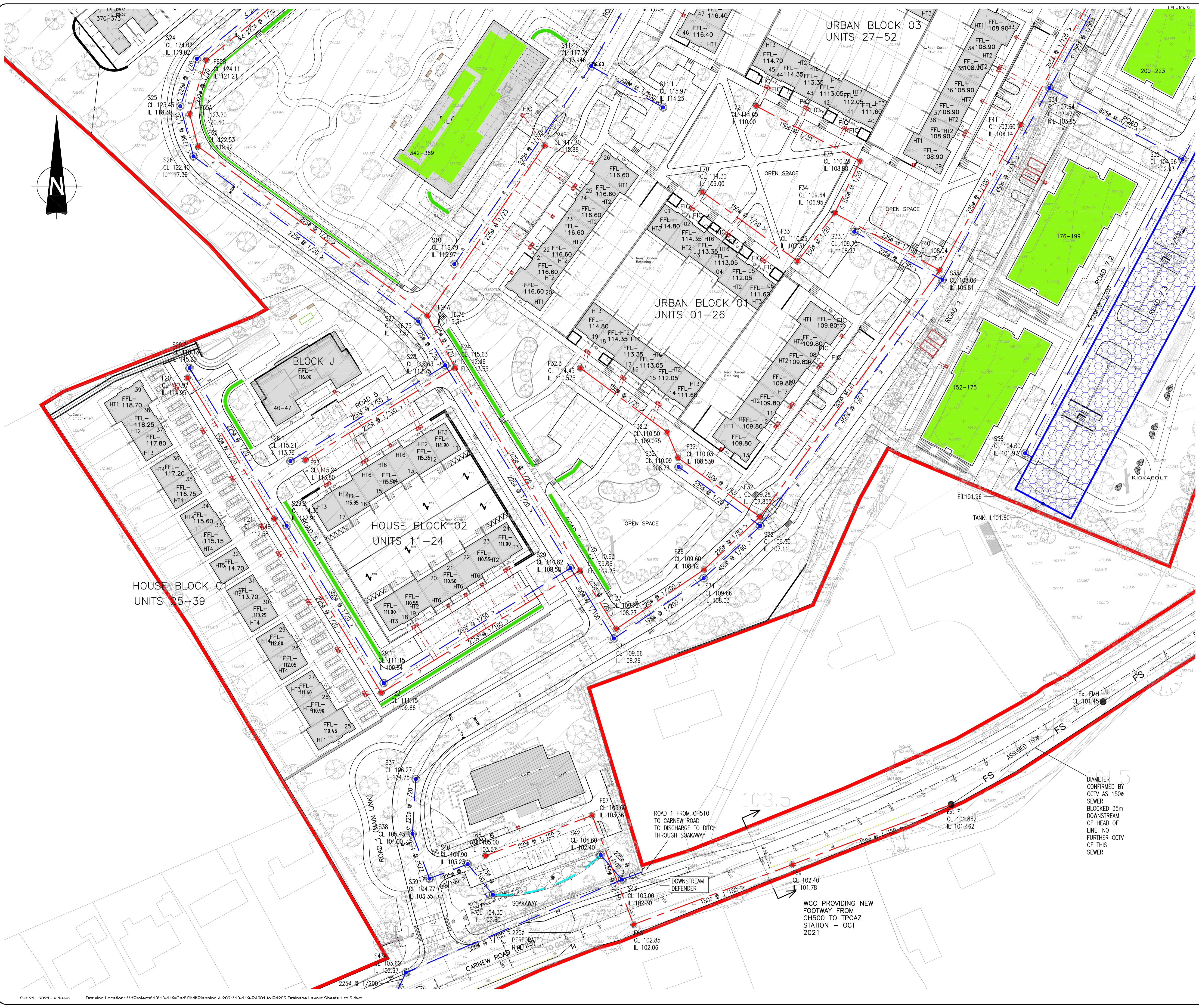
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PROJECT **LANDS AT KILNAHUE & GOREY HILL, GOREY**
TITLE **PROPOSED DRAINAGE LAYOUT SHEET 1 OF 5**

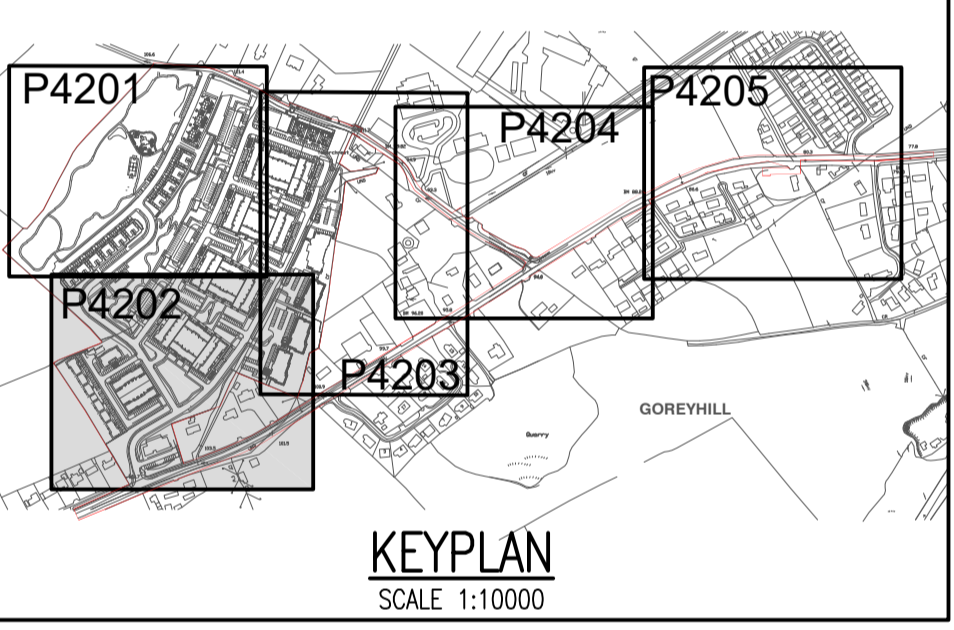
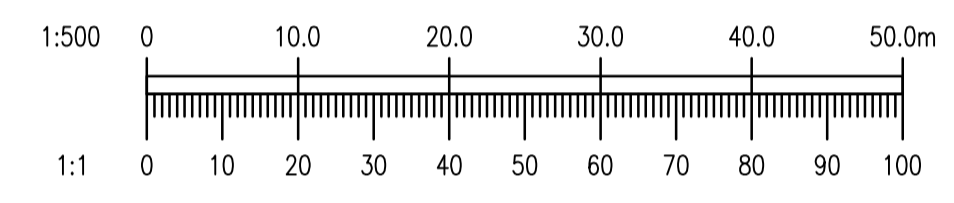
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SW	EXISTING SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
XXXmm @ 1/XXX	PROPOSED FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
uPVC S18	PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
XXXmm @ 1/XXX	PROPOSED FOUL INSPECTION CHAMBER AND CONNECTION
---	PROPOSED SURFACE WATER INSPECTION CHAMBER AND CONNECTION
---	PROPOSED PERFORATED PIPE
G	PROPOSED GULLY AND CONNECTION
---	PROPOSED SOAK PIT
---	PROPOSED UNDERGROUND ATTENUATION STORAGE



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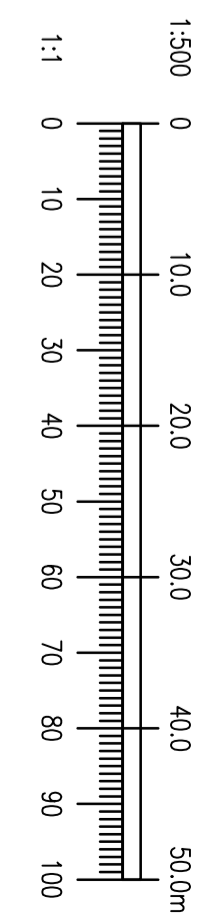
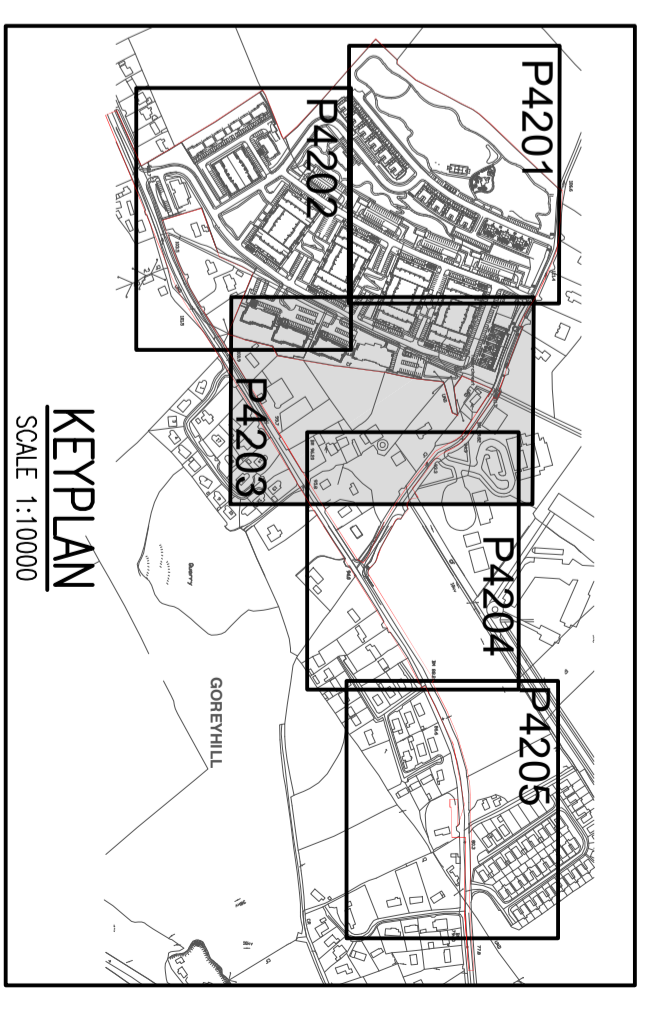
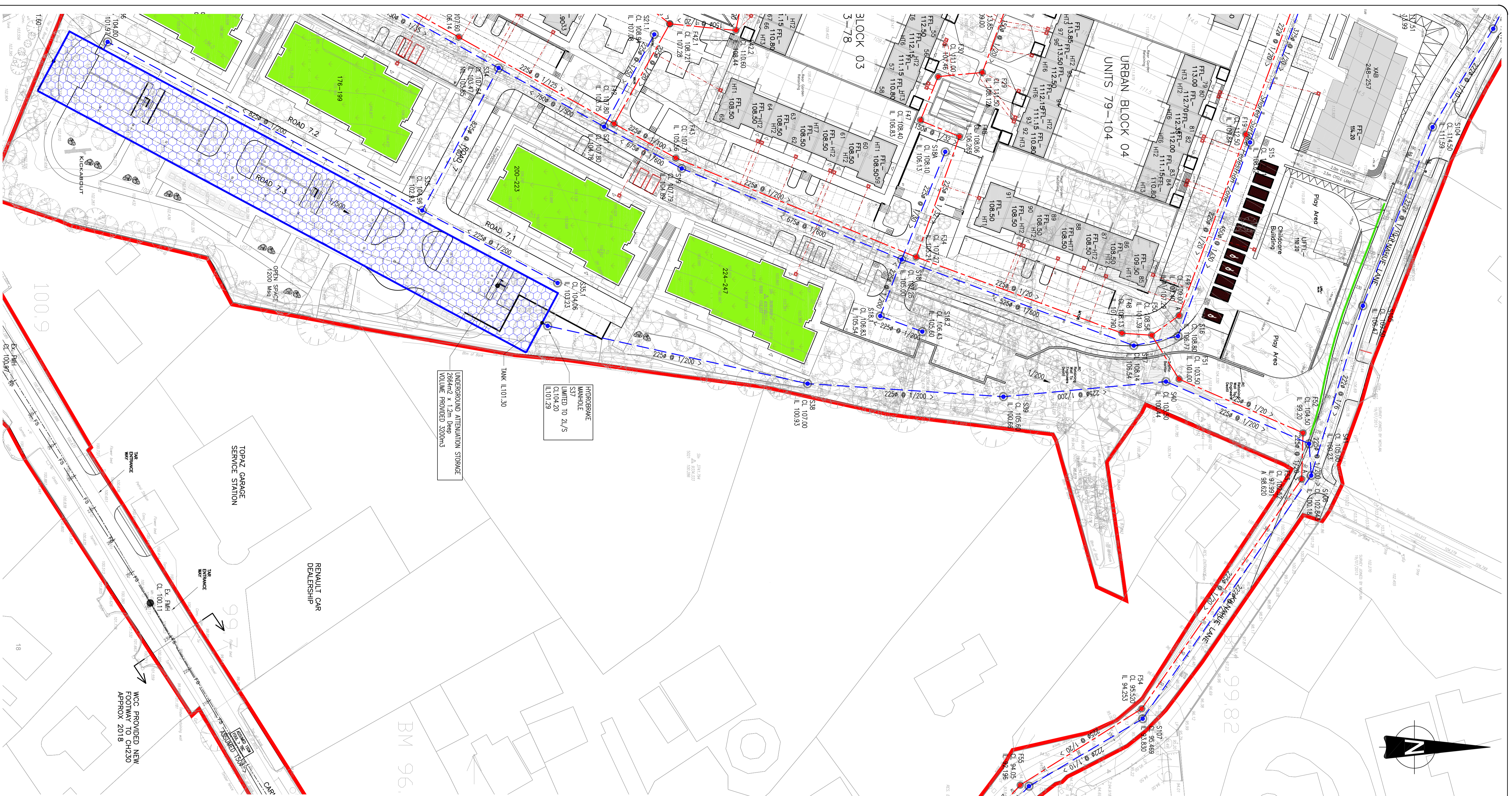
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- CL X EXISTING SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- FX PROPOSED FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- CL X PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- XXmm @ 1/XXX PROPOSED FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- XXmm @ 1/XXX PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- PROPOSED FOUL INSPECTION CHAMBER AND CONNECTION
- PROPOSED SURFACE WATER INSPECTION CHAMBER AND CONNECTION
- PROPOSED PERFORATED PIPE
- PROPOSED GULLY AND CONNECTION
- PROPOSED SOAK PIT
- PROPOSED UNDERGROUND ATTENUATION STORAGE



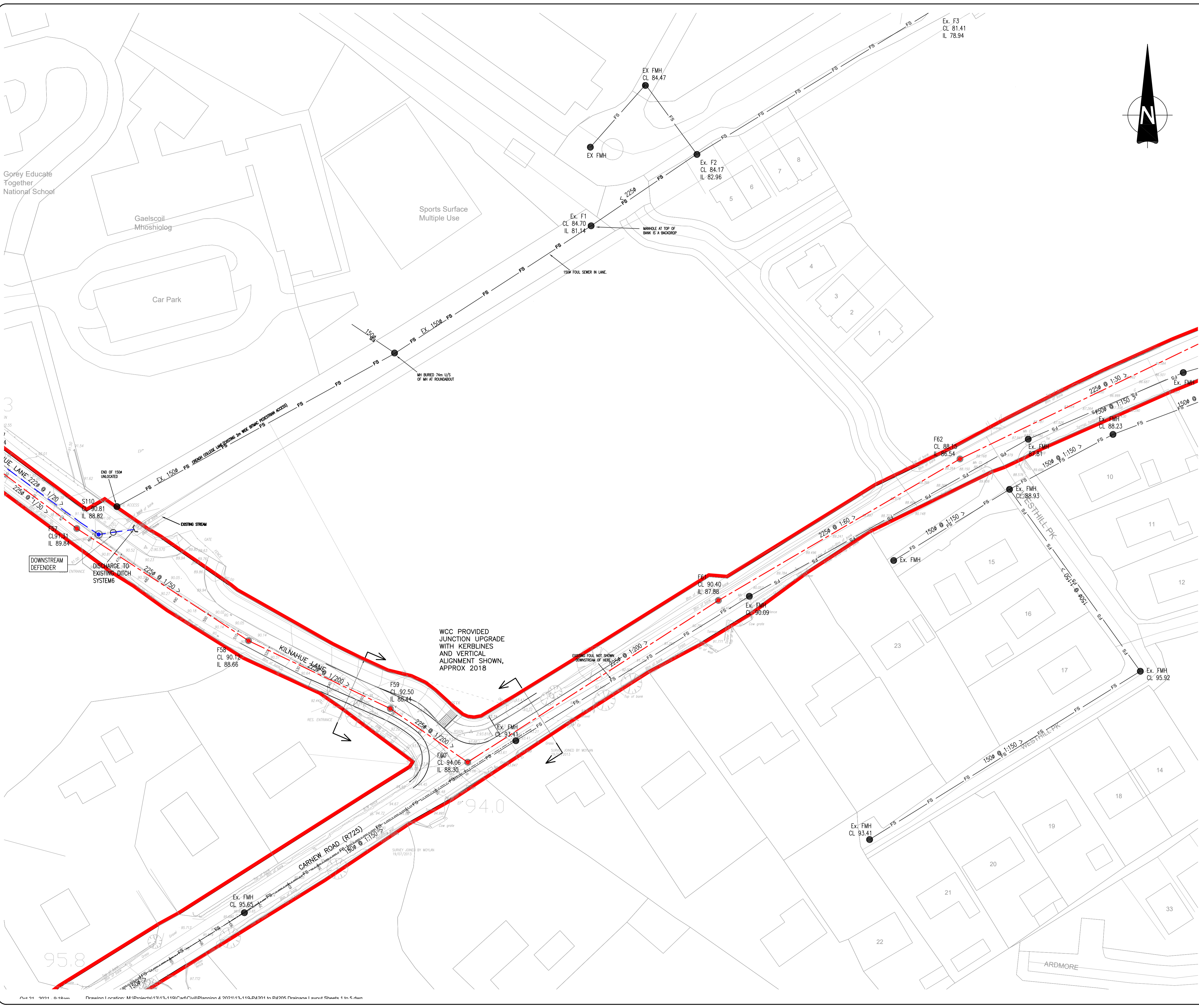
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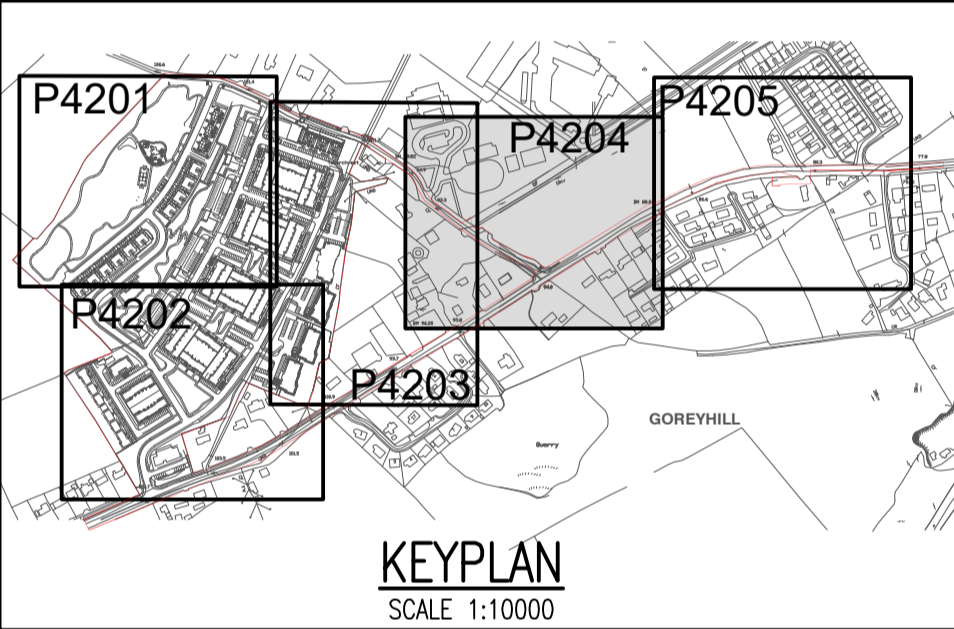
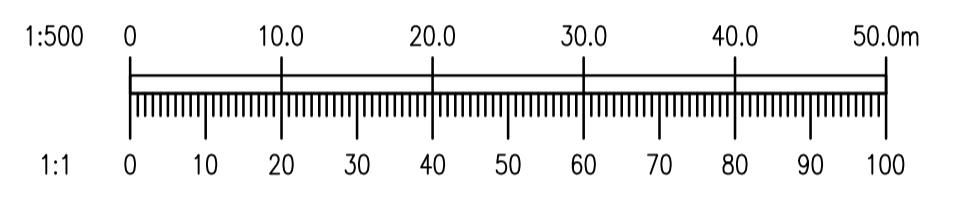
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- SW CL X IL X: EXISTING SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- XXXmm @ 1/XXX uPVC SN8: PROPOSED FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- XXXmm @ 1/XXX SX: PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- - - - -: PROPOSED FOUL INSPECTION CHAMBER AND CONNECTION
- - - - -: PROPOSED SURFACE WATER INSPECTION CHAMBER AND CONNECTION
- - - - -: PROPOSED PERFORATED PIPE
- G: PROPOSED GULLY AND CONNECTION
- [Symbol]: PROPOSED SOAK PIT
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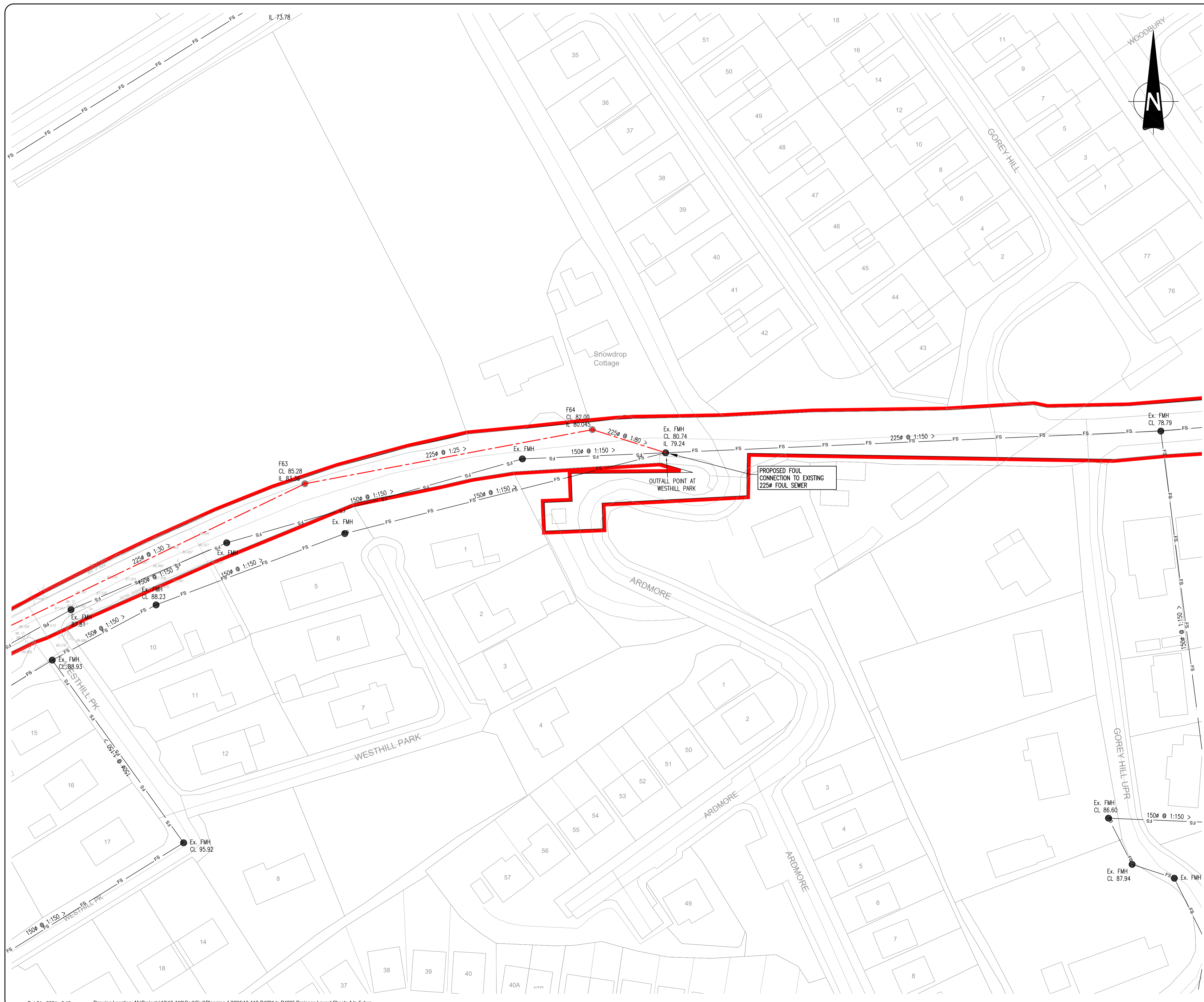
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TITLE	PROPOSED DRAINAGE LAYOUT SHEET 4 OF 5

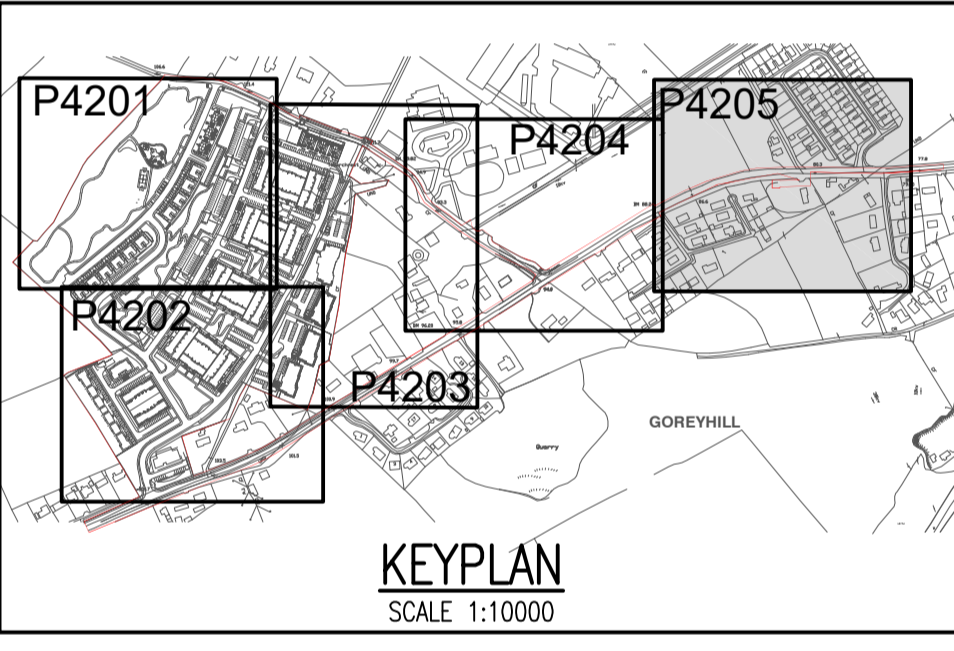
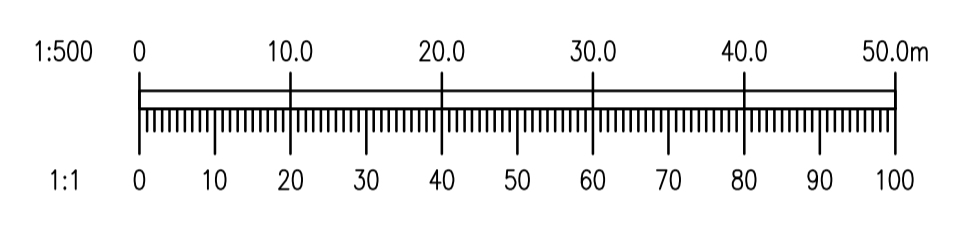
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- EXS CL X IL X: EXISTING SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- FX CL X IL X: PROPOSED FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- SX CL X IL X: PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
- Proposed Foul Inspection Chamber and Connection
- Proposed Surface Water Inspection Chamber and Connection
- Proposed Perforated Pipe
- Proposed Gully and Connection
- Proposed Soak Pit
- Proposed Underground Attenuation Storage



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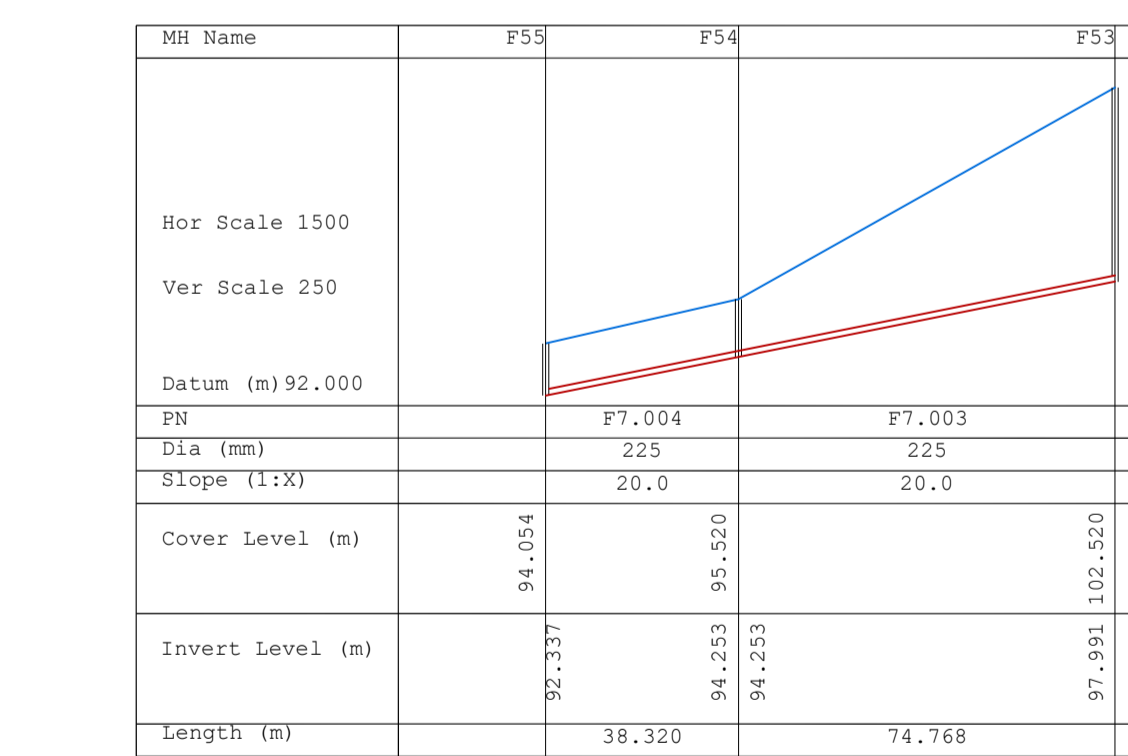
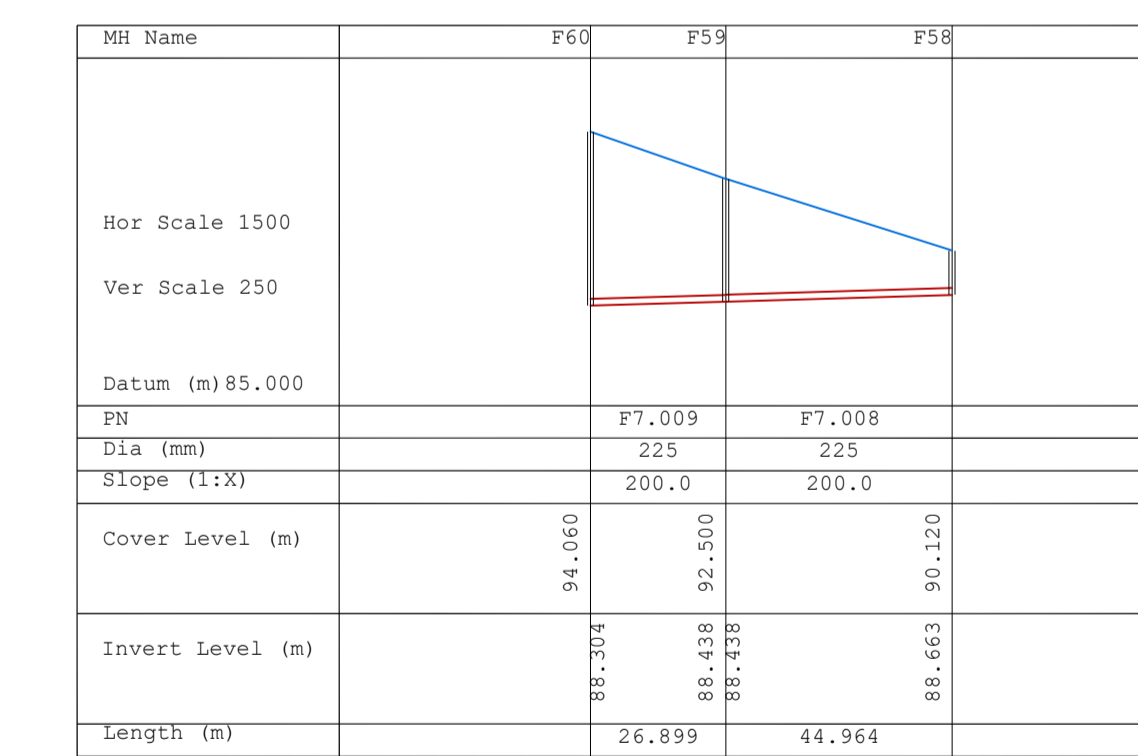
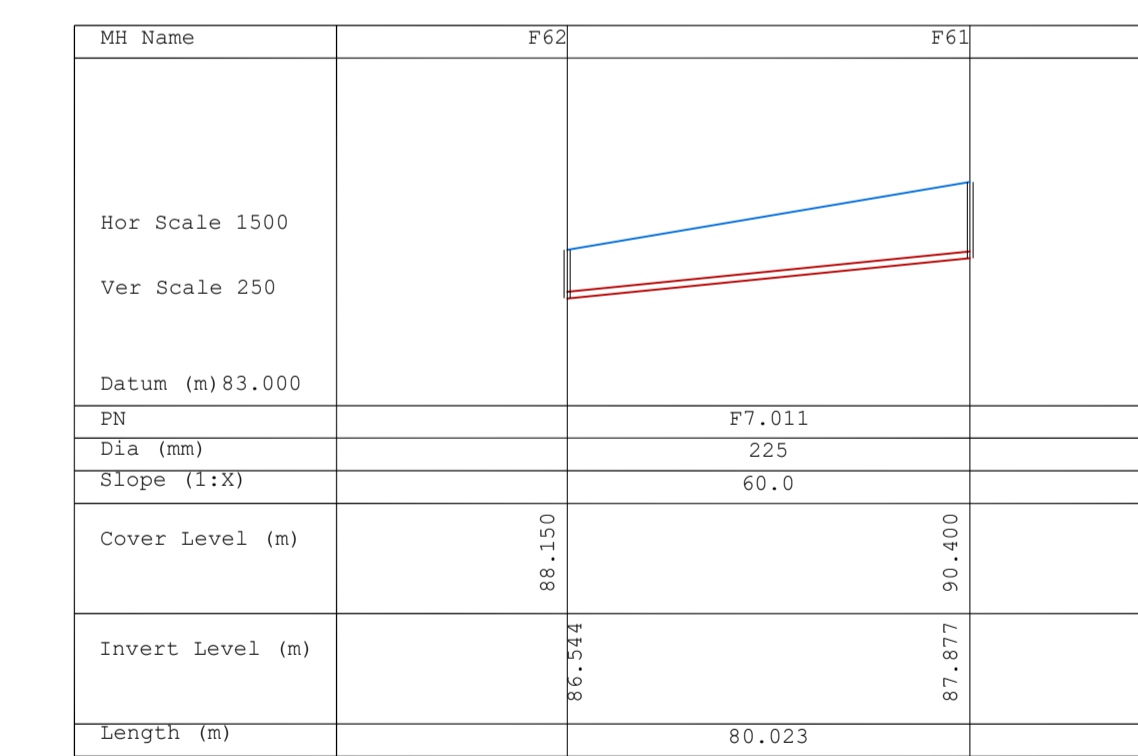
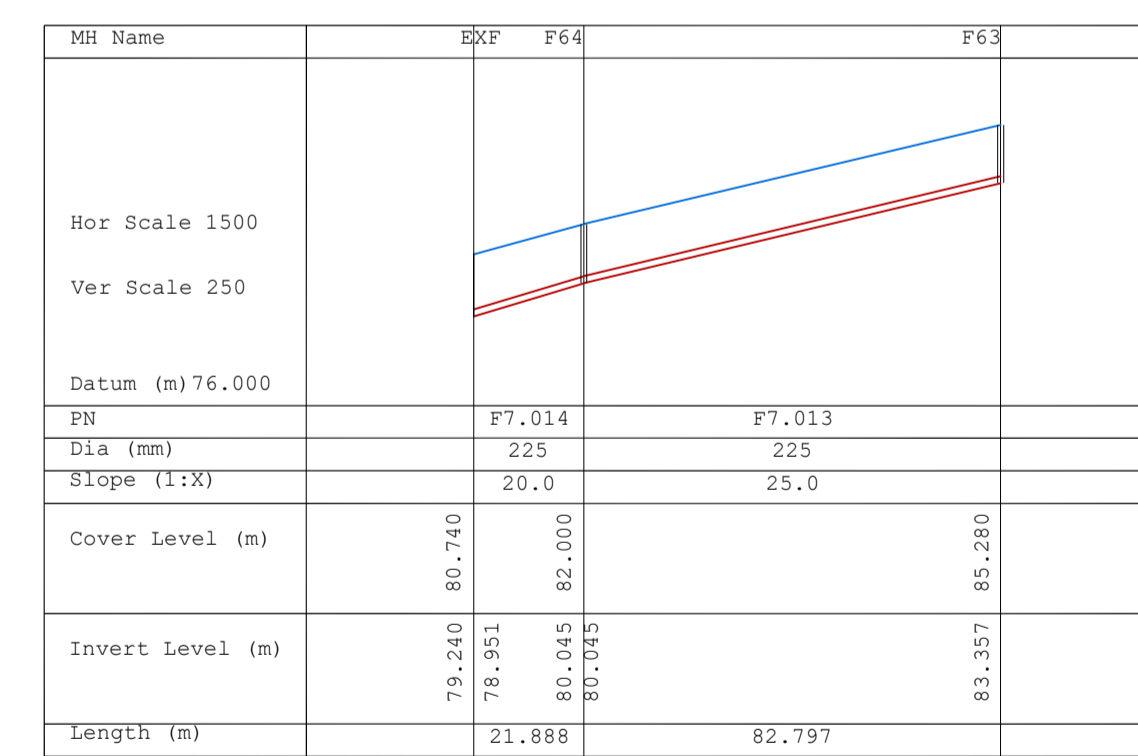
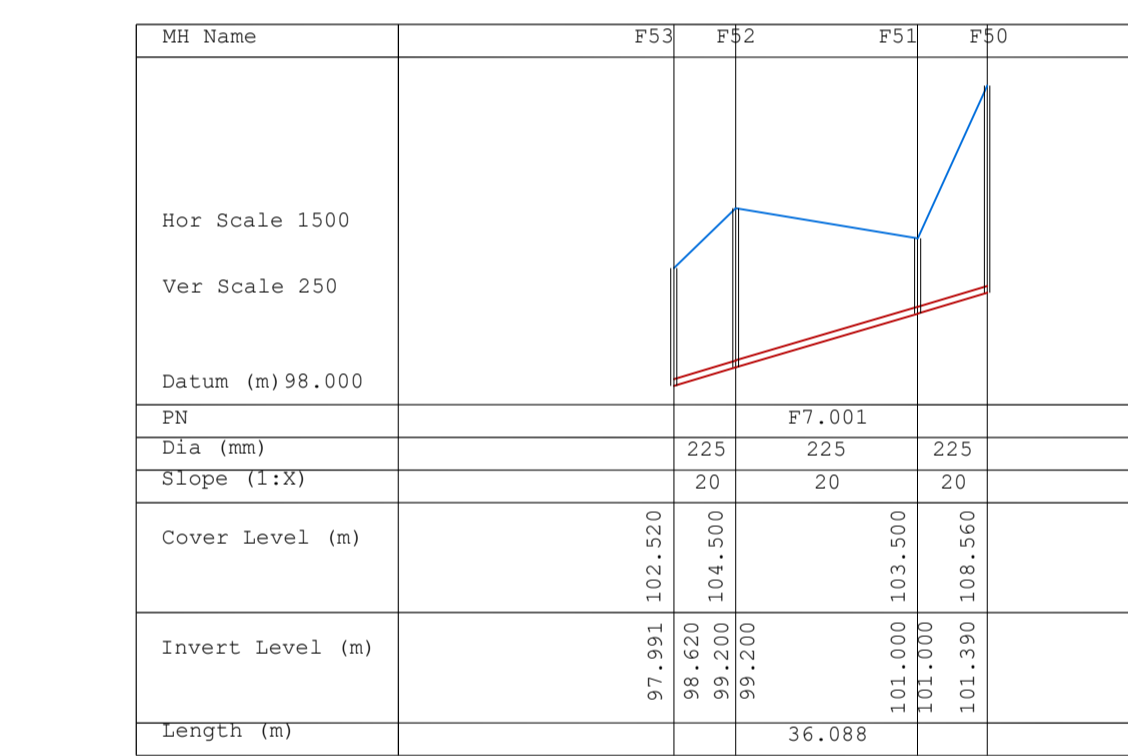
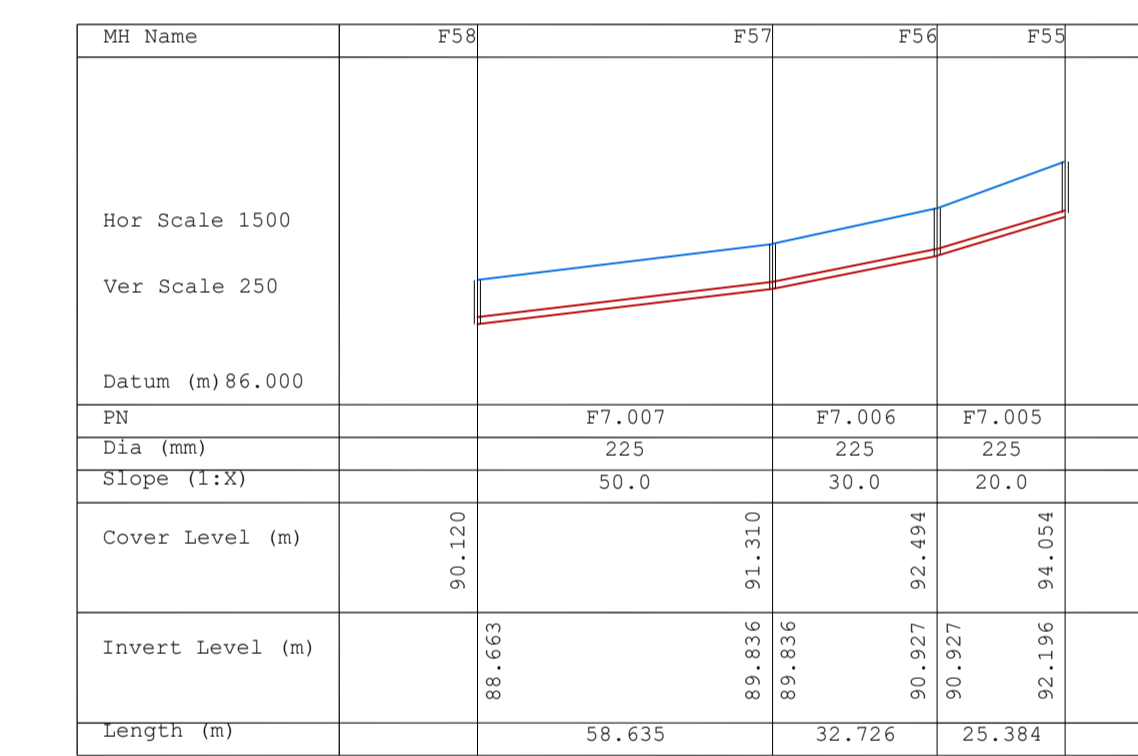
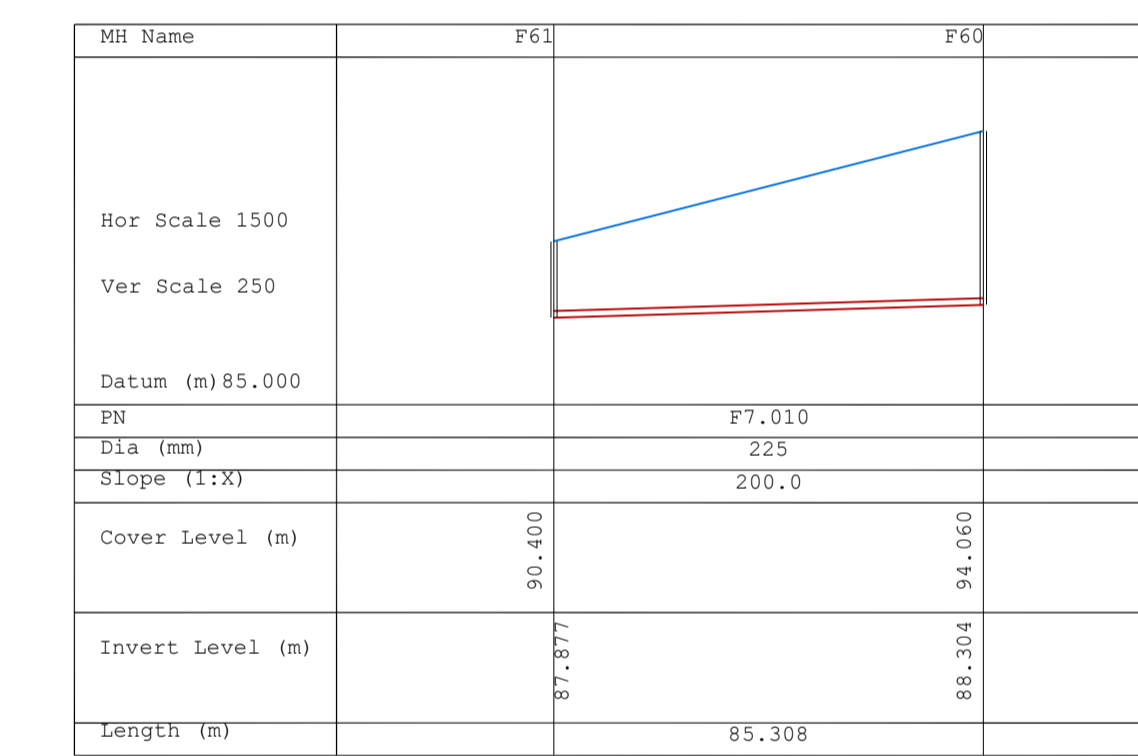
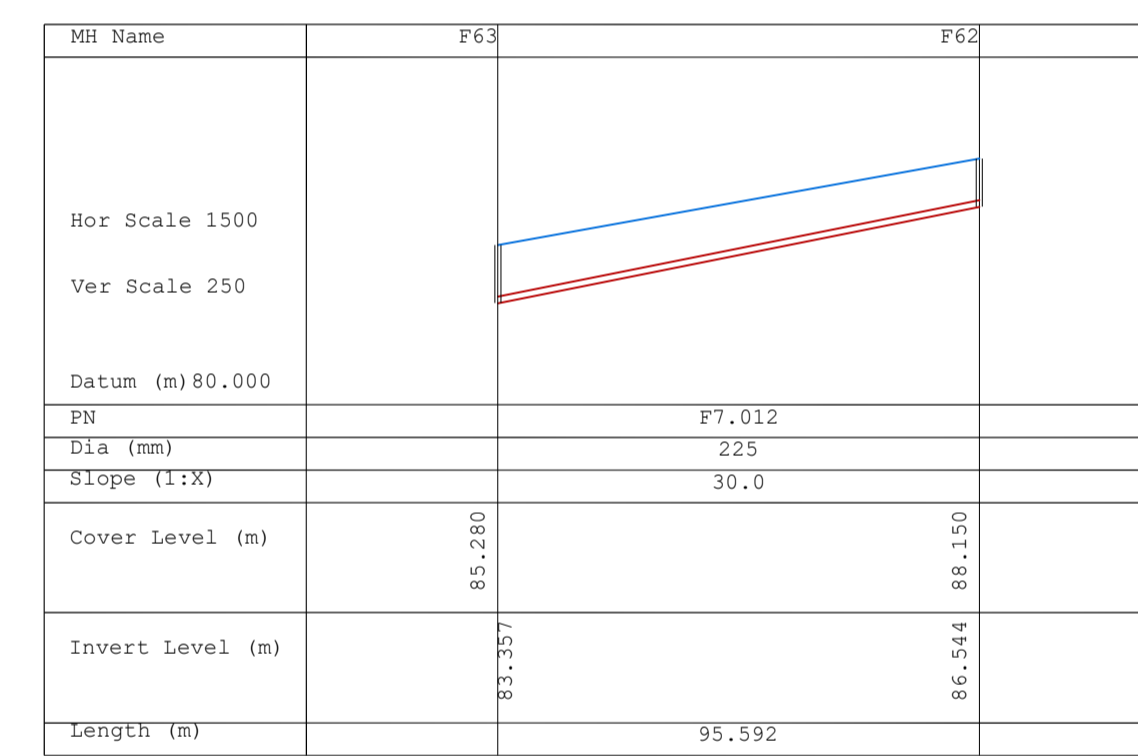
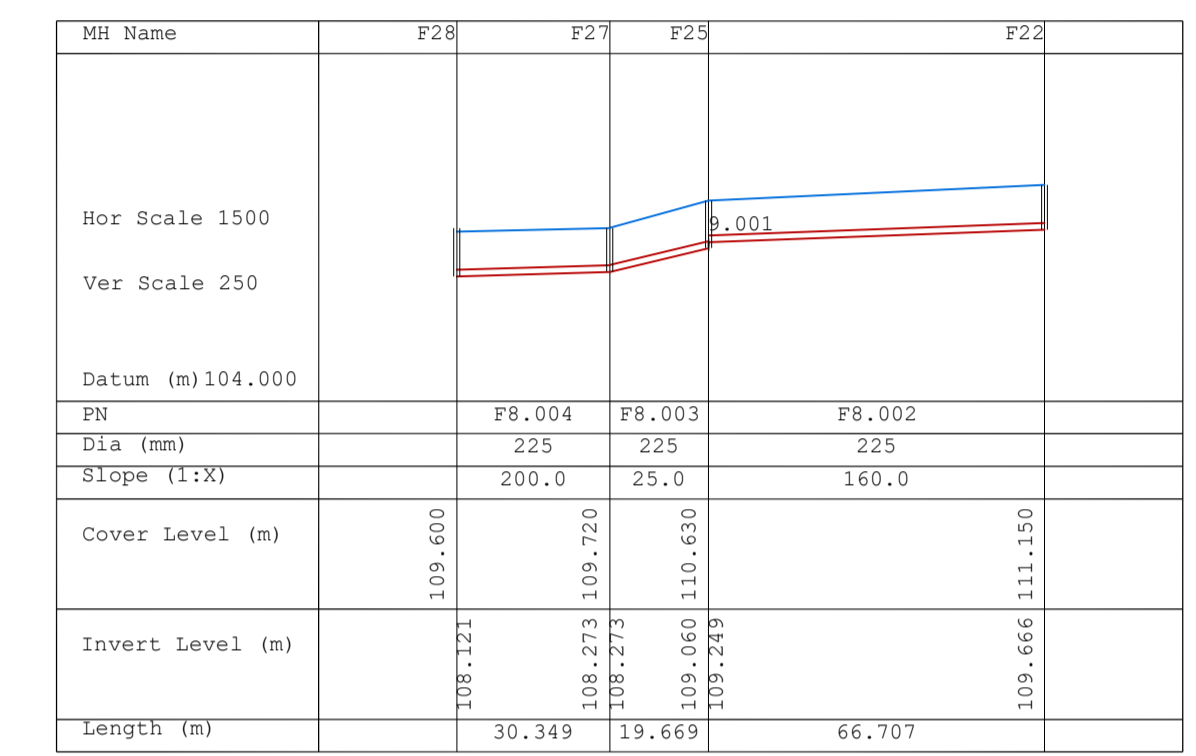
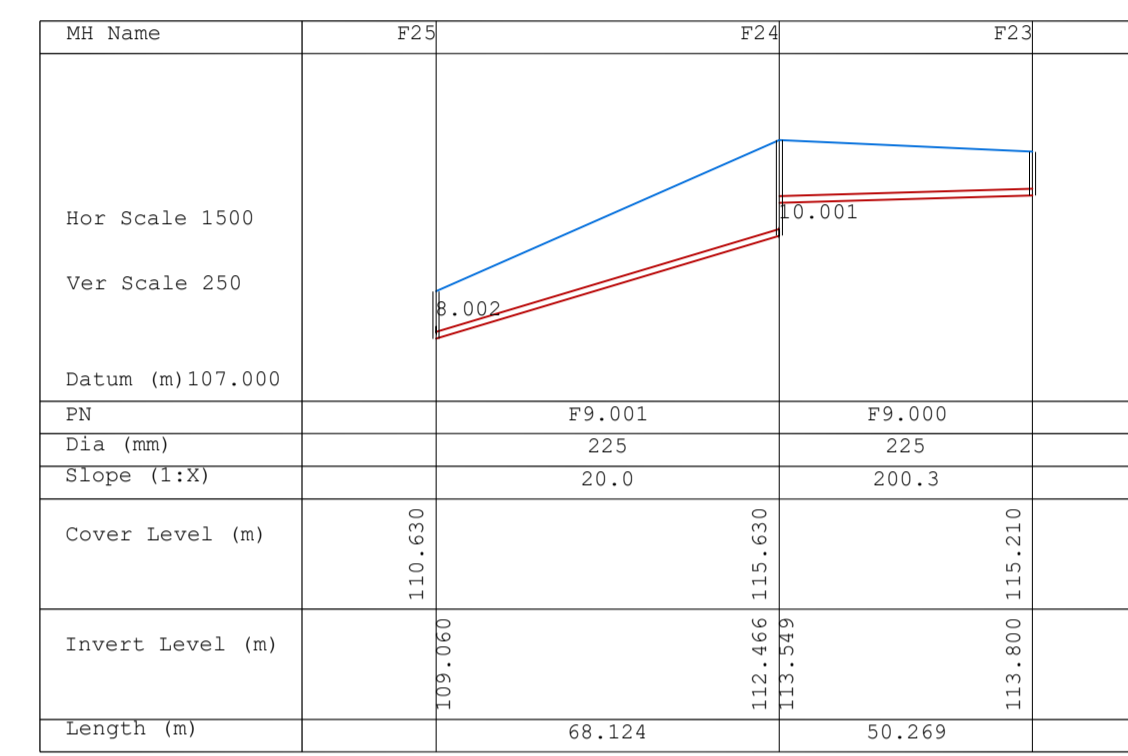
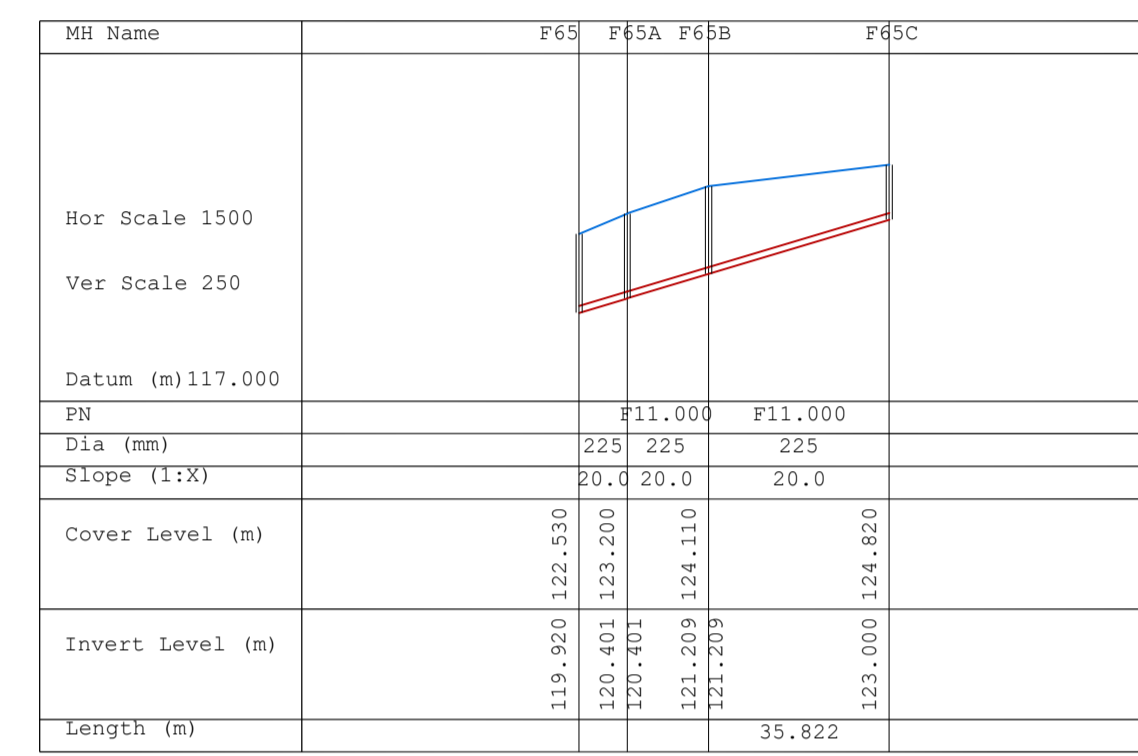
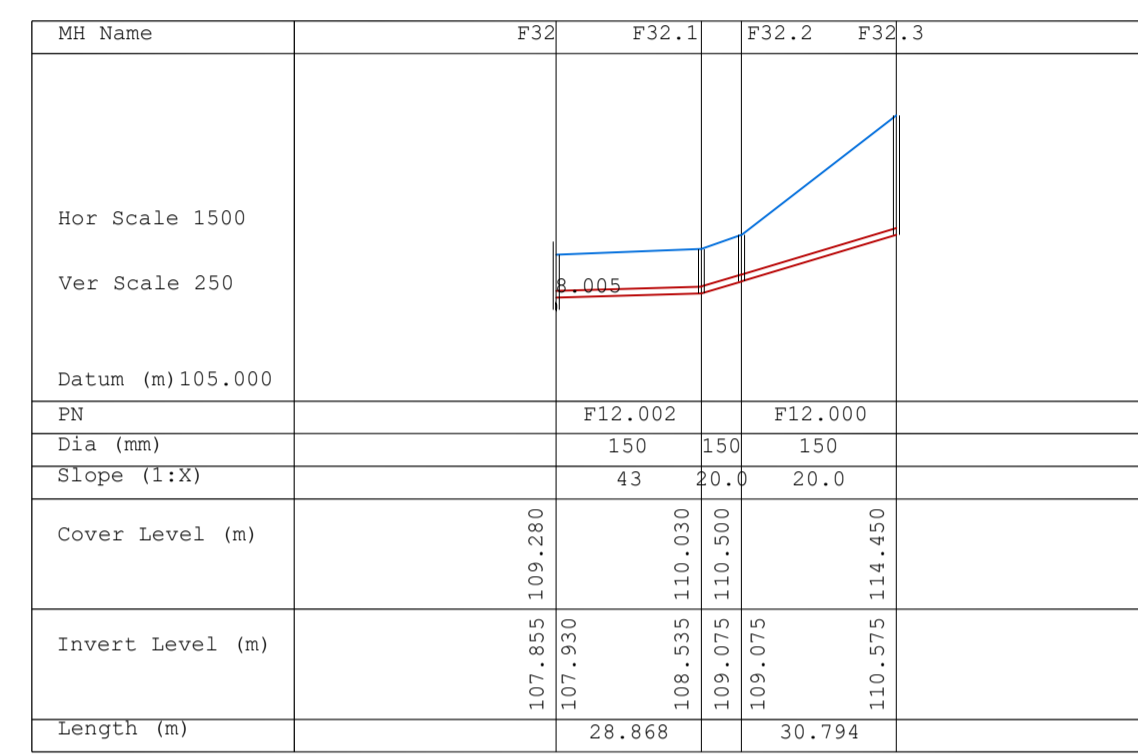
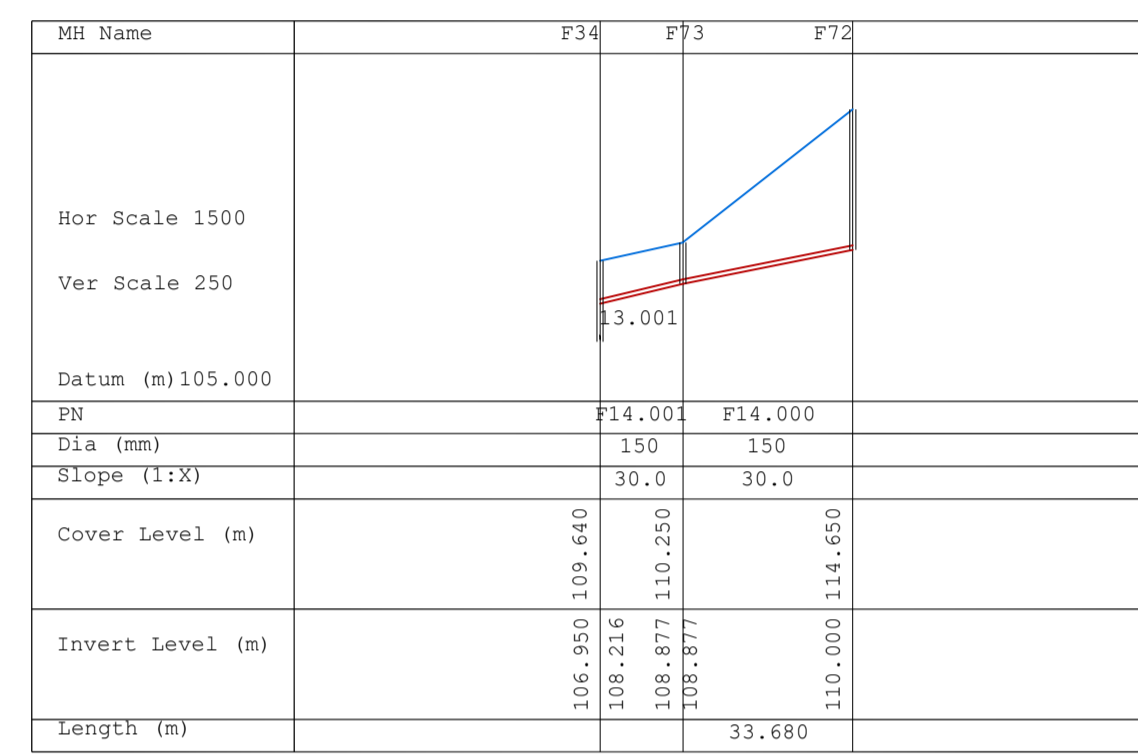
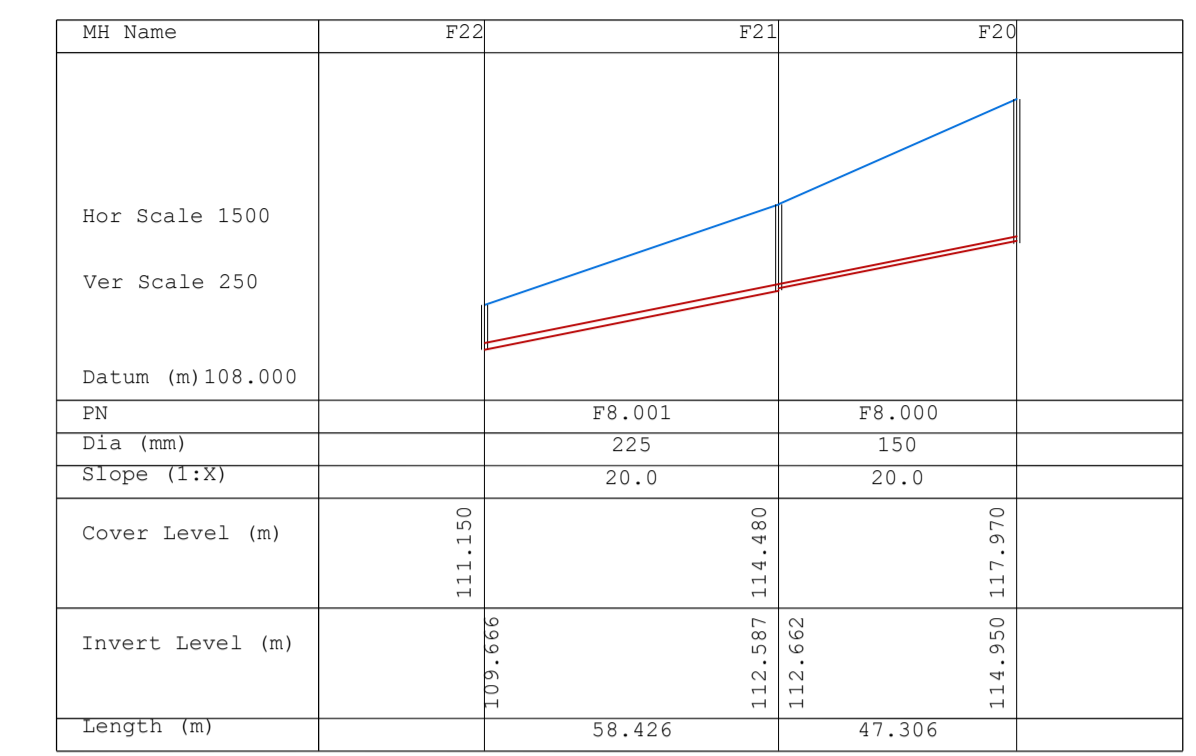
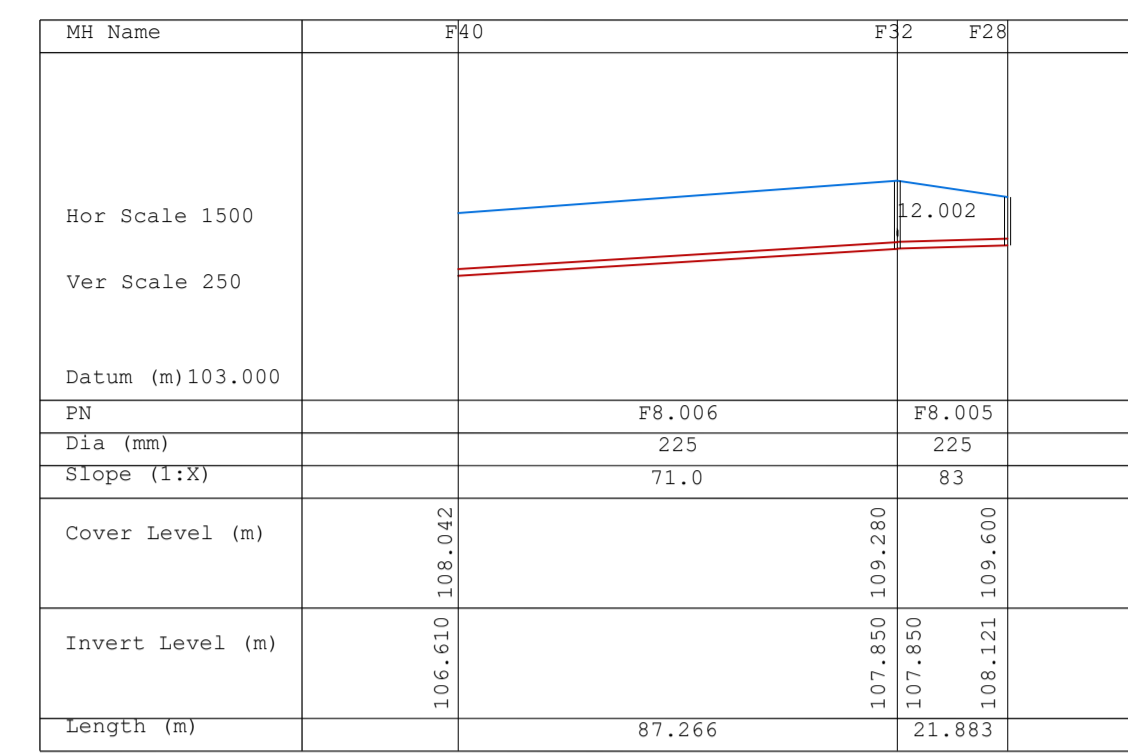
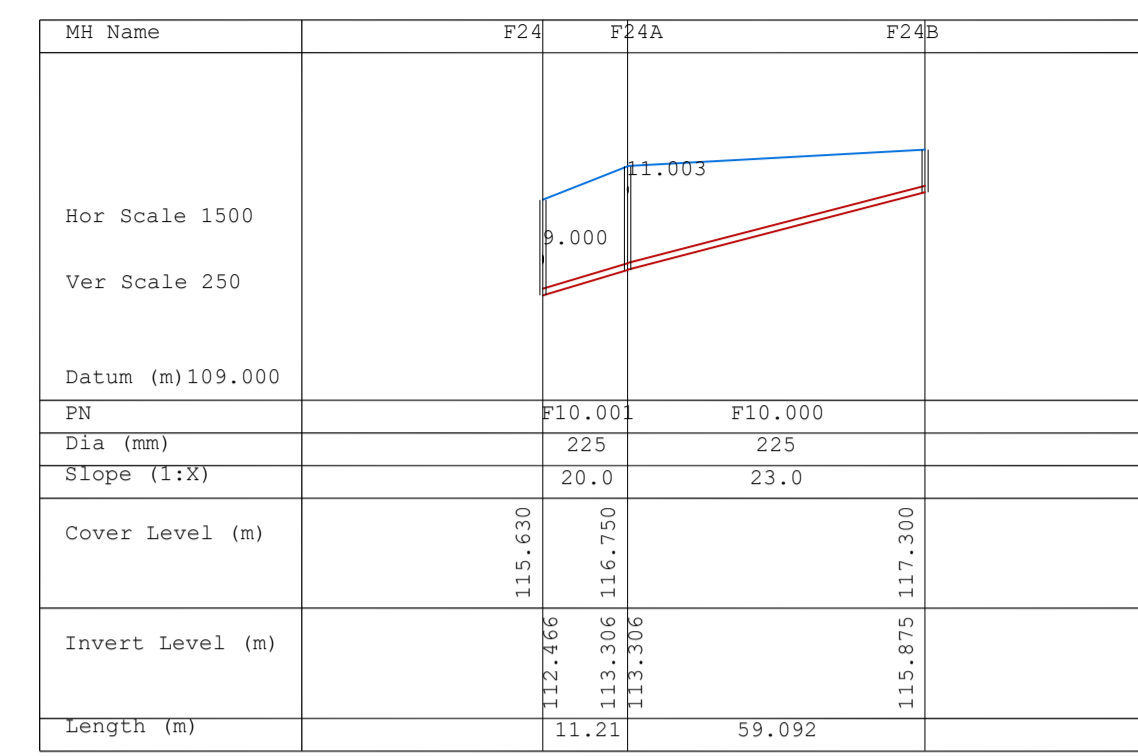
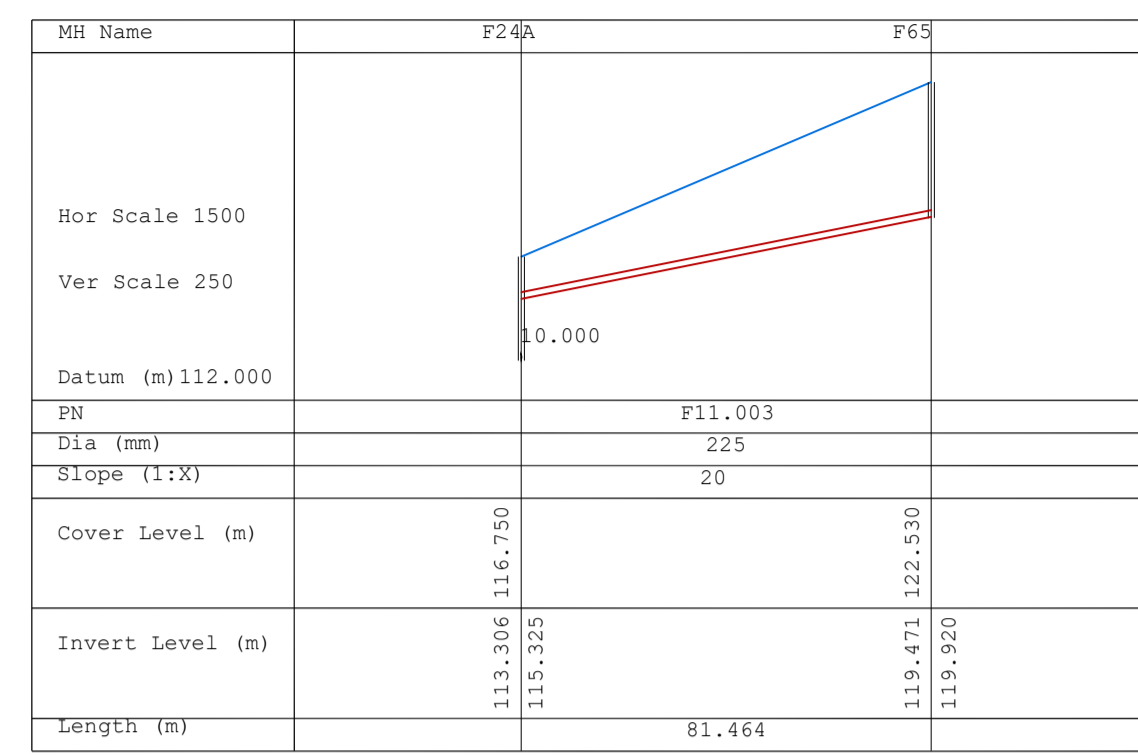
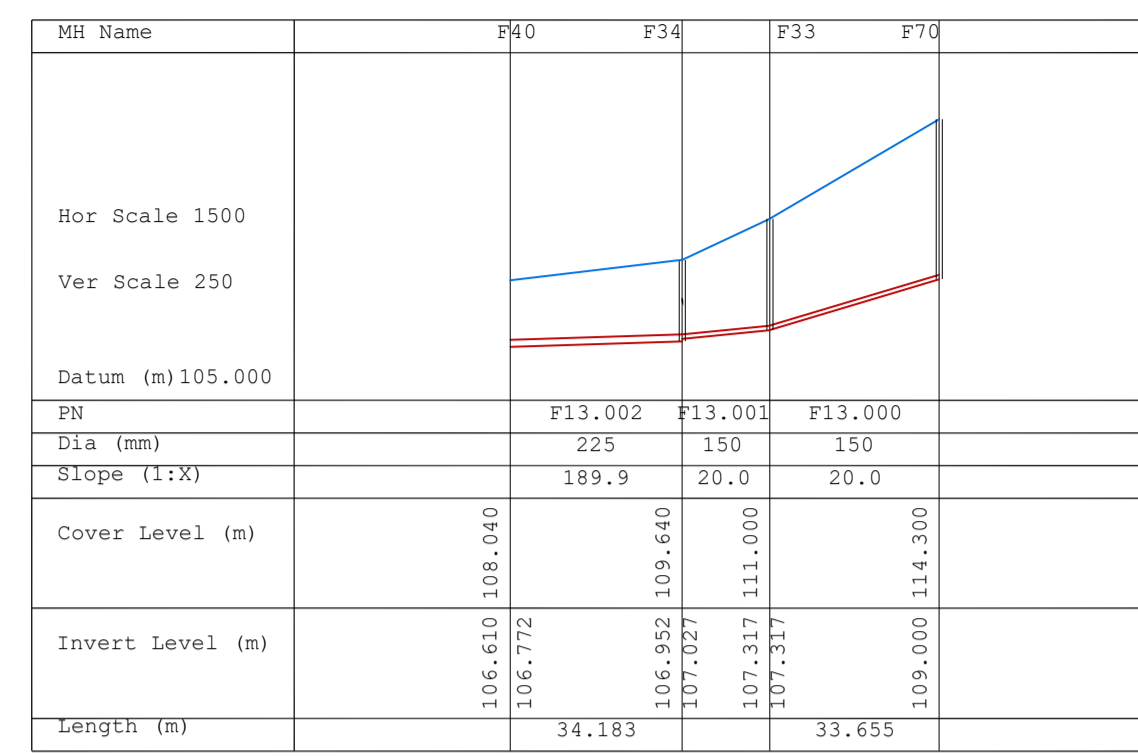
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ARCHITECT **CONNOLLY ARCHITECTS**
PROJECT **LANDS AT KILNAHUE & GOREY HILL, GOREY**

TITLE **PROPOSED DRAINAGE LAYOUT**
SHEET 5 OF 5

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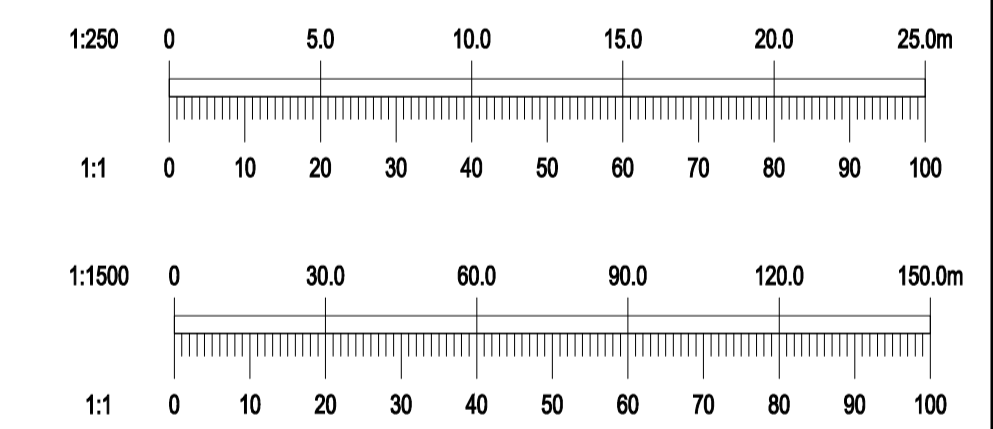
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LEGEND

- INDICATES PROPOSED GROUND LEVEL
- INDICATES PROPOSED uPVC 8N8 FOUL PIPE



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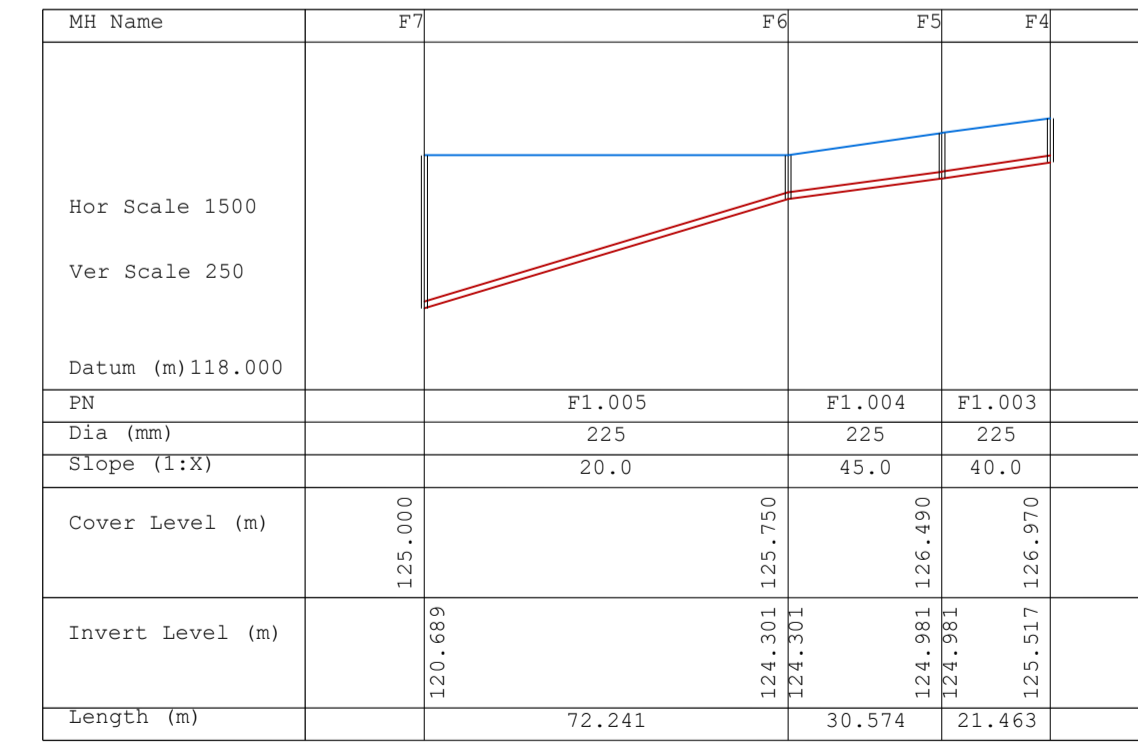
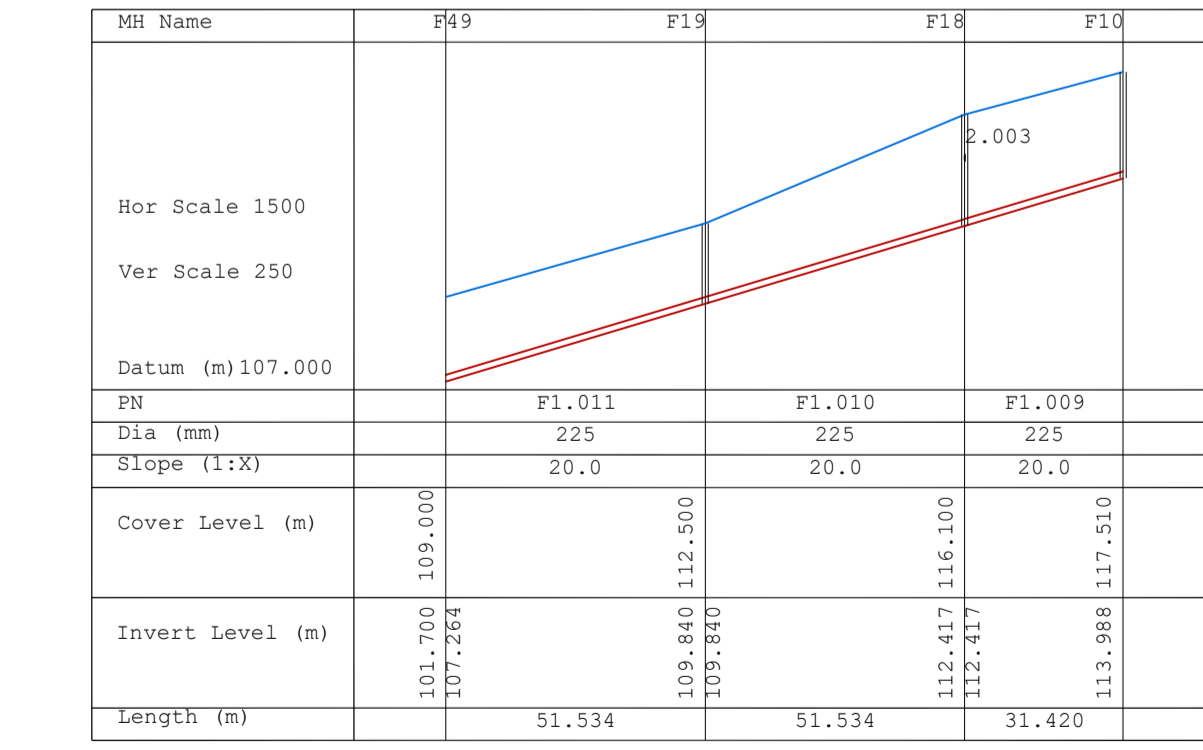
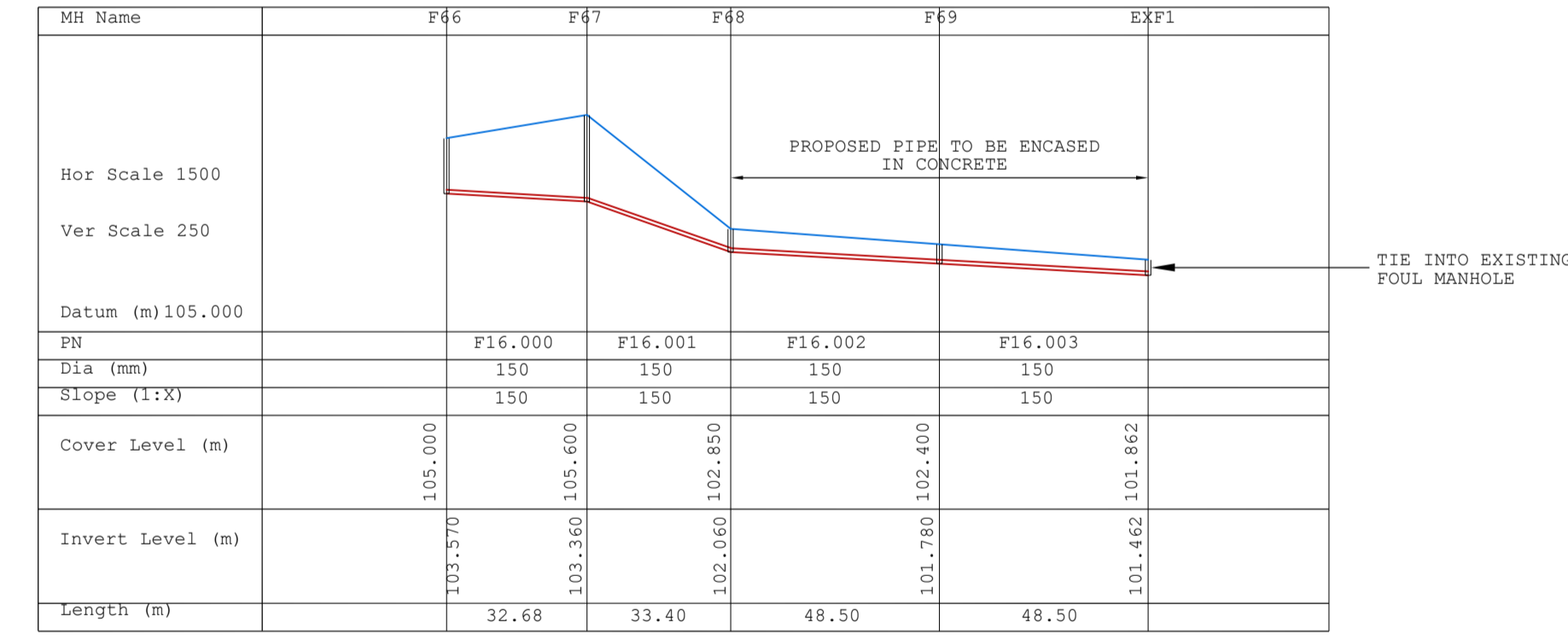
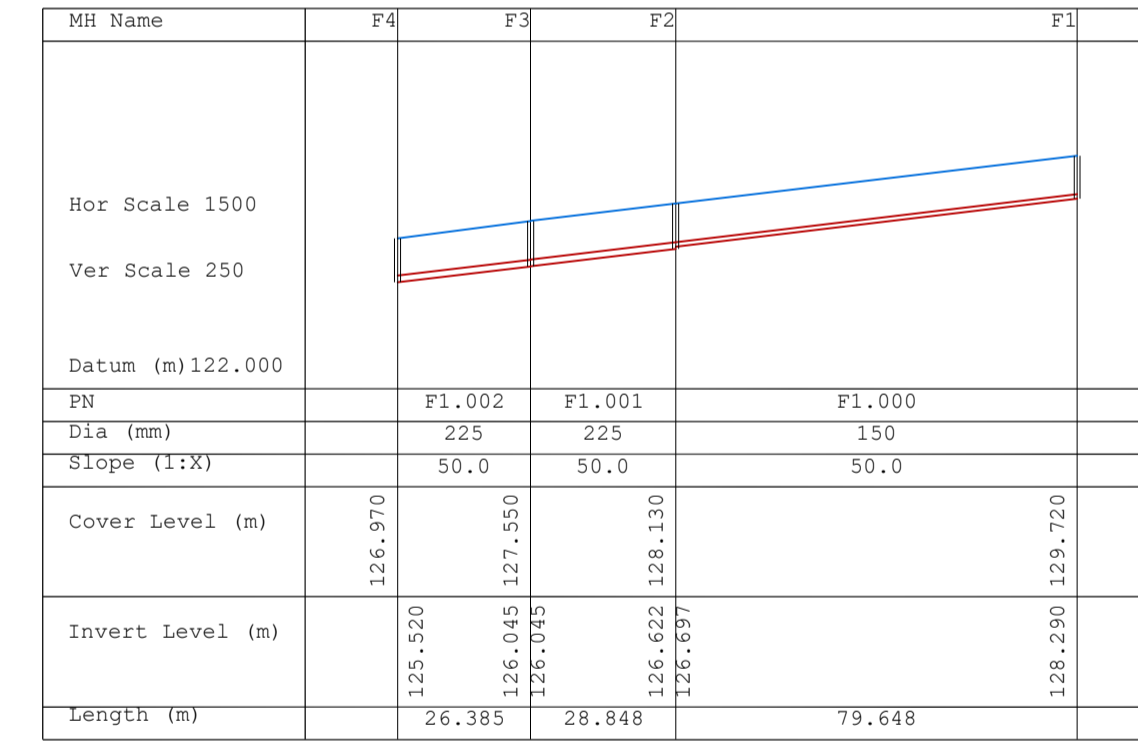
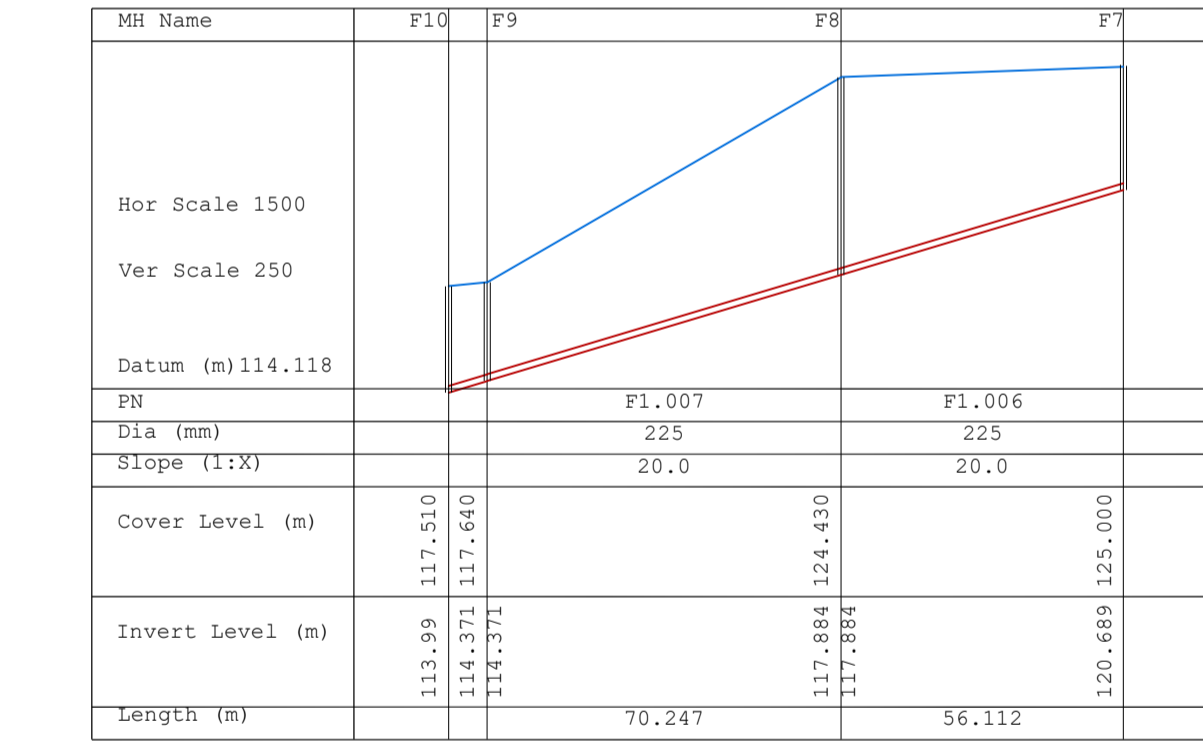
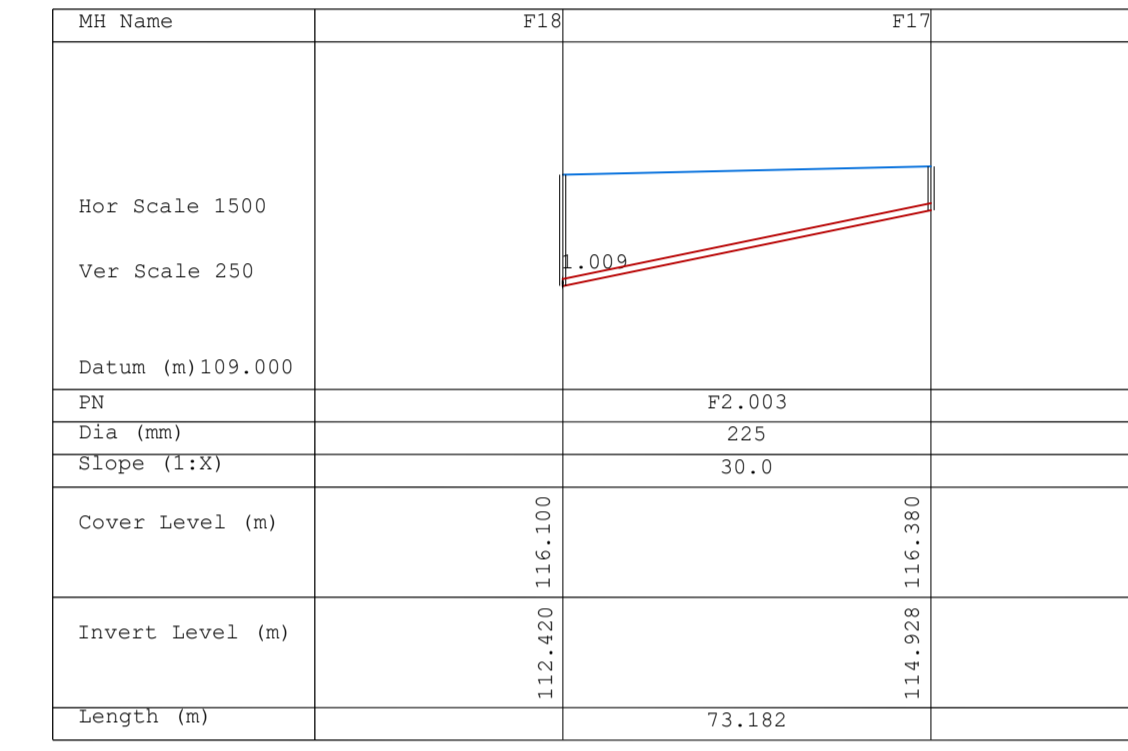
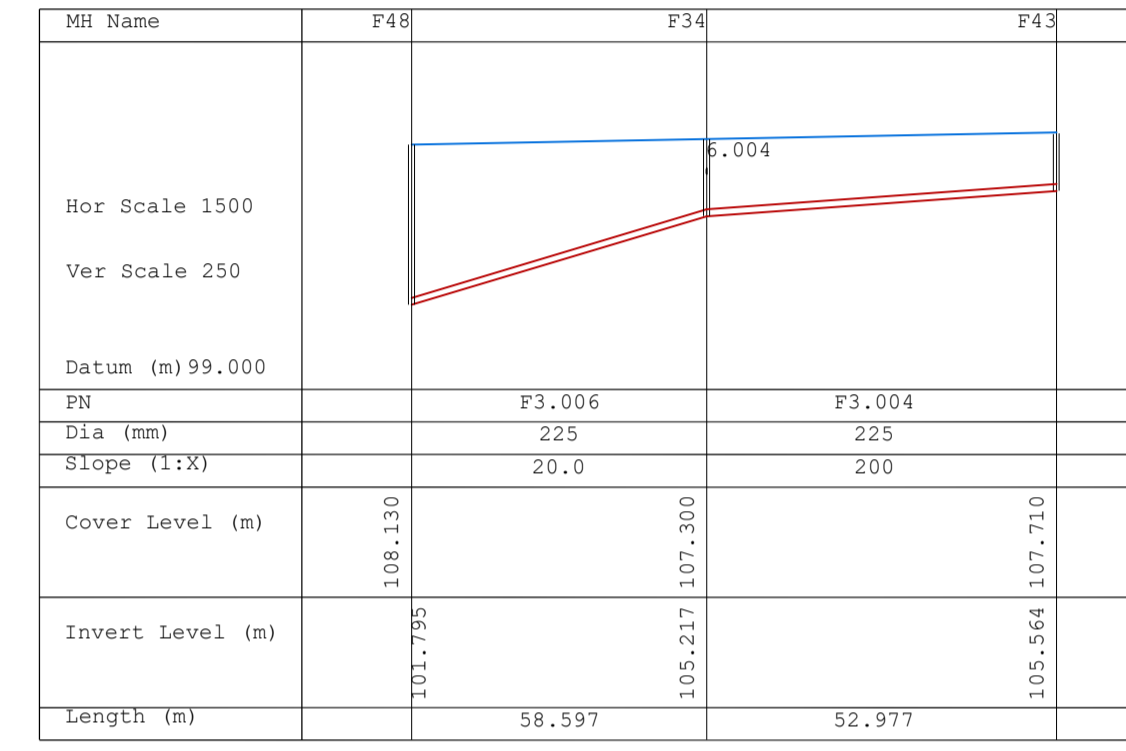
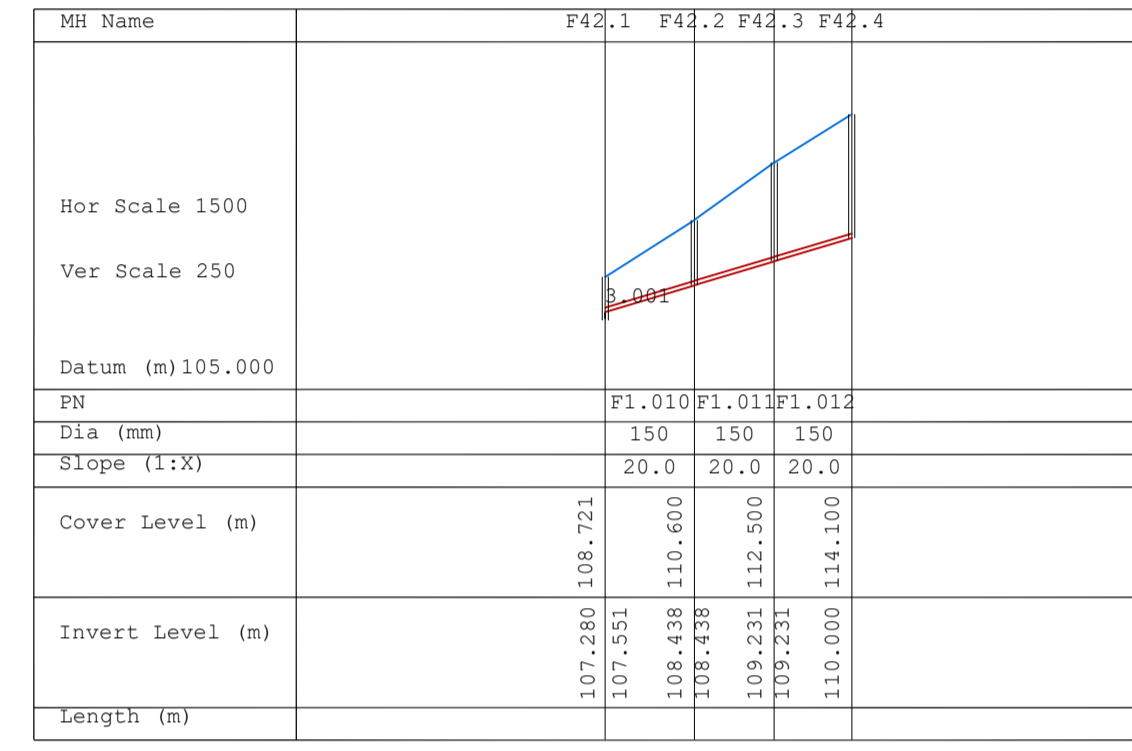
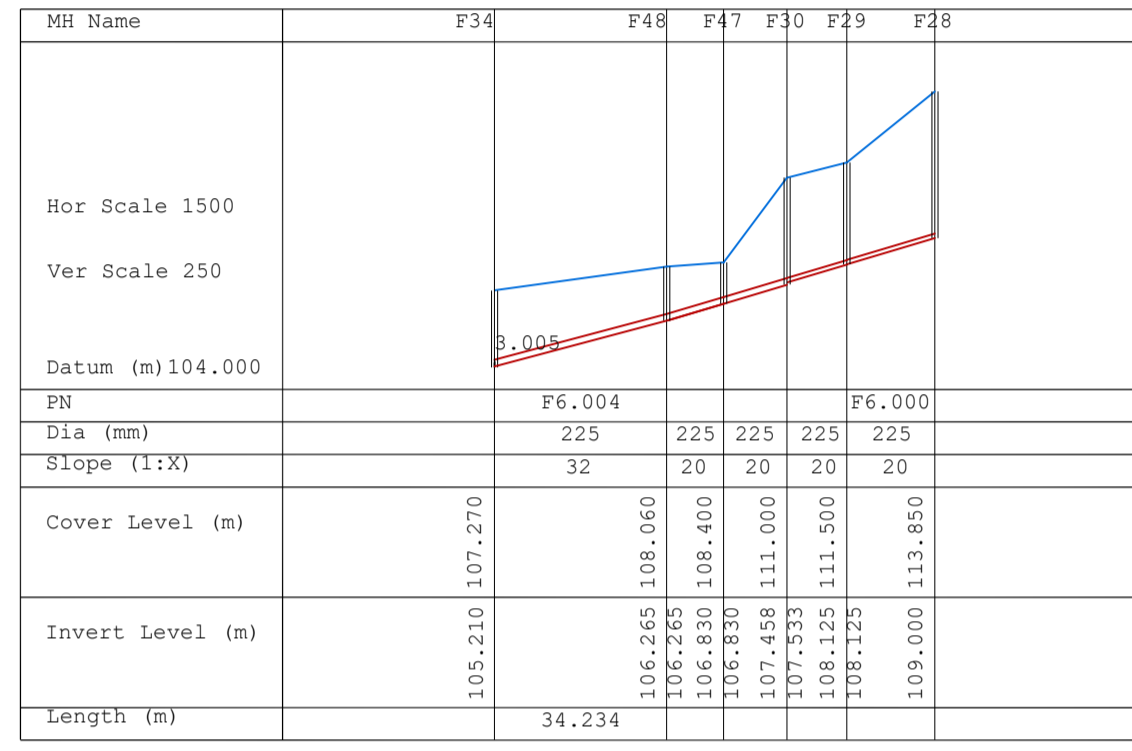
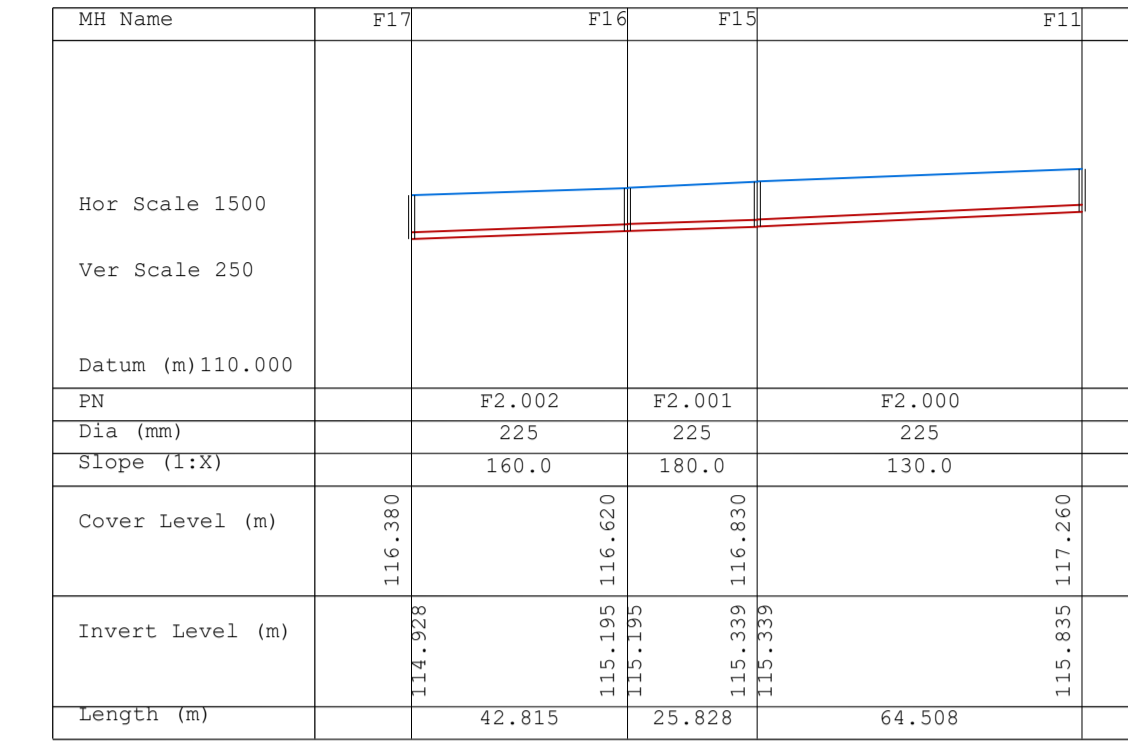
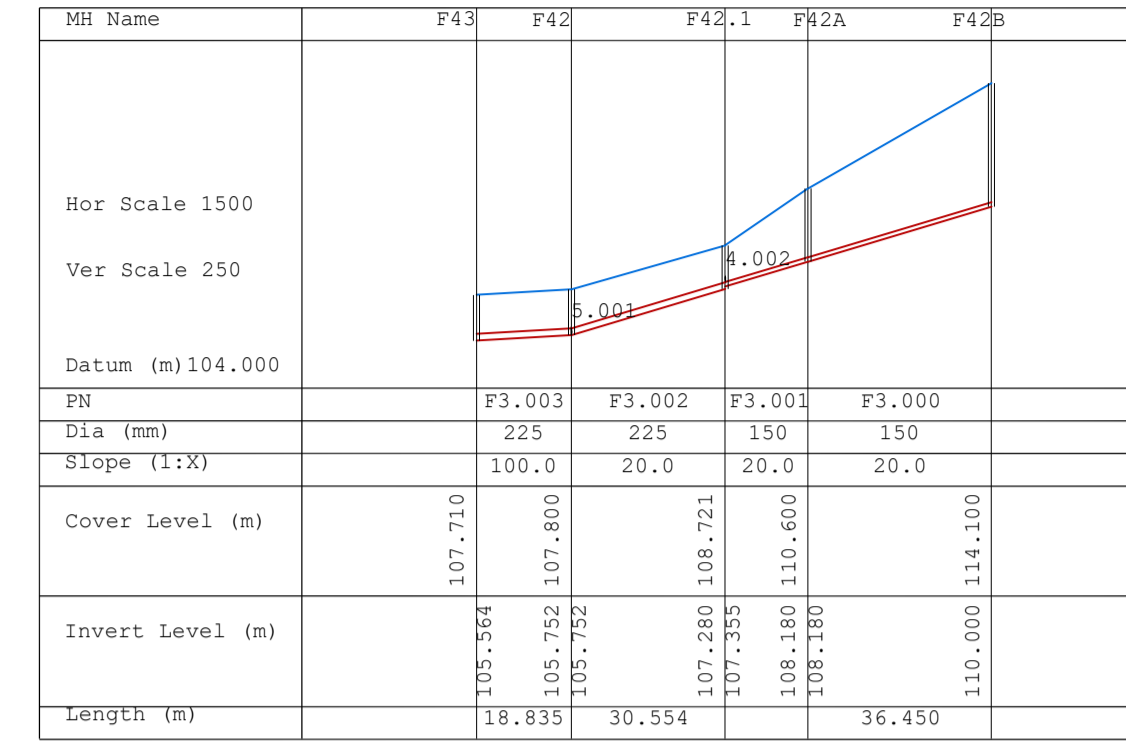
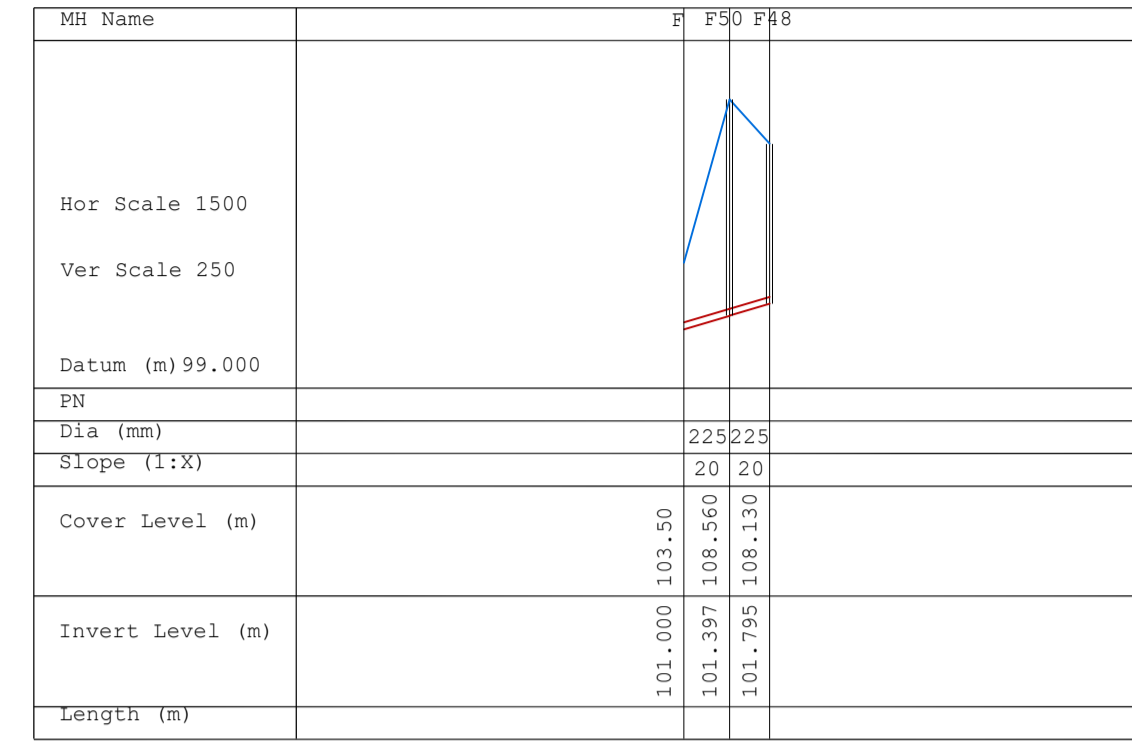
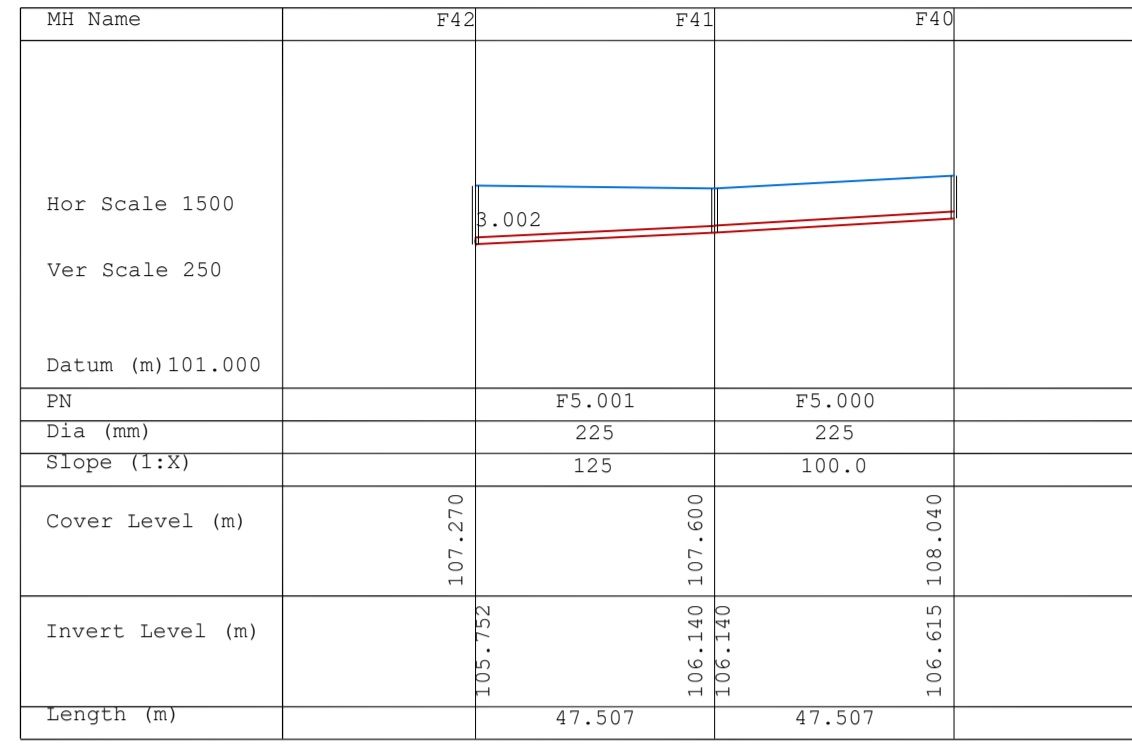
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Tel: (01) 664 8900 Fax: (01) 661 3618
Email: info@waterman-moylan.ie www.waterman-moylan.ie

CLIENT	GERARD GANNON PROPERTIES		
ARCHITECT	CONNOLLY ARCHITECTS		
PROJECT	LANDS AT KILNAHUE & GOREY HILL, GOREY		
TITLE	FOUL DRAINAGE LONGITUDINAL SECTIONS SHEET 1 OF 2		
DRAWN	DESIGNED	APPROVED	DATE
PJD	DA	MD	OCT '21
SCALE	JOB NO.	DRG. NO.	REVISION
1:250H, 1:1500H	13-119	P4220	

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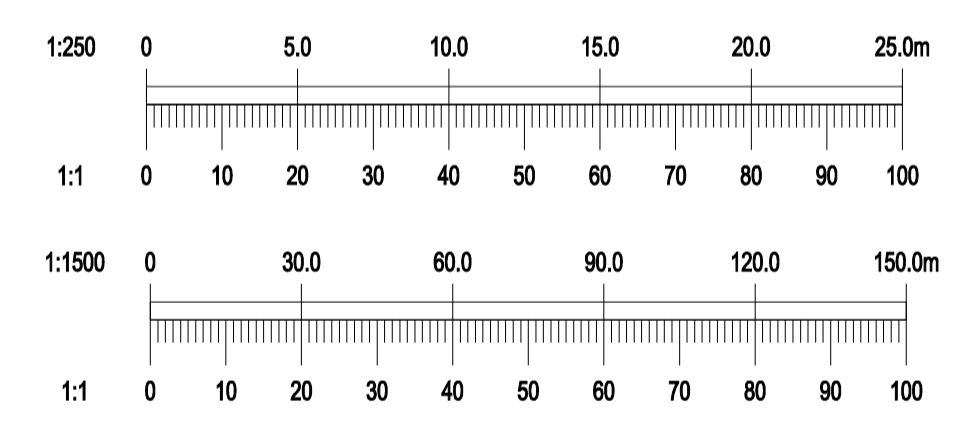
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LEGEND

———— INDICATES PROPOSED GROUND LEVEL

———— INDICATES PROPOSED uPVC SN8 FOUL PIPE



REV.	DATE	AMENDMENT	DRN	APPD

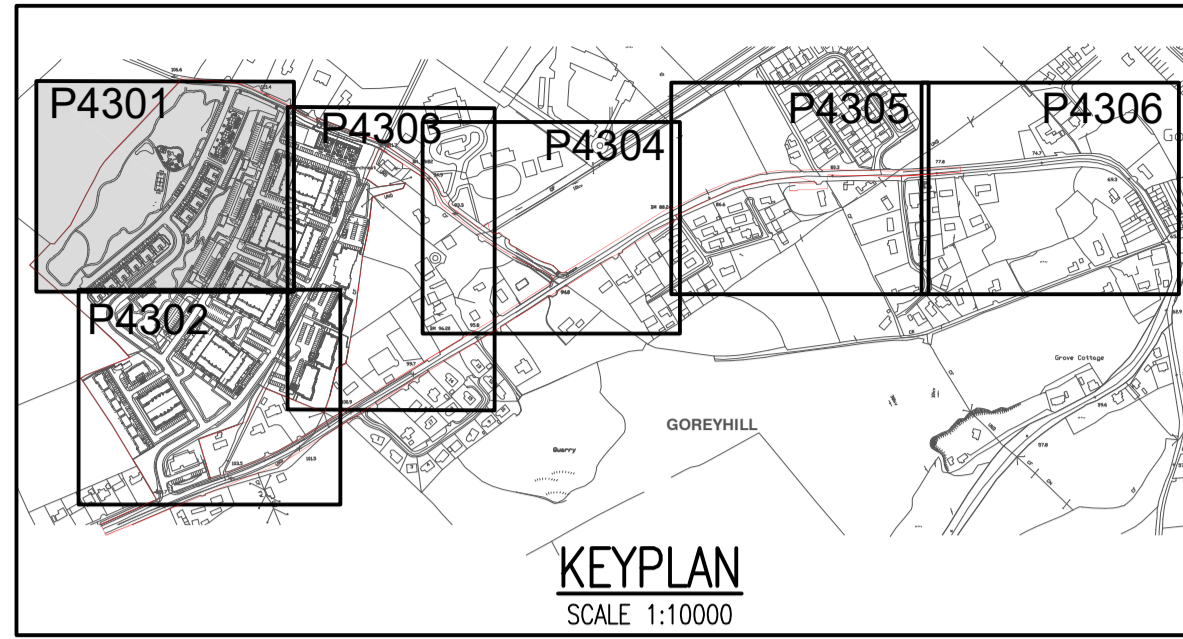
STATUS: **FOR PLANNING**
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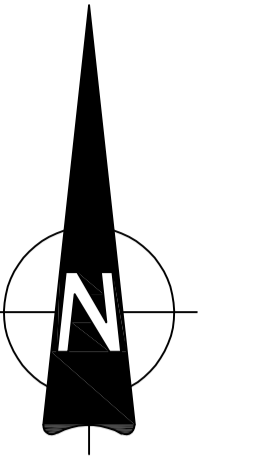
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CLIENT	GERARD GANNON PROPERTIES
ARCHITECT	CONNOLLY ARCHITECTS
PROJECT	LANDS AT KILNAHUE & GOREY HILL, GOREY
TITLE	FOUL DRAINAGE LONGITUDINAL SECTIONS SHEET 2 OF 2

DRAWN	DESIGNED	APPROVED	DATE
PJD	DA	MD	OCT '21
SCALE	JOB NO.	DRG. NO.	REVISION
1:250V, 1:1500H	13-119	P4221	

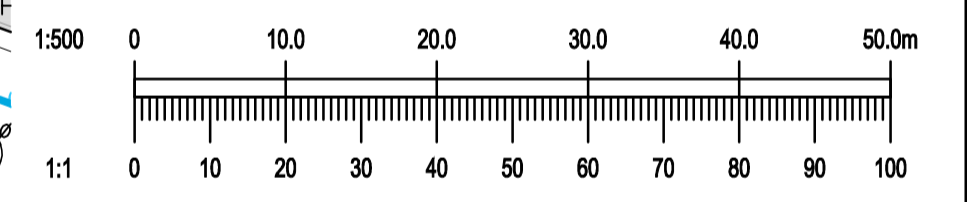


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LEGEND:

	PROPOSED 110mm HDPE SDR17 WATERMAIN WITH PIPE SIZE
	PROPOSED 160mm HDPE SDR17 WATERMAIN WITH PIPE SIZE
	PROPOSED 150mm HDPE SDR17 WATERMAIN WITH PIPE SIZE
	EXISTING WATERMAIN WITH PIPE SIZE
	PROPOSED SLUICE VALVE
	PROPOSED HYDRANT
	PROPOSED SCOUR VALVE
	PROPOSED AIR VALVE
	PROPOSED NON-RETURN VALVE
	PROPOSED BULK WATER METER TO IRISH WATER DETAILS
	SURFACE WATER MANHOLE
	TYPICAL SCHEMATIC CONNECTION OF OFFLINE SCOUR VALVE
	PROPOSED BOUNDARY BOX AND CONNECTION
	ROAD LOW POINT
	ROAD HIGH POINT



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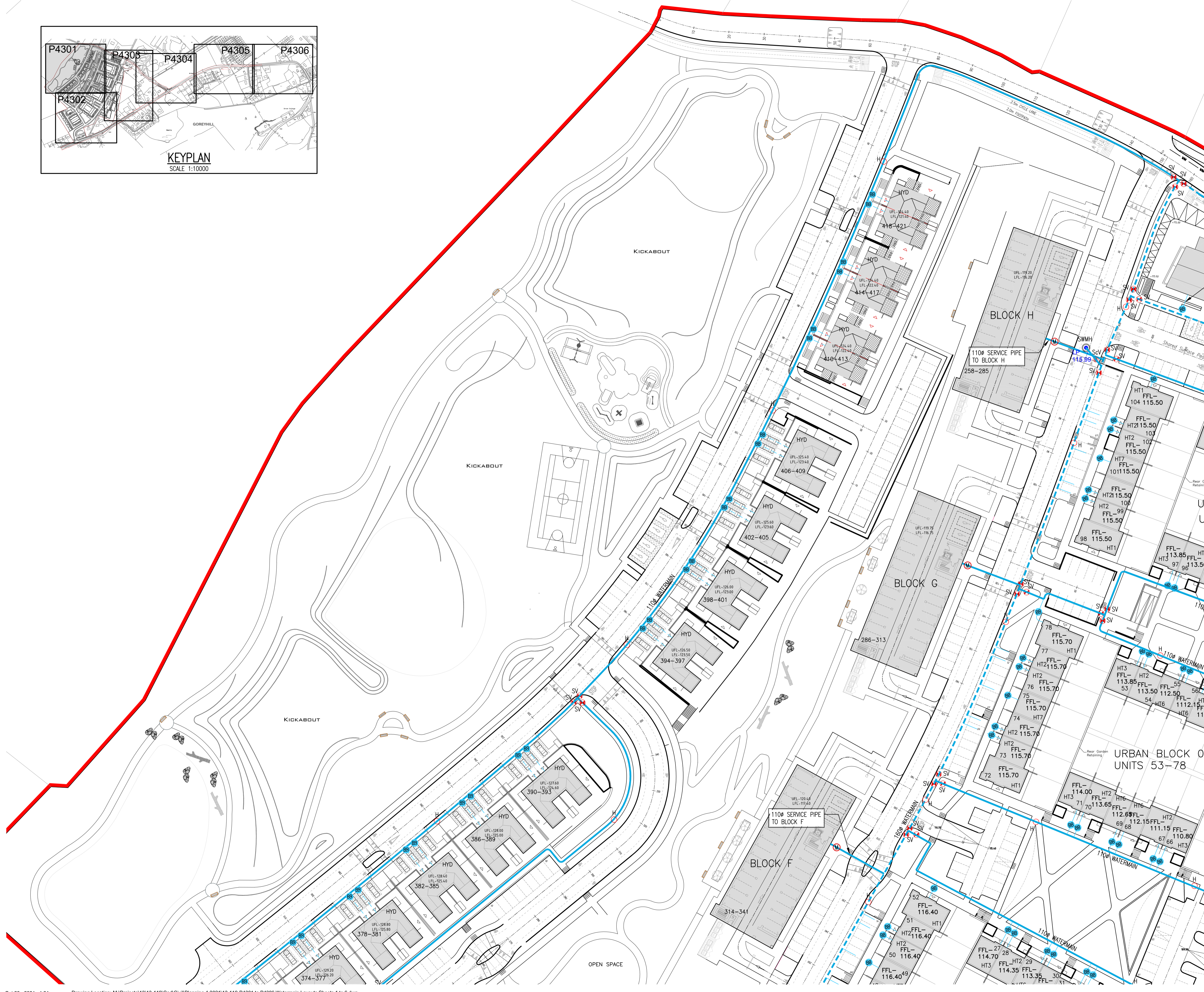
REV. DATE	AMENDMENT	DRN	APPD

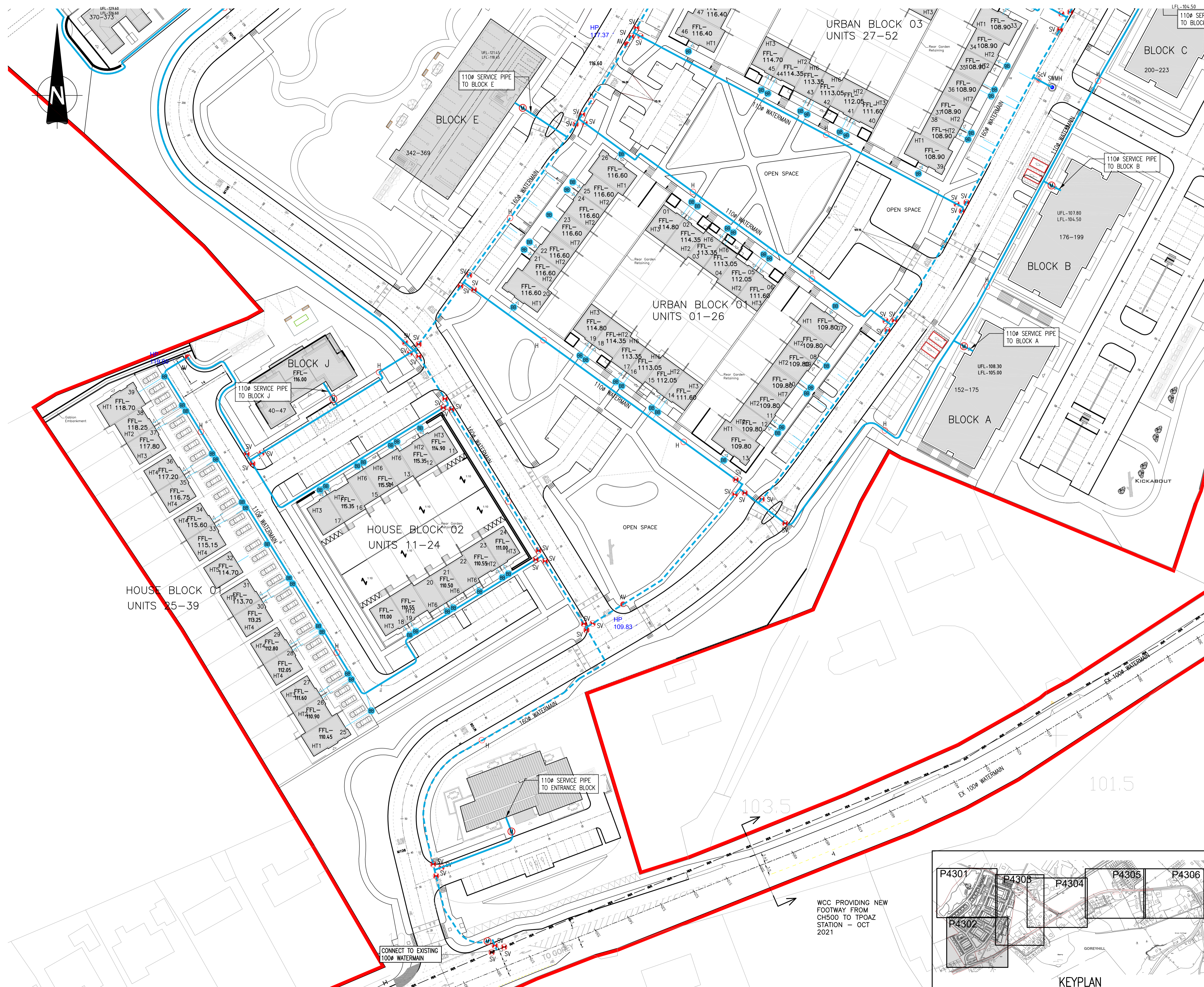
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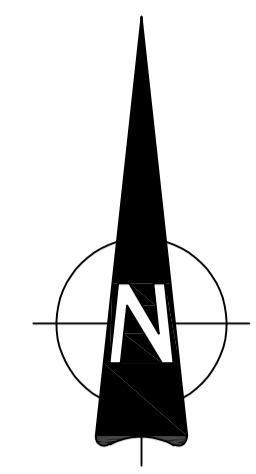
CLIENT GERARD GANNON PROPERTIES
ARCHITECT CONNOLLY ARCHITECTS
PROJECT LANDS AT KILNAHUE & GOREY HILL, GOREY,
TITLE PROPOSED WATERMAIN LAYOUT SHEET 1 OF 6

DRAWN PJD	DESIGNED PJD	APPROVED	DATE AUG 2021
SCALE 1:500 @A1	JOB NO. 13-119	DRG. NO. P4301	REVISION



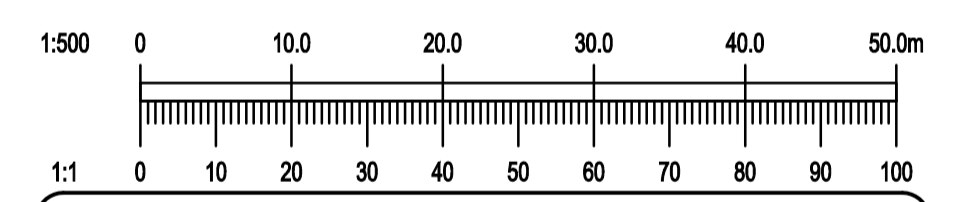


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LEGEND:

- 110mm ϕ PROPOSED 110 ϕ HDPE SDR17 WATERMAIN WITH PIPE SIZE
- 160mm ϕ PROPOSED 160 ϕ HDPE SDR17 WATERMAIN WITH PIPE SIZE
- 160mm ϕ PROPOSED 150 ϕ HDPE SDR17 WATERMAIN WITH PIPE SIZE
- XXXmm ϕ EXISTING WATERMAIN WITH PIPE SIZE
- SV PROPOSED SLUICE VALVE
- H PROPOSED HYDRANT
- ScV PROPOSED SCOUR VALVE
- AV PROPOSED AIR VALVE
- NRV PROPOSED NON-RETURN VALVE
- M PROPOSED BULK WATER METER TO IRISH WATER DETAILS
- SWMH SURFACE WATER MANHOLE
- ScV NRV SWMH TYPICAL SCHEMATIC CONNECTION OF OFFLINE SCOUR VALVE
- BB PROPOSED BOUNDARY BOX AND CONNECTION
- LP ROAD LOW POINT
- HP ROAD HIGH POINT



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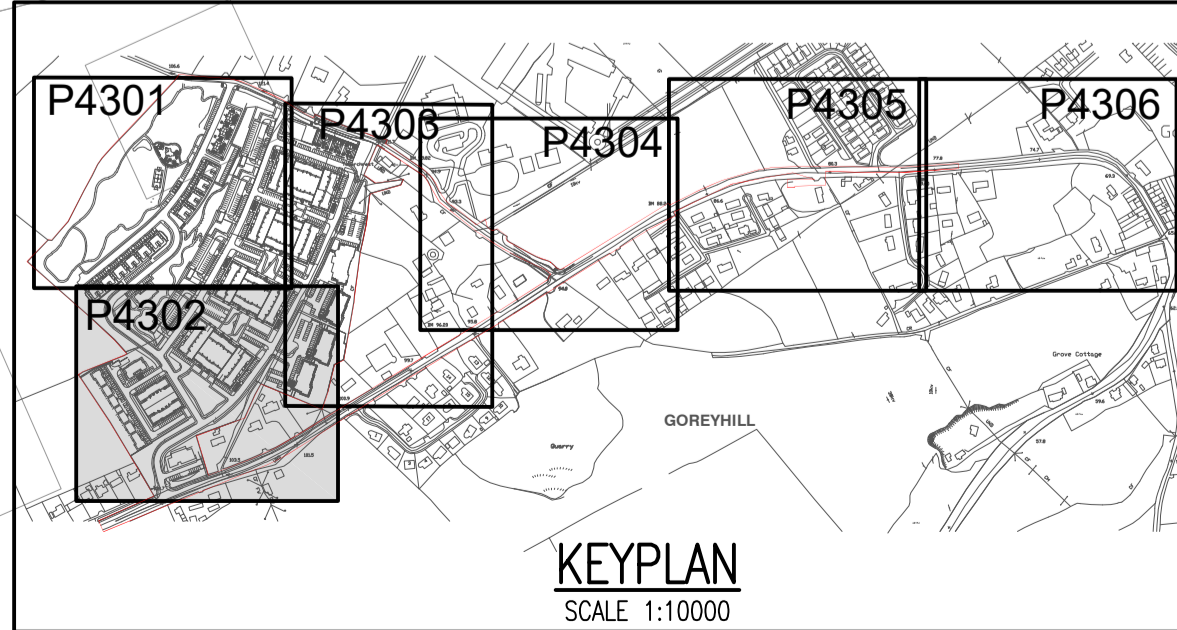
REV.	DATE	AMENDMENT	DRN	APPD

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CLIENT GERARD GANNON PROPERTIES
ARCHITECT CONNOLLY ARCHITECTS
PROJECT LANDS AT KILNAHUE & GOREY HILL, GOREY
TITLE PROPOSED WATERMAIN LAYOUT SHEET 2 OF 6

DRAWN PJD	DESIGNED DA	APPROVED	DATE AUG 2021
SCALE 1:500 @A1	JOB NO. 13-119	DRG. NO. P4302	REVISION

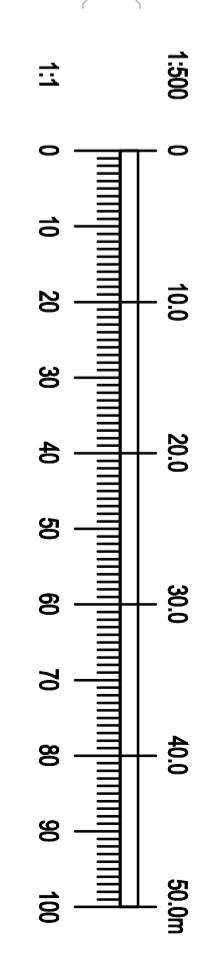
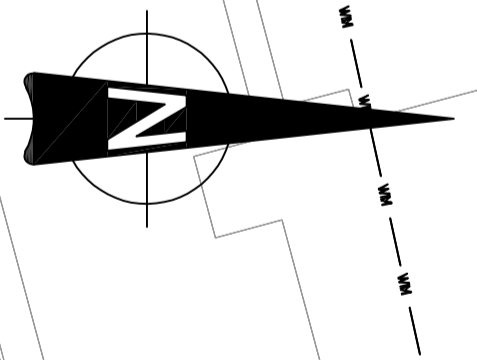


WCC PROVIDING NEW FOOTWAY FROM CH500 TO TPOAZ STATION - OCT 2021

NOTES:
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LEGEND:

	PROPOSED 110Ø HOPE SRR17 WATERMAIN WITH PIPE SIZE
	PROPOSED 160Ø HOPE SRR17 WATERMAIN WITH PIPE SIZE
	PROPOSED 150Ø HOPE SRR17 WATERMAIN WITH PIPE SIZE
	EXISTING WATERMAIN WITH PIPE SIZE
	PROPOSED SLUICE VALVE
	PROPOSED HYDRANT
	PROPOSED SCOUR VALVE
	PROPOSED AIR VALVE
	PROPOSED NON-RETURN VALVE
	PROPOSED BULK WATER METER TO IRISH WATER DETAILS
	SURFACE WATER MANHOLE
	TYPICAL SCHEMATIC CONNECTION OF OFFLINE SCOUR VALVE
	PROPOSED BOUNDARY BOX AND CONNECTION
	ROAD LOW POINT
	ROAD HIGH POINT
	WATERMAIN
	SEWER
	SMWH
	LP
	HP



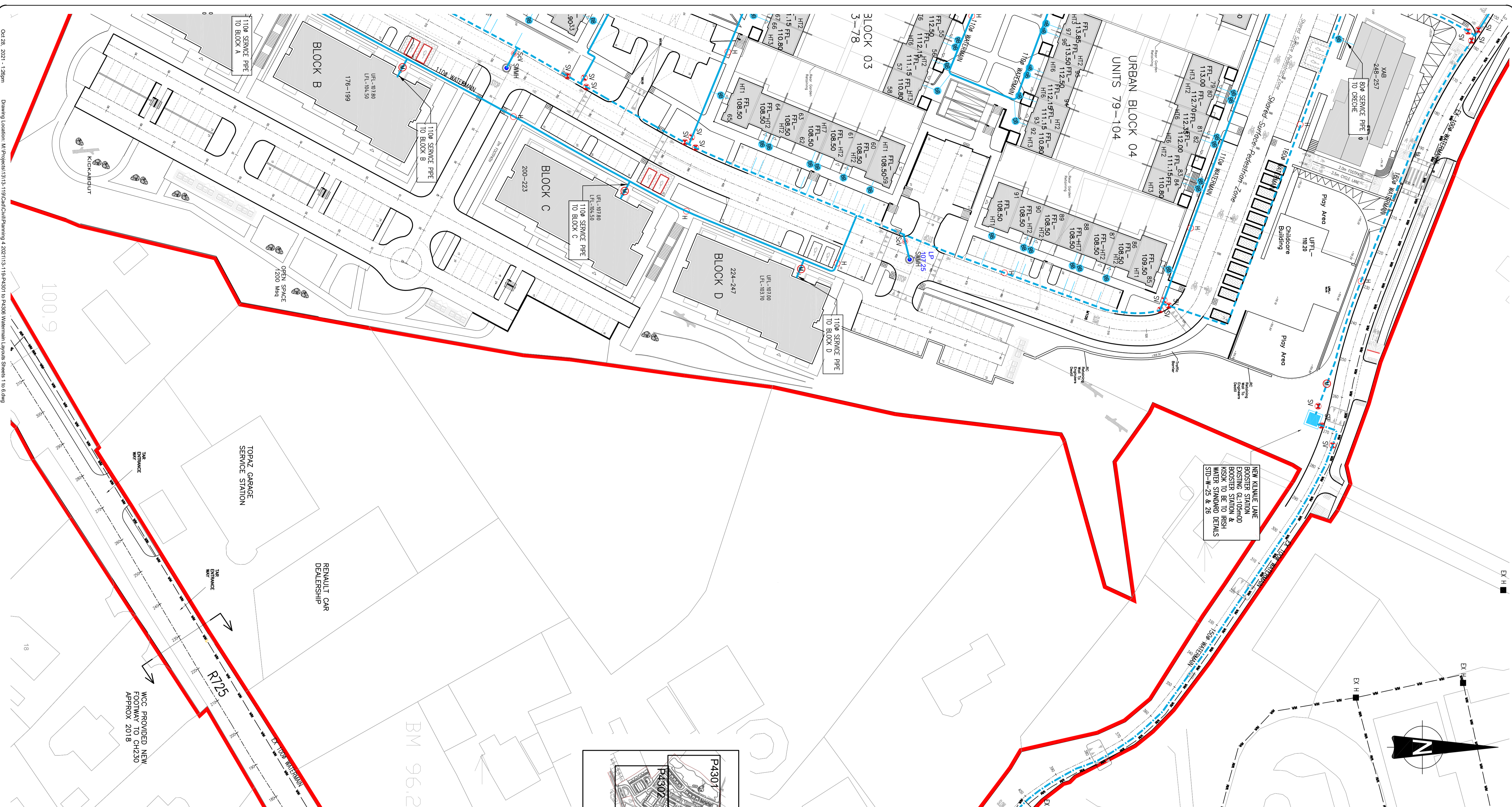
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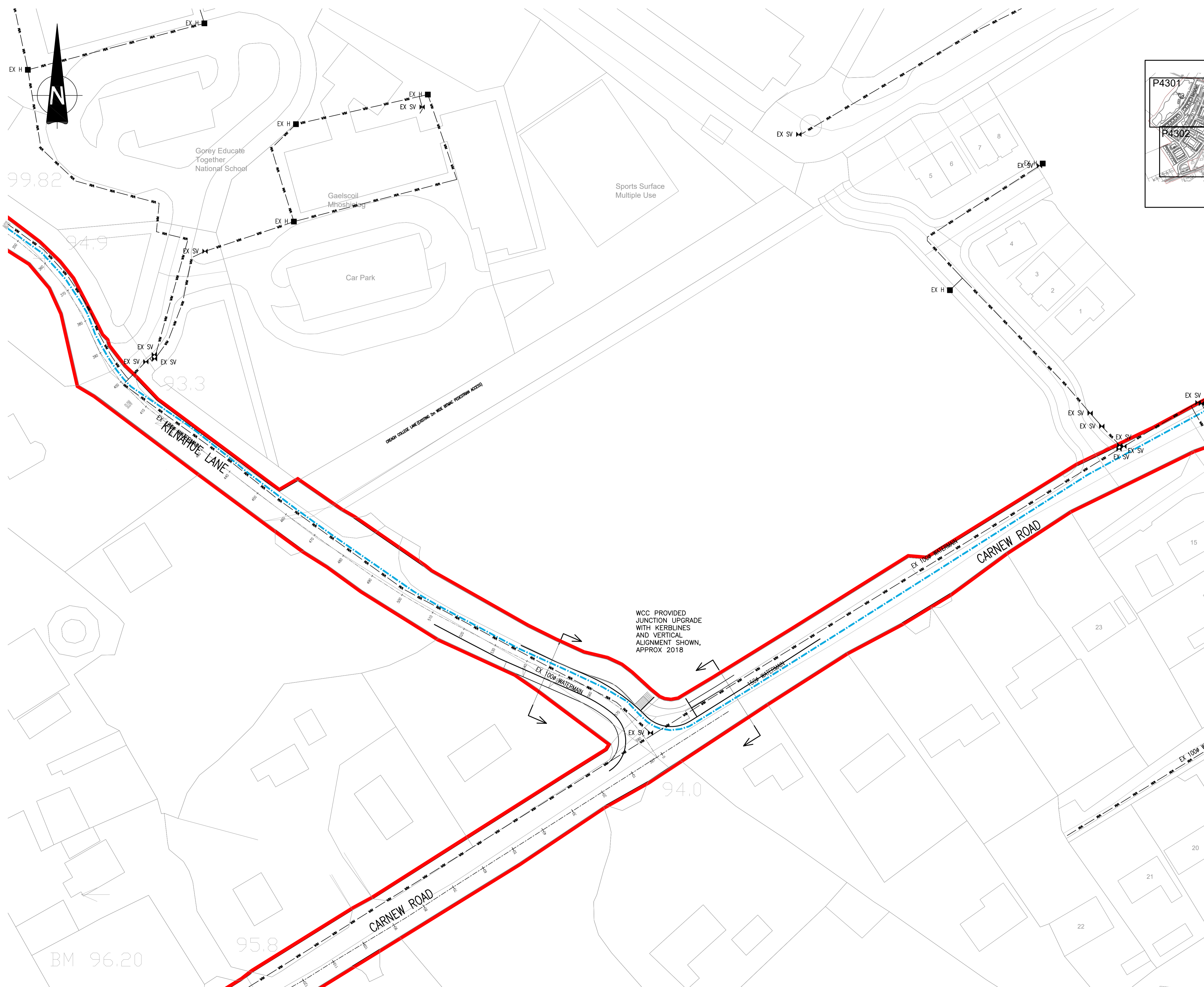
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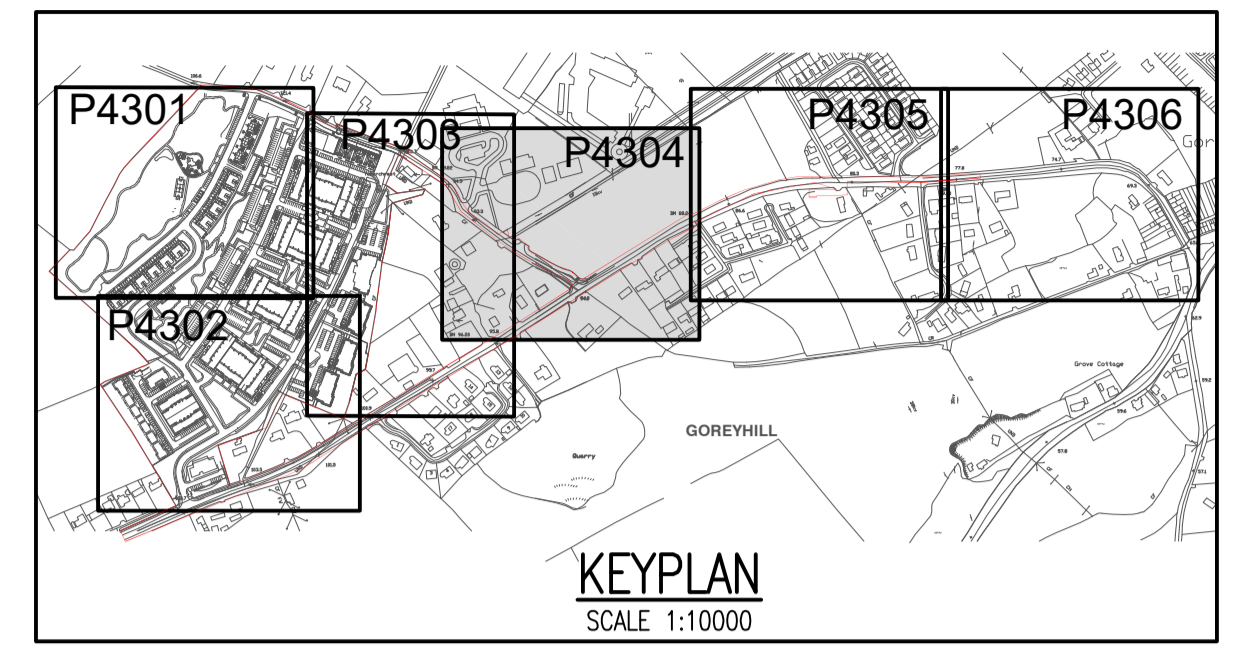
PROPOSED WATERMAIN LAYOUT
 SHEET 3 OF 6

DESIGNED	APPROVED	DATE
RJD	RJD	AUG 2021
JOB NO. 13-119	DRG. NO. PA303	REVISION
SCALE 1:500 @ A1		



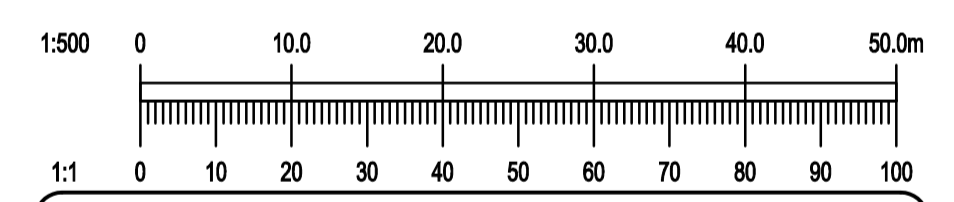


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LEGEND:

	EXISTING WATERMAIN WITH PIPE SIZE
	PROPOSED 150Ø WATERMAIN
	PROPOSED 200Ø WATERMAIN



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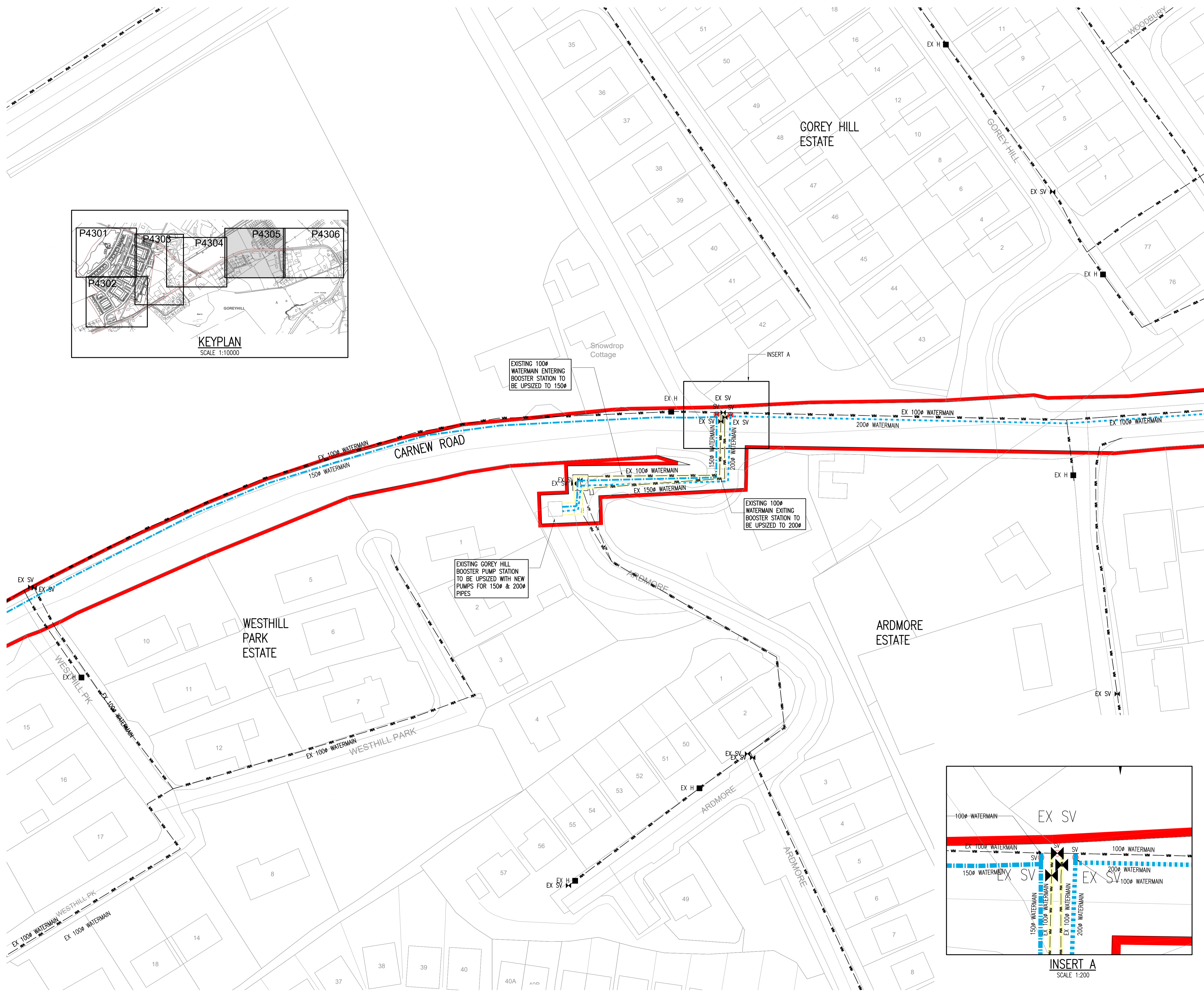
CLIENT **GERARD GANNON PROPERTIES**
ARCHITECT **CONNOLLY ARCHITECTS**

PROJECT
LANDS AT KILNAHUE & GOREY HILL, GOREY

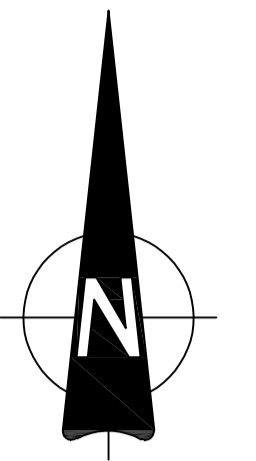
TITLE
**PROPOSED WATERMAIN LAYOUT
SHEET 4 OF 6**

DRAWN PJD	DESIGNED DA	APPROVED	DATE AUG 2021
SCALE 1:500 @A1	JOB NO. 13-119	DRG. NO. P4304	REVISION

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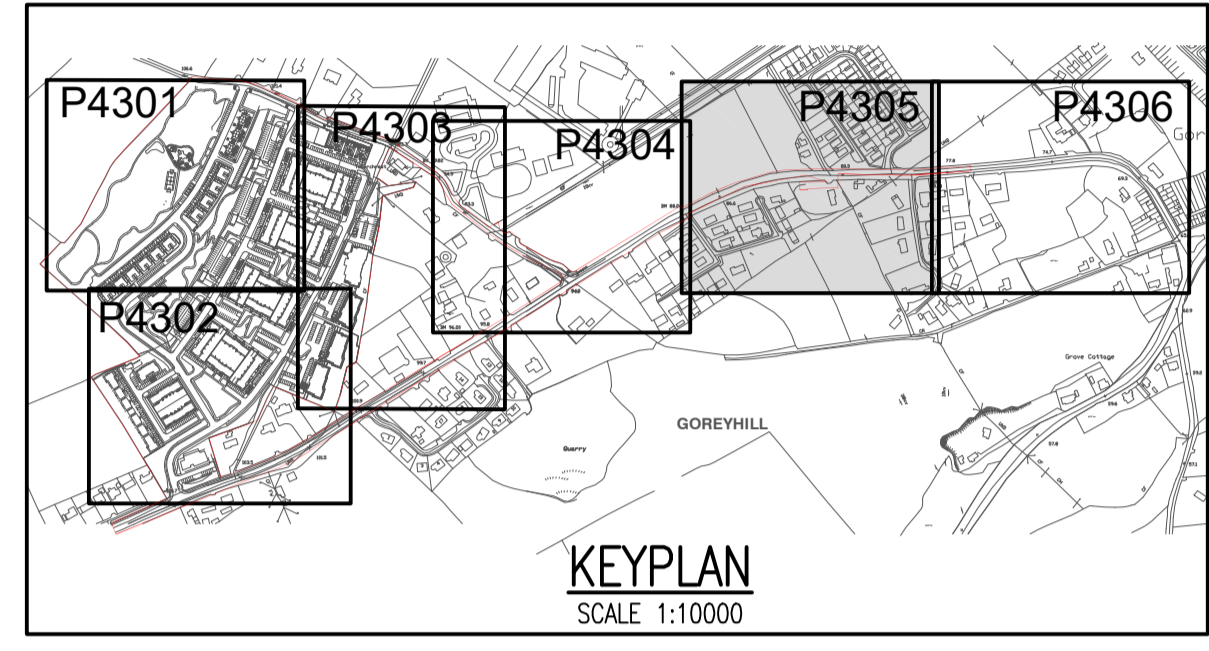


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LEGEND:

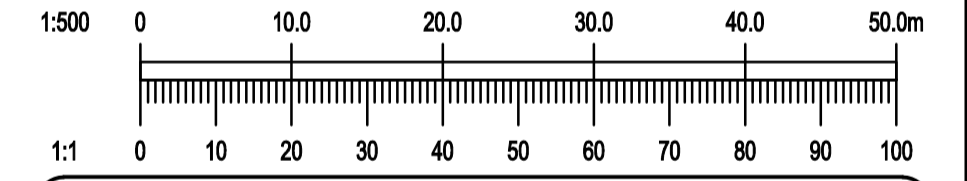
- XXXmm ϕ --- EXISTING WATERMAIN WITH PIPE SIZE
- XXXmm ϕ --- EXISTING WATERMAIN ENTERING AND EXISTING BOOSTER STATION TO BE DECOMMISSIONED ONCE WATERMAIN HAS BEEN UPSIZED
- 150mm ϕ --- PROPOSED 150 ϕ WATERMAIN
- 200mm ϕ --- PROPOSED 200 ϕ WATERMAIN



EXISTING 100 ϕ WATERMAIN ENTERING BOOSTER STATION TO BE UPSIZED TO 150 ϕ

EXISTING 100 ϕ WATERMAIN EXITING BOOSTER STATION TO BE UPSIZED TO 200 ϕ

EXISTING GOREY HILL BOOSTER PUMP STATION TO BE UPSIZED WITH NEW PUMPS FOR 150 ϕ & 200 ϕ PIPES



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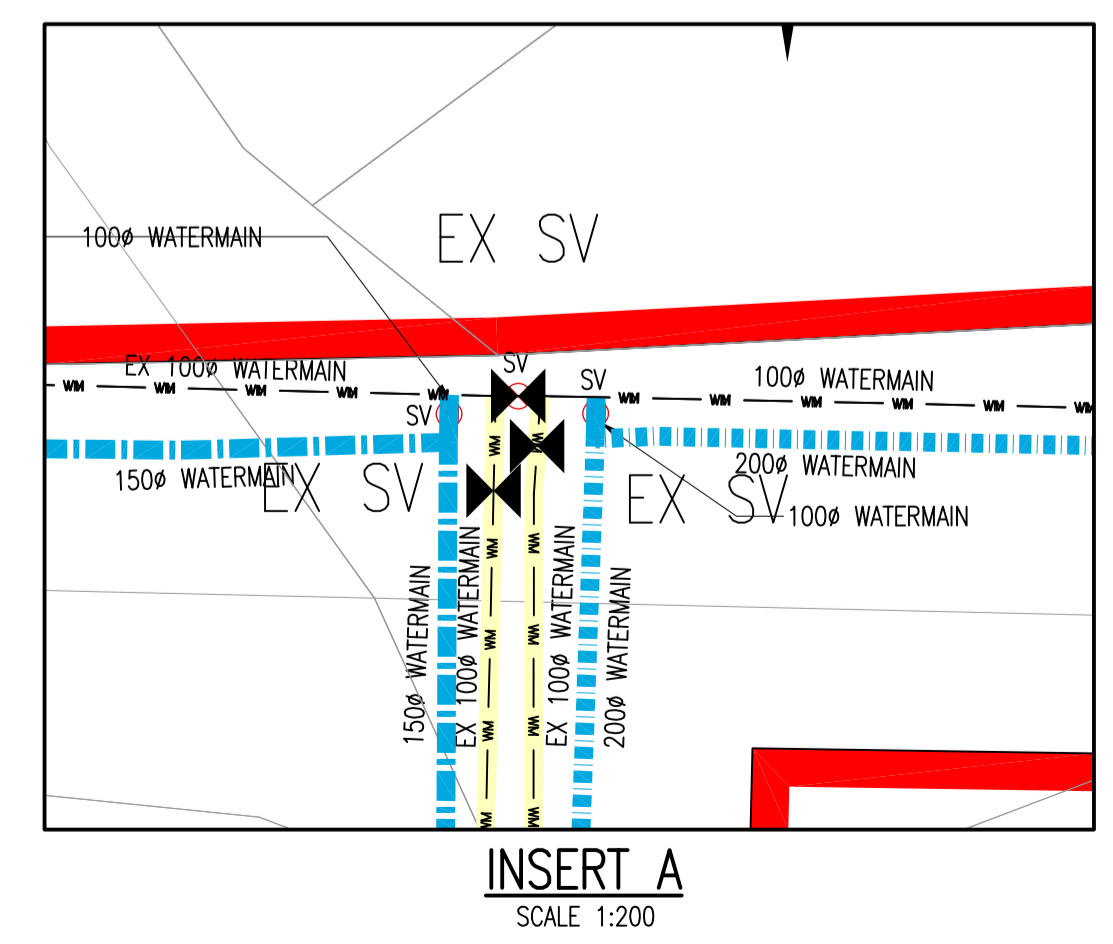
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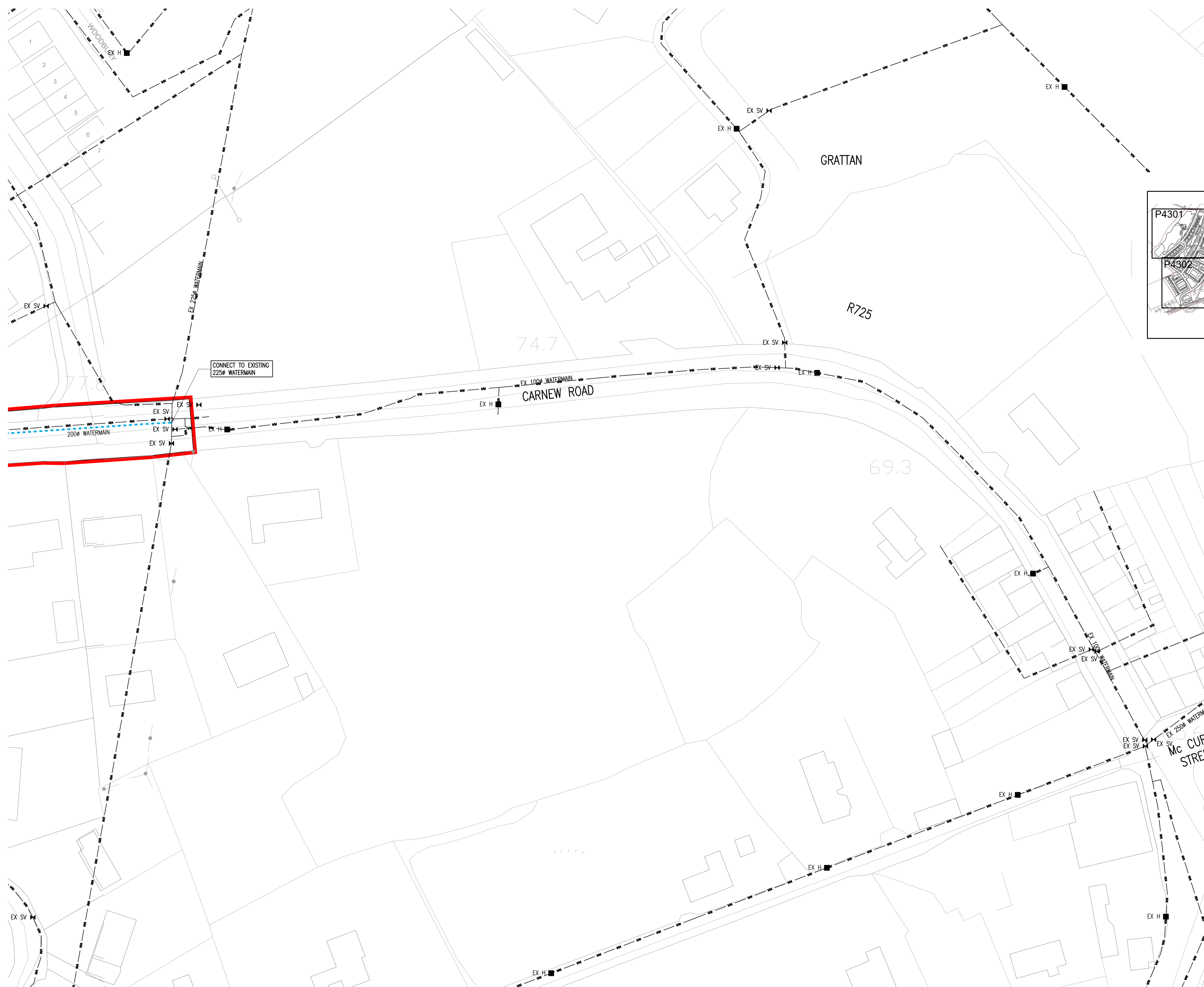
CLIENT **GERARD GANNON PROPERTIES**
ARCHITECT **CONNOLLY ARCHITECTS**

PROJECT
LANDS AT KILNAHUE & GOREY HILL, GOREY

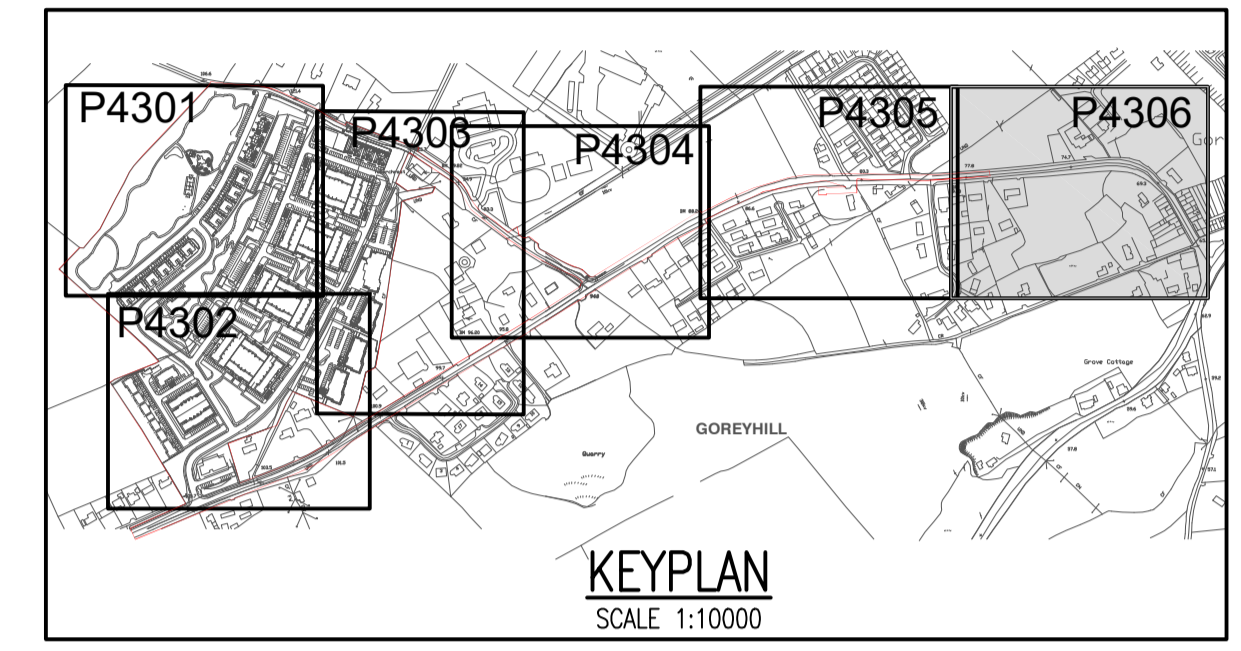
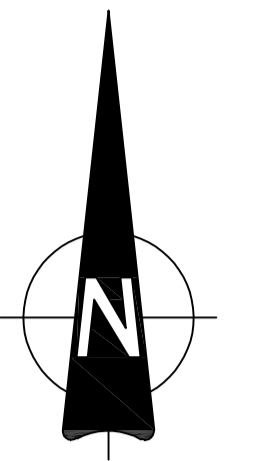
TITLE
PROPOSED WATERMAIN LAYOUT SHEET 5 OF 6

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SCALE 1:500 @ A1	JOB NO. 13-119	DRG. NO. P4305	REVISION



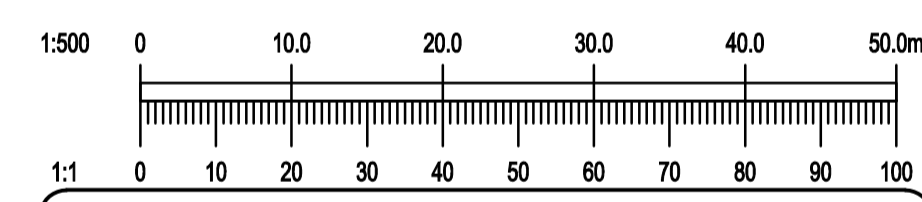


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LEGEND:

--- XXXmm ϕ --- WM	EXISTING WATERMAIN WITH PIPE SIZE
--- 150mm ϕ --- P	PROPOSED 150 ϕ WATERMAIN
--- 200mm ϕ --- P	PROPOSED 200 ϕ WATERMAIN



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CLIENT **GERARD GANNON PROPERTIES**
ARCHITECT **CONNOLLY ARCHITECTS**

PROJECT
LANDS AT KILNAHUE & GOREY HILL, GOREY

TITLE
**PROPOSED WATERMAIN LAYOUT
SHEET 6 OF 6**

DRAWN PJD	DESIGNED DA	APPROVED	DATE AUG 2021
SCALE 1:500 \odot A1	JOB NO. 13-119	DRG. NO. P4306	REVISION

B. GSDS Attenuation Calculations



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Engineering Consultants

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Alfie Byrne Road, Dublin D03 H3F4
t 01 664 8900 f 01 661 3618 e info@waterman-moylan.ie

Calculation By: SDN
Approved by: DA

Project Data

Project Name	Kilnahue, Gorey, Catchments 1-7
Project Number	13-119
Client	Gerard Gannon Properties
Architect	Connolly Architects
Status	Planning
Date	09/11/2021

Description	%	Area
Total Site Area	-	148,625m ²
Paved Area	Total	50% 74,313m ²
	Drained	100% 74,313m ²
Soil Area	Total	50% 74,313m ²
	Drained	0% 0m ²

Soil Type:	Type 4
SPR Index (from FSR):	0.47
SAAR:	1052mm
Rain Data:	Kilnahue, Gorey
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times \text{Area}^{0.89} \times \text{SAAR}^{1.17} \times \text{Soil}^{2.17}$$

Area	= 0.14863km ²	... Total site area in km ²
SAAR	= 1,052mm	... Standard Average Annual Rainfall in mm
SOIL	= 0.47	... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

Q _{BARrural}	= 0.116m ³ /s	
Q _{BARrural}	= 115.569 l/s	Note: Allowable discharge reduced to c.75% (90.00l/s)
Q _{BARrural}	= 7.776 l/s/Ha	

Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	98.23	242.69	300.48
Q _{BAR} (l/s/Ha)	6.61	16.33	20.22
Allowable Discharge	90.00	90.00	90.00

Rainfall Data:

Rain Data From: Kilnahue, Gorey (provided by Met Eireann)
Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	13.1	16.8	19.4	22.2	23.9	26.3	29.9
1	18.2	23.4	27.0	31.0	33.4	36.6	41.6
2	25.4	32.6	37.7	43.1	46.6	51.1	58.0
4	35.4	45.5	52.6	60.1	64.9	71.3	80.9
6	43.1	55.2	63.8	73.1	78.8	86.6	98.3
12	60.0	77.0	89.2	101.9	109.9	120.8	137.2



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Calculation By: SDN

Approved by: DA

Summary

Project Name	Kilnahue, Gorey, Catchments 1-7
Project Number	13-119
Client	Gerard Gannon Properties
Architect	Connolly Architects
Status	Planning
Date	09/11/2021

Summary of GSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	222.94m ³
Treatment Volume	668.81m ³

Criterion 2: River Regime Protection

1-in-1-Year Storm	1,668.33m ³
1-in-30-Year Storm	2,945.77m ³
1-in-100-Year Storm	2,024.27m ³
Reduction of Long-Term Storage	-1,037.09m ³
Volume Required	5,601.28m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage (no interception provided)	1,037.09m ³
Long Term Storage (Interception provided)	814.15m ³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	1,668.33m ³
1-in-30-Year Storm	2,945.77m ³
1-in-100-Year Storm	2,024.27m ³
Total	6,638.37m³

The maximum attenuation volume required is 6,638.37m³



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Calculation By: SDN

Approved by: DA

Criterion 1
River Protection Volume

Project Name: Kilnahue, Gorey, Catchments 1-7

Project Number: 13-119

Client: Gerard Gannon Properties

Architect: Connolly Architects

Status: Planning

Date: 09/11/2021

1.1 Interception

Paved surfaces connected to drainage system	$148625m^2 \times 0.5 \times 0.75 =$ $55,734.38m^2$	<i>148,625m² site area</i> <i>50% of the site is paved</i> <i>75% of the paved area</i>
Volume of Interception Storage	$55734.375m^2 \times 5mm \times 0.8 =$ 222.94m³	<i>Paved area directly drained</i> <i>5mm rainfall depth</i> <i>80% paved runoff factor</i>

1.2 Treatment Volume

Paved surfaces draining to river	$148625m^2 \times 0.5 \times 0.75 =$ $55,734.38m^2$	<i>148,625m² site area</i> <i>50% of the site is paved</i> <i>75% of the paved area</i>
Volume of Treatment Storage	$55734.375m^2 \times 15mm \times 0.8 =$ 668.81m³	<i>Paved area directly drained</i> <i>15mm rainfall depth</i> <i>80% runoff from paved surfaces</i>



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Calculation By: SDN

Approved by: DA

Criterion 2
River Regime Protection

Project Name: Kilnahue, Gorey, Catchments 1-7

Project Number: 13-119

Client: Gerard Gannon Properties

Architect: Connolly Architects

Status: Planning

Date: 09/11/2021

1-Year Return Period

(Climate Change Factor = 20%)

Duration	Rainfall Rate	Runoff <i>= Rainfall Rate x Area x Soil Type</i>				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m ³	l/s	m ³	l/s	m ³
0.5	72.67	540.00	0.00	540.00	972.0	90.00	162.0	450.00	810.0
1	50.67	376.52	0.00	376.52	1,355.5	90.00	324.0	286.52	1,031.5
2	35.33	262.57	0.00	262.57	1,890.5	90.00	648.0	172.57	1,242.5
4	24.58	182.68	0.00	182.68	2,630.7	90.00	1,296.0	92.68	1,334.7
6	19.94	148.21	0.00	148.21	3,201.4	90.00	1,944.0	58.21	1,257.4
12	13.89	103.21	0.00	103.21	4,458.8	90.00	3,888.0	13.21	570.8

30-Year Return Period


(Climate Change Factor = 20%)

Duration	Rainfall Rate	Runoff <i>= Rainfall Rate x Area x Soil Type</i>				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m ³	l/s	m ³	l/s	m ³
0.5	132.67	985.88	0.00	985.88	1,774.6	90.00	27.9	895.88	277.9
1	92.67	688.63	0.00	688.63	2,479.1	90.00	123.3	598.63	820.4
2	64.67	480.55	0.00	480.55	3,460.0	90.00	340.4	390.55	1,477.3
4	45.08	335.03	0.00	335.03	4,824.4	90.00	805.8	245.03	2,193.7
6	36.50	271.24	0.00	271.24	5,858.8	90.00	1,281.2	181.24	2,580.1
12	25.44	189.08	0.00	189.08	8,168.4	90.00	2,675.7	99.08	2,945.8

100-Year Return Period

(Climate Change Factor = 20%)

Duration	Rainfall Rate	Runoff <i>= Rainfall Rate x Area x Soil Type</i>				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m ³	l/s	m ³	l/s	m ³
0.5	166.00	#####	0.00	#####	2,220.5	90.00	-174.9	#####	-2,222.0
1	115.67	859.55	0.00	859.55	3,094.4	90.00	-176.6	769.55	-1,510.1
2	80.50	598.22	0.00	598.22	4,307.2	90.00	-110.0	508.22	-621.3
4	56.17	417.39	0.00	417.39	6,010.4	90.00	119.3	327.39	434.0
6	45.50	338.12	0.00	338.12	7,303.4	90.00	391.4	248.12	1,079.0
12	31.75	235.94	0.00	235.94	#####	90.00	1,248.3	145.94	2,024.3

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		River Flood Protection	
		Project Name	Kilnahue, Gorey, Catchments 1-7
		Project Number	13-119
		Client	Gerard Gannon Properties
		Architect	Connolly Architects
Calculation By:	SDN	Status	Planning
Approved by:	DA	Date	09/11/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol_{XS} ... *Extra runoff volume of development over Greenfield runoff*

RD = 98 mm ... *Rainfall depth of the 100 year, 6 hour event mm*

A = 14.863 Ha ... *Area of site*

PIMP = 50% ... *Impermeable area of total site*

$\alpha 0.8$ = 100% ... *Proportion of paved area drained to drainage network or river with 80% runoff*

β = 60% ... *Proportion of pervious area drained to the network or river*

Soil = 0.47 ... *SPR index*

$$Vol_{XS} = 1,037.09m^3$$



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Calculation By: SDN
Approved by: DA

Project Data

Project Name	Kilnahue, Gorey, Catchment 8
Project Number	13-119
Client	Gerard Gannon Properties
Architect	Connolly Architects
Status	Planning
Date	09/11/2021

Description	%	Area
Southern Catchment	-	5,107m ²
Paved Area	Total	50% 2,554m ²
	Drained	100% 2,554m ²
Soil Area	Total	50% 2,554m ²
	Drained	0% 0m ²

Soil Type:	Type 2
SPR Index (from FSR):	0.30
SAAR:	1052mm
Rain Data:	Kilnahue, Gorey
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times Area^{0.89} \times SAAR^{1.17} \times Soil^{2.17}$$

Area	= 0.00511km ²	... Total site area in km ²
SAAR	= 1,052mm	... Standard Average Annual Rainfall in mm
SOIL	= 0.30	... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

$$Q_{BARrural} = 0.001m^3/s$$

$$Q_{BARrural} = 1.499 \text{ l/s}$$

$$Q_{BARrural} = 3.916 \text{ l/s/Ha}$$

Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	1.70	4.20	5.20
Q _{BAR} (l/s/Ha)	3.33	8.22	10.18
Allowable Discharge	2.00	2.00	2.00

Rainfall Data:

Rain Data From: Kilnahue, Gorey (provided by Met Eireann)
Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	13.1	16.8	19.4	22.2	23.9	26.3	29.9
1	18.2	23.4	27.0	31.0	33.4	36.6	41.6
2	25.4	32.6	37.7	43.1	46.6	51.1	58.0
4	35.4	45.5	52.6	60.1	64.9	71.3	80.9
6	43.1	55.2	63.8	73.1	78.8	86.6	98.3
12	60.0	77.0	89.2	101.9	109.9	120.8	137.2



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Summary

Project Name	Kilnahue, Gorey, Catchment 8
Project Number	13-119
Client	Gerard Gannon Properties
Architect	Connolly Architects
Status	Planning
Date	09/11/2021

Summary of GSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	7.66m³
Treatment Volume	22.98m³

Criterion 2: River Regime Protection

1-in-1-Year Storm	83.51m ³
1-in-30-Year Storm	127.47m ³
1-in-100-Year Storm	69.56m ³
Reduction of Long-Term Storage	-95.36m ³
Volume Required	185.18m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage (no interception provided)	95.36m³
Long Term Storage (Interception provided)	87.70m³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	83.51m ³
1-in-30-Year Storm	127.47m ³
1-in-100-Year Storm	69.56m ³
Total	280.54m³

The maximum attenuation volume required is 280.54m³



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Criterion 1
River Protection Volume

Project Name: Kilnahue, Gorey, Catchment 8

Project Number: 13-119

Client: Gerard Gannon Properties

Architect: Connolly Architects

Status: Planning

Date: 09/11/2021

1.1 Interception

Paved surfaces connected to drainage system	$5107m^2 \times 0.5 \times 0.75 =$ 1,915.13m ²	5,107m ² site area 50% of the site is paved 75% of the paved area
Volume of Interception Storage	$1915.125m^2 \times 5mm \times 0.8 =$ 7.66m³	Paved area directly drained 5mm rainfall depth 80% paved runoff factor

1.2 Treatment Volume

Paved surfaces draining to river	$5107m^2 \times 0.5 \times 0.75 =$ 1,915.13m ²	5,107m ² site area 50% of the site is paved 75% of the paved area
Volume of Treatment Storage	$1915.125m^2 \times 15mm \times 0.8 =$ 22.98m³	Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces



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Calculation By: SDN

Approved by: DA

Criterion 2
River Regime Protection

Project Name: Kilnahue, Gorey, Catchment 8

Project Number: 13-119

Client: Gerard Gannon Properties

Architect: Connolly Architects

Status: Planning

Date: 09/11/2021

1-Year Return Period

(Climate Change Factor = 20%)

Duration	Rainfall Rate	Runoff <i>= Rainfall Rate x Area x Soil Type</i>				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m ³	l/s	m ³	l/s	m ³
0.5	72.67	18.56	0.00	18.56	33.4	2.00	3.6	16.56	29.8
1	50.67	12.94	0.00	12.94	46.6	2.00	7.2	10.94	39.4
2	35.33	9.02	0.00	9.02	65.0	2.00	14.4	7.02	50.6
4	24.58	6.28	0.00	6.28	90.4	2.00	28.8	4.28	61.6
6	19.94	5.09	0.00	5.09	110.0	2.00	43.2	3.09	66.8
12	13.89	3.55	0.00	3.55	153.2	2.00	86.4	1.55	66.8

30-Year Return Period


(Climate Change Factor = 20%)

Duration	Rainfall Rate	Runoff <i>= Rainfall Rate x Area x Soil Type</i>				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m ³	l/s	m ³	l/s	m ³
0.5	132.67	33.88	0.00	33.88	61.0	2.00	-0.6	31.88	-9.4
1	92.67	23.66	0.00	23.66	85.2	2.00	1.0	21.66	11.2
2	64.67	16.51	0.00	16.51	118.9	2.00	5.2	14.51	37.7
4	45.08	11.51	0.00	11.51	165.8	2.00	14.8	9.51	70.2
6	36.50	9.32	0.00	9.32	201.3	2.00	24.9	7.32	91.3
12	25.44	6.50	0.00	6.50	280.7	2.00	56.7	4.50	127.5

100-Year Return Period

(Climate Change Factor = 20%)

Duration	Rainfall Rate	Runoff <i>= Rainfall Rate x Area x Soil Type</i>				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m ³	l/s	m ³	l/s	m ³
0.5	166.00	42.39	0.00	42.39	76.3	2.00	-6.0	40.39	-121.6
1	115.67	29.54	0.00	29.54	106.3	2.00	-6.9	27.54	-95.2
2	80.50	20.56	0.00	20.56	148.0	2.00	-6.5	18.56	-60.7
4	56.17	14.34	0.00	14.34	206.5	2.00	-2.7	12.34	-16.6
6	45.50	11.62	0.00	11.62	251.0	2.00	2.8	9.62	13.5
12	31.75	8.11	0.00	8.11	350.2	2.00	22.8	6.11	69.6

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		River Flood Protection	
		Project Name	Kilnahue, Gorey, Catchment 8
		Project Number	13-119
		Client	Gerard Gannon Properties
		Architect	Connolly Architects
Calculation By:	SDN	Status	Planning
Approved by:	DA	Date	09/11/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol_{XS} ... Extra runoff volume of development over Greenfield runoff

RD = 98 mm ... Rainfall depth of the 100 year, 6 hour event mm

A = 0.511 Ha ... Area of site

PIMP = 50% ... Impermeable area of total site

$\alpha 0.8$ = 100% ... Proportion of paved area drained to drainage network or river with 80% runoff

β = 60% ... Proportion of pervious area drained to the network or river

Soil = 0.30 ... SPR index

$$Vol_{XS} = 95.36m^3$$

C. External Quality Audit

Title: **QUALITY AUDIT**

INCLUDING

Road Safety Audit, Access Audit, Cycle Audit and Walking Audit.

For;

Proposed Strategic Housing Development, Kilnahue, Gorey, Co. Wexford.

Client: **Water Moylan/Gannon Properties**

Date: **October 2021**

Report reference: **1178R01**

VERSION: **FINAL (15-11-2021)**

Prepared By:

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1.0 Introduction

This report was prepared in response to a request from Mr. Stephen Dent Neville, Waterman Moylan Consulting Engineers, for a Quality Audit of the proposed strategic housing development (SHD) at Kilnahue, Gorey, Co. Wexford.

The Quality Audit has been carried out in accordance with the guidance in the Design Manual for Urban Roads and Streets (DMURS), produced by Department of Transport Tourism and Sport in March 2013 and as updated in June 2019.

This portion of the Quality Audit is a design stage audit and includes a Stage 1 Road Safety Audit (in accordance with TII Publication GE-DTY-01024, dated December 2017), an access audit, a walking audit and a cycling audit. (i.e. aspects of a quality Audit carried out independent of the Design Team and generally included as appendices to the overall Audit)

The Road Safety and Quality Audit Team comprised of;

Team Leader: **Norman Bruton**, BE CEng FIEI, Cert Comp RSA.

TII Road safety Auditor approval number: NB 168446

Team Member: **Owen O'Reilly**, B.SC. Eng Dip Struct. Eng NCEA Civil Dip Civil. Eng CEng MIEI

TII Auditor Approval no. OO 1291756

This portion of the Quality Audit involved the examination of drawings and other material and a site visit by the Audit Team, on the 7th of October 2021. The weather at the time of the site visit was mainly dry with some rain and the road surface was wet.

The problems raised in this Quality Audit may belong to more than one of the categories of Audit named above. A table has been provided at the start of Section 3 of this report detailing which category of audit each problem is associated with.

Recommendations have been provided to help improve the quality of the design with regard to the areas described above. A feedback form has also been provided for the designer to complete indicating whether or not he/she will accept those recommendations or provide alternative recommendations for implementation.

The information supplied to the Audit Team is listed in **Appendix A**.

A feedback form for the Designer to complete is contained in **Appendix B**.

A plan drawing showing the problem locations is contained in **Appendix C**.

2.0 Background

It is proposed to construct a SHD at Kilnahue and Kilnahue Lane, Gorey, Co. Wexford. The development consists of 421 no. residential units comprising of 133 no. houses, 60 no. duplexes and 228 no. apartments and a creche.

The site is located west of Gorey town. It is bounded to the northeast by Kilnahue Lane, to the northwest and southwest by greenfield lands and to the southeast by the R725 Carnew Road, a filling station and some existing residential dwellings.

It is proposed to provide priority junction vehicular accesses onto the R725 (1 no. access with right turning lane) and Kilnahue Lane (2 no. accesses) from the development. A footpath will be provided along Carnew Road from the combined access for 6 no. houses west of the proposed development access to join with the existing footpath closer to the town centre, at the filling station.

Pedestrian and cycle facilities will be provided on Kilnahue Lane connecting with the existing facilities at the school and onwards to Carnew Road.

Creagh College and Gaelscoil Moshíológ are located off Kilnahue Lane closer to the Carnew Road junction than the proposed development accesses.

Cycle facilities within the development will be on-road and footpath will be provided throughout the internal road network.

Gorey Town centre is served by public buses.

Gorey has a train station on the Dublin to Wexford rail line.

The speed limit at the proposed Carnew Road junction location is 60km/hr, the speed limit reduces to 50km/hr before the Kilnahue Lane Junction. The speed limit on Kilnahue Lane increases to 80km/hr after the schools.

The site location map is shown below.



Site Location Map (image courtesy of openstreetmap.org)

The Road Safety Authority’s website shows that in the 12-year period 2005 to 2016 that there were two minor injury collisions on the R725 Carnew Road in the vicinity of the proposed development site.

Ireland road collisions [Restart](#)

Help

Collisions

Severity

Fatal Serious Minor All

Year

2016 2015 2014 2013 2012 2011
 2010 2009 2008 2007 2006 2005
 All

Type

All Pedestrian Bicycle Motorcycle
 Car Goods vehicle Bus Other

Collision information

Severity	Minor
Year	2007
Vehicle	Goods vehicle
Circumstances	Unknown
Day of week	Friday
Time	0300-0700
Speed limit	60 KPH
No. casualties - minor	1
No. casualties - total	1

3.0 Issues Identified in the Stage 1 Quality Audit

Summary Table of Problem Categories

Problem Reference	Access Audit	Walking Audit	Cycling Audit	Road Safety Audit	Quality Audit
3.1				✓	✓
3.2		✓	✓	✓	✓
3.3		✓	✓	✓	✓
3.4		✓	✓	✓	✓
3.5		✓	✓	✓	✓
3.6		✓		✓	✓
3.7	✓				✓
3.8	✓				✓
3.9				✓	✓
3.10	✓	✓	✓		✓
3.11		✓	✓		✓

3.1 Problem

LOCATION

Drawing 13-119 P4103 Rev -, Kilnahue Lane.

ISSUE

There is very limited forward visibility/stopping sight distance for drivers travelling westbound on Kilnahue Lane after the school access due to the boundary hedge of the private residential property. This could lead to drivers being unable to stop if a hazard (e.g. pedestrian or stopped vehicle) is located on the road ahead resulting in collisions.





RECOMMENDATION

It is recommended that the hedge be taken back. If this is not feasible due to 3rd party ownership then the speeds on Kilnahue Lane should be reduced by the introduction of additional traffic calming such that the stopping sight distance available matches the design speed. Some adjustment to the ghost island road markings for the right turning lane may also improve visibility.

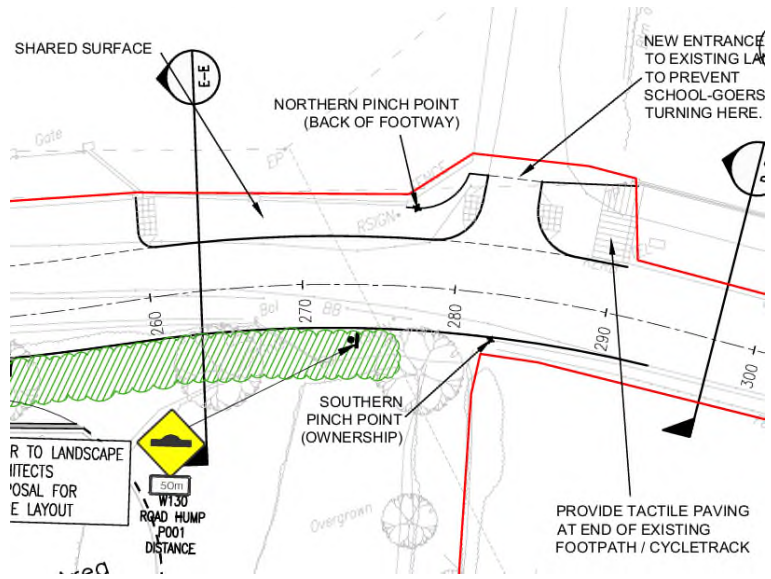
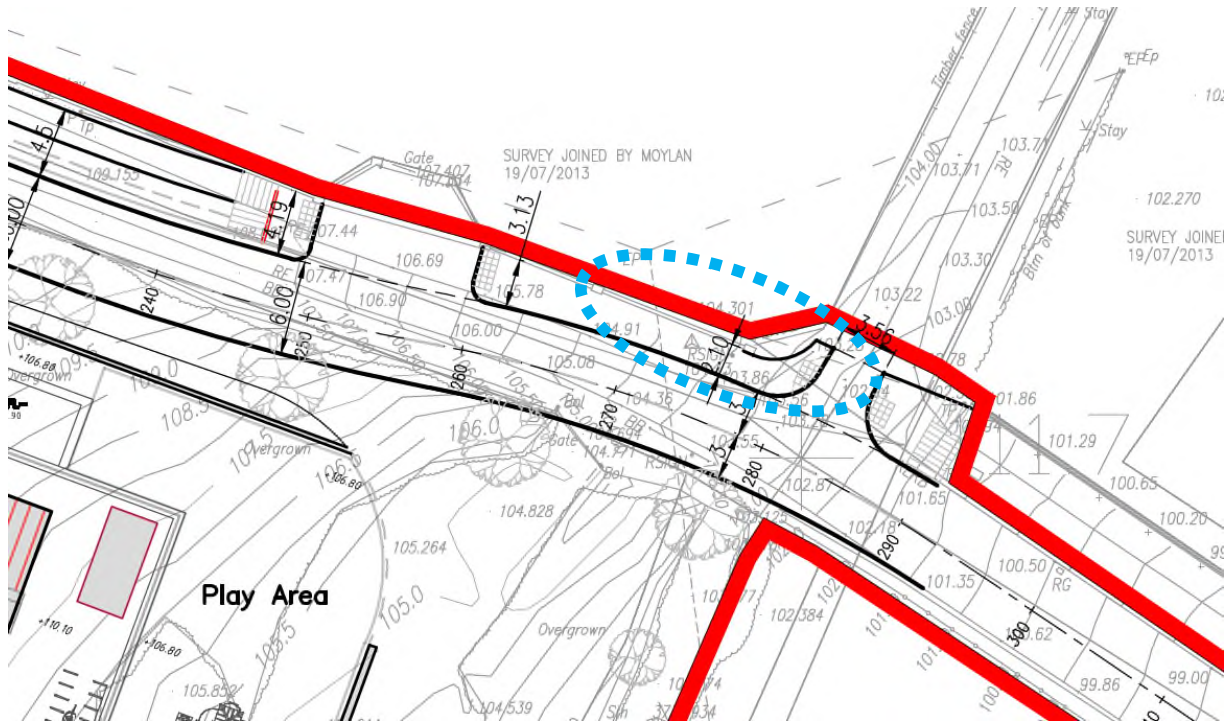
3.2 Problem

LOCATION

Drawing 13-119 P4103 & P4130 Rev -, Kilnahue Lane.

ISSUE

There is a short section along Kilnahue Lane where the segregated cycle and pedestrian facilities are merged into a shared facility and the cross sectional width (2.1m) is less than the segregated widths. There is a risk that at school times this section of the path will not be wide enough to cater for the high volume of cyclists and pedestrians and may lead to cyclists colliding with pedestrians or entering the carriageway by dismounting the kerbs which may not be expected by drivers and could lead to collisions.



RECOMMENDATION

It is recommended that a section of on-road cycle track be provided with suitable transitions from off road-to on road and vice versa at the pinch-point.

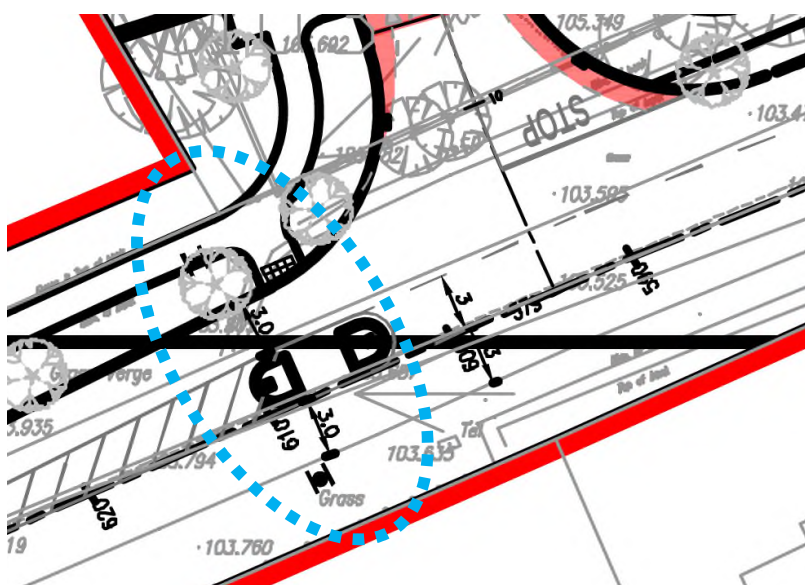
3.3 Problem

LOCATION

Drawing 13-119 P4100 Rev -, Carnew Road, R725.

ISSUE

It is proposed to provide an uncontrolled pedestrian crossing with a traffic island on the R725 just west of the proposed access. It is assumed that this is to allow dismounted cyclists travelling from the town centre direction to cross the R725 and to provide some traffic calming. There is however no refuge area on the southern verge of the R725 for dismounted cyclists or pedestrians to wait. The cross section of the R725 is such that there may be no hard strip. In the town bound direction there will be a 3.0m lane between the traffic island and the kerb of the footpath. This could lead to cyclists being 'squeezed' by passing vehicles.



RECOMMENDATION

It is recommended a gateway type treatment be provided with provision for cyclists in both directions. The gateway should include lighting and signage which denotes the transition into the urban (60km/hr) area for drivers and acts as a traffic calming feature.

3.4 Problem

LOCATION

Drawing 13-119 P4102, R725 Access.

ISSUE

The corner radii at the proposed access on the R725 are 10m. This could lead to high turning speeds, greater blind spots to cyclists for left turning drivers and longer areas for pedestrians to cross if they

take the desire line rather than the route to the raised table and uncontrolled crossing which are set back.



RECOMMENDATION

It is recommended that the corner radii be reduced and that the crossing area be moved closer to the desire line.

3.5 Problem

LOCATION

Internal junctions within the proposed development.

ISSUE

The internal junctions within the development are shown to be yield control junctions. Yield control leads to higher turning speeds which in turn leads to higher injury severity if a vulnerable road user is struck.

RECOMMENDATION

It is recommended that stop control be used instead of yield control.

3.6 Problem

LOCATION

Drawing 13-119 P4102, Road 1

ISSUE

The uncontrolled crossing on Road 1, chainage 142 approx is located at the base of the raised table. Pedestrians may be more vulnerable if they cross at this location as it is likely that drivers will feel that they should stop at the crossing point in advance of the ramp.



RECOMMENDATION

It is recommended that the raised table be extended to include the pedestrian crossing.

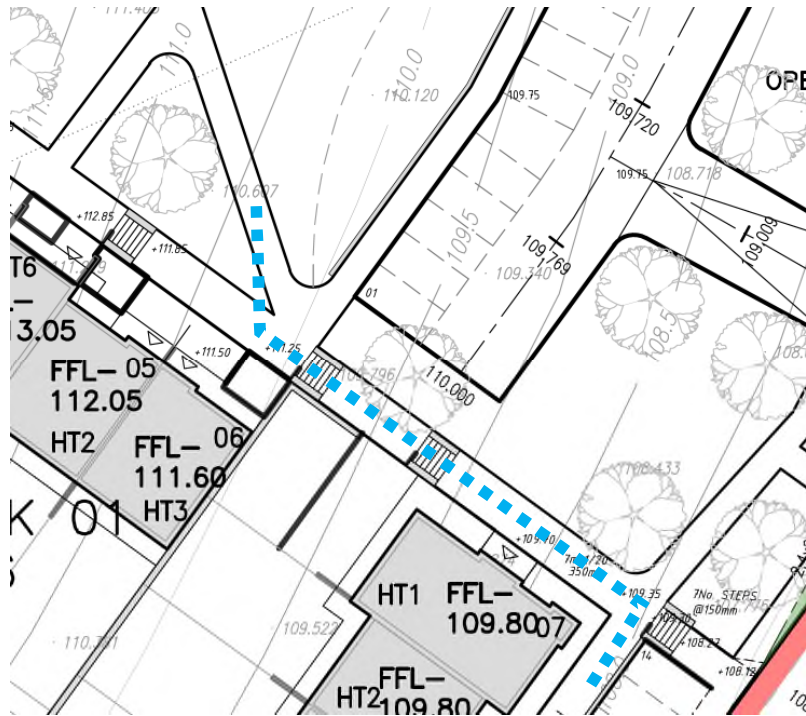
3.7 Problem

LOCATION

Drawing 13-119 P4102, Access to opens paces.

ISSUE

The topography of the site leads to many steps throughout the footpath network. Steps are not accessible by all. There is a risk that the mobility impaired may not be able to get to the open areas adjacent to their houses.



Example only

RECOMMENDATION

Ensure that alternative access to the adjacent open spaces is available with gradients that are in accordance with the Technical Guidance Document of Part M of the Building Regulations without steps and without excessive long routes.

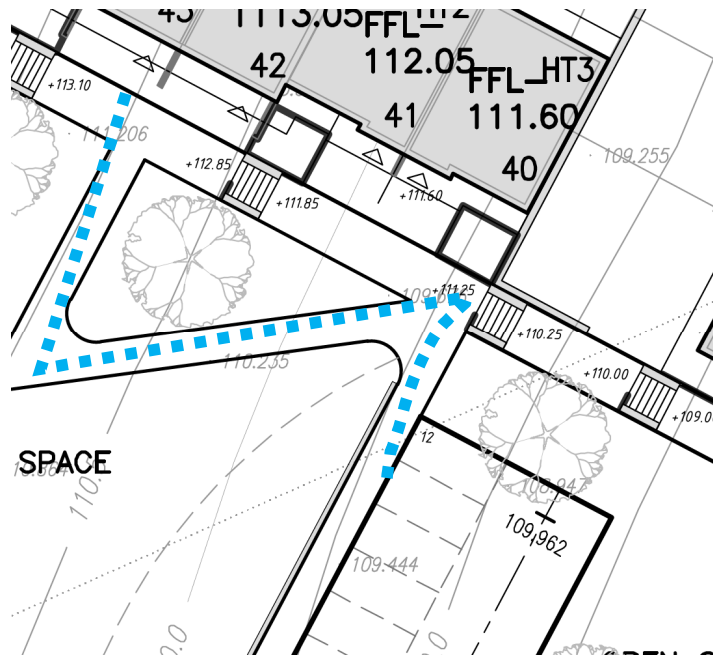
3.8 Problem

LOCATION

Drawing 13-119 P4102, Access to houses from car parking spaces.

ISSUE

The topography of the site leads to many steps throughout the footpath network. Steps are not accessible by all. There is a risk that the mobility impaired may not be able to get to their houses from their car parking areas if steps are encountered along the route.



Example only

RECOMMENDATION

Ensure that suitable pedestrian provision with gradients in accordance with the Technical Guidance Document of Part M of the Building Regulations without steps be provided from dedicated car parking spaces to the associated residential units.

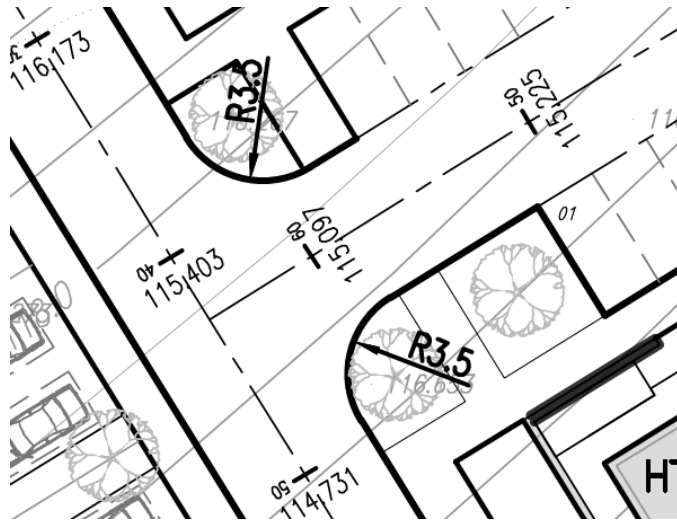
3.9 Problem

LOCATION

Throughout the development, trees

ISSUE

It is proposed to provide trees at the corners of internal junctions,. This could lead to a lack of visibility for drivers exiting the junctions which in turn could lead to side-impact collisions.



RECOMMENDATION

Ensure that tree types and locations are chosen such that the girth, clear stem and canopies will not interfere with visibility both when planted and when mature.

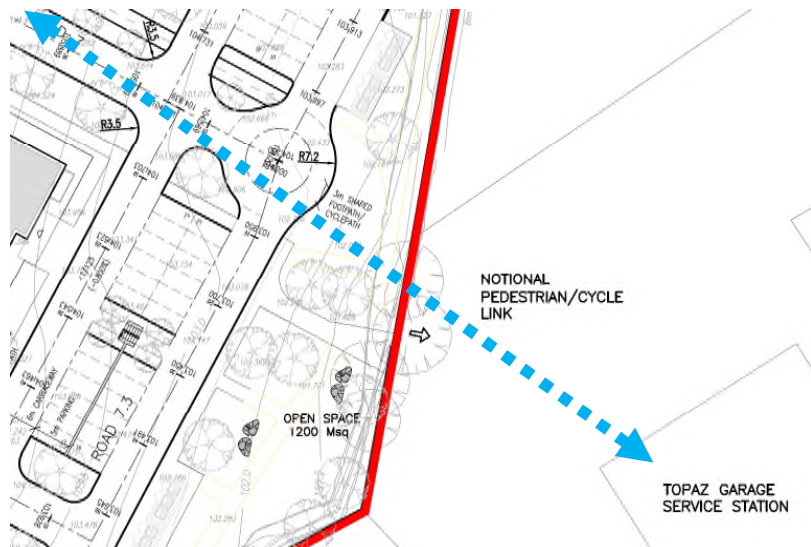
3.10 Problem

LOCATION

Drawing 13-119 P4103, Notional Link to Circle K Service Station.

ISSUE

There is a notional pedestrian/cycle link to the Circle K Garage on the R725 which will be a highly used desire line given that the proposed development is at the out limits of the urban area. The link from Road 1 to the Service station is discontinuous and the access point at the service station may not be suitable for cyclists when deliveries are being made.



RECOMMENDATION

It is recommended that the link between Road 1 and the service station be clearly defined and continuous and that details of the proposed route for pedestrians/cyclists to the shop door/cycle parking be provided to ensure that this is a safe route for users.

3.11 Problem

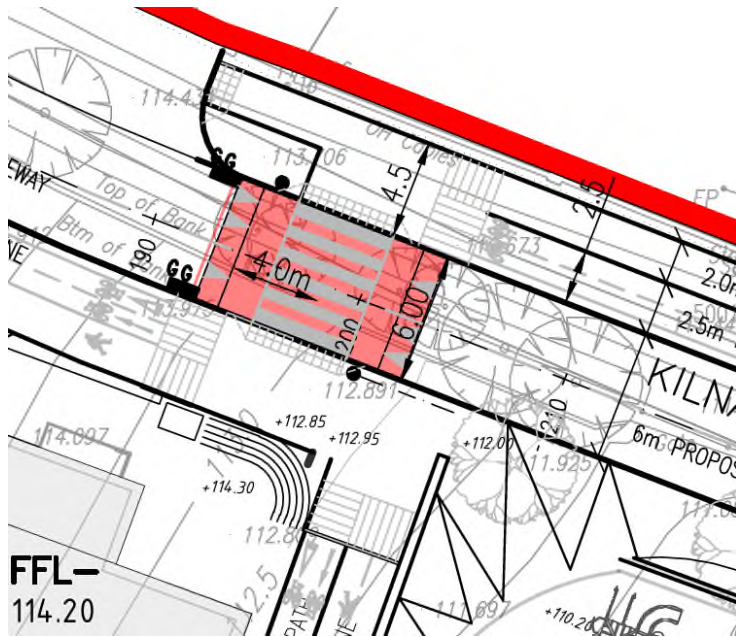
LOCATION

Drawing 13-119 P4103, Zebra crossing on Kilnahue Lane.

ISSUE

It is proposed to provide a zebra crossing on Kilnahue Lane. This crossing is controlled with pedestrian priority. Blind or partially sighted pedestrians may not realise that they have priority if suitable tactile paving is not provided.

There is also a risk of confusion with regard to the sharing of the zebra crossing with cyclists.




RECOMMENDATION

Provide L shaped red coloured tactile paving at the crossing.

4.0 Quality Audit Statement

This portion of the Quality Audit has been carried out in accordance with the guidance given in DMURS and takes into consideration the principles approaches and standards of that Manual.

The quality audit has been carried out by the persons named below who have not been involved in any design work on this scheme as a member of the Design Team.

Norman Bruton Signed: 
(Quality Audit Team Leader) Dated: 15/11/2021

Owen O'Reilly Signed: 
(Quality Audit Team Member) Dated: 15/11/2021

Appendix A

List of Material Supplied for this Quality Audit;

- Drawing13-119-P4102 Proposed Road Layouts & Levels Sheet 2 of 3
- Drawing13-119-P4103 Proposed Road Layouts & Levels Sheet 3 of 3
- Drawing13-119-P4104 Typical Road Construction Details
- Drawing13-119-P4105 Road Longitudinal Sections Sheet 1 of 2
- Drawing13-119-P4106 Road Longitudinal Sections Sheet 2 of 2
- Drawing13-119-P4107 Proposed Traffic Calming
- Drawing13-119-P4110 Carnew Road Improvements
- Drawing13-119-P4130 Kilnahue Lane Upgrade
- Drawing13-119-P4142 Sitelines at Junction of Proposed Carnew Road
- Drawing13-119-P4001 Site Location Plan
- Drawing13-119-P4030 Existing & Proposed Footway links
- Drawing13-119-P4100 Proposed Road Layout General Arrangement
- Drawing13-119-P4101 Proposed Road Layouts & Levels Sheet 1 of 3

Appendix B

Feedback Form

QUALITY AUDIT FORM – FEEDBACK ON QUALITY AUDIT REPORT

Scheme: SHD Carnew Road, Gorey
 Quality Audit- Stage 1

Date Audit (site visit) Completed 7-10-2021

Paragraph No. in Quality Audit Report	Problem accepted (yes/no)	Recommended measure accepted (yes/no)	Alternative measures (describe)	Alternative measures accepted by Auditors (Yes/No)
3.1	yes	yes	Reduce speed on Kilnahue Lane to 30kph from Junction with Carnew Rd to Northern extent of proposed works, keep spacing of ramps where visibility is poor, to a minimum, so SSD = design speed.	
3.2	yes	no	Reduce road width locally from 6m to 5.5m increasing shared footpath width to 2.6m	Yes
3.3	yes	yes	Keep 1 island, remove pedestrian link from north to south of road. Provide cycleways locally through the entry gate. Provide Gateway signage, lighting and markings to make clear.	
3.4	yes	yes	Entry radii reduced to 6m.	
3.5	yes	yes		
3.6	Yes	Yes		
3.7	Yes	Yes		
3.8	Yes	Yes		
3.9	Yes	Yes		
3.10	No	No	The link to the Topaz garage will not form part of this application.	Yes
3.11	Yes	Yes		

Signed *Mark Duignan*
 Design Team Leader

Date15/11/2021

Signed *Norman Bruton*

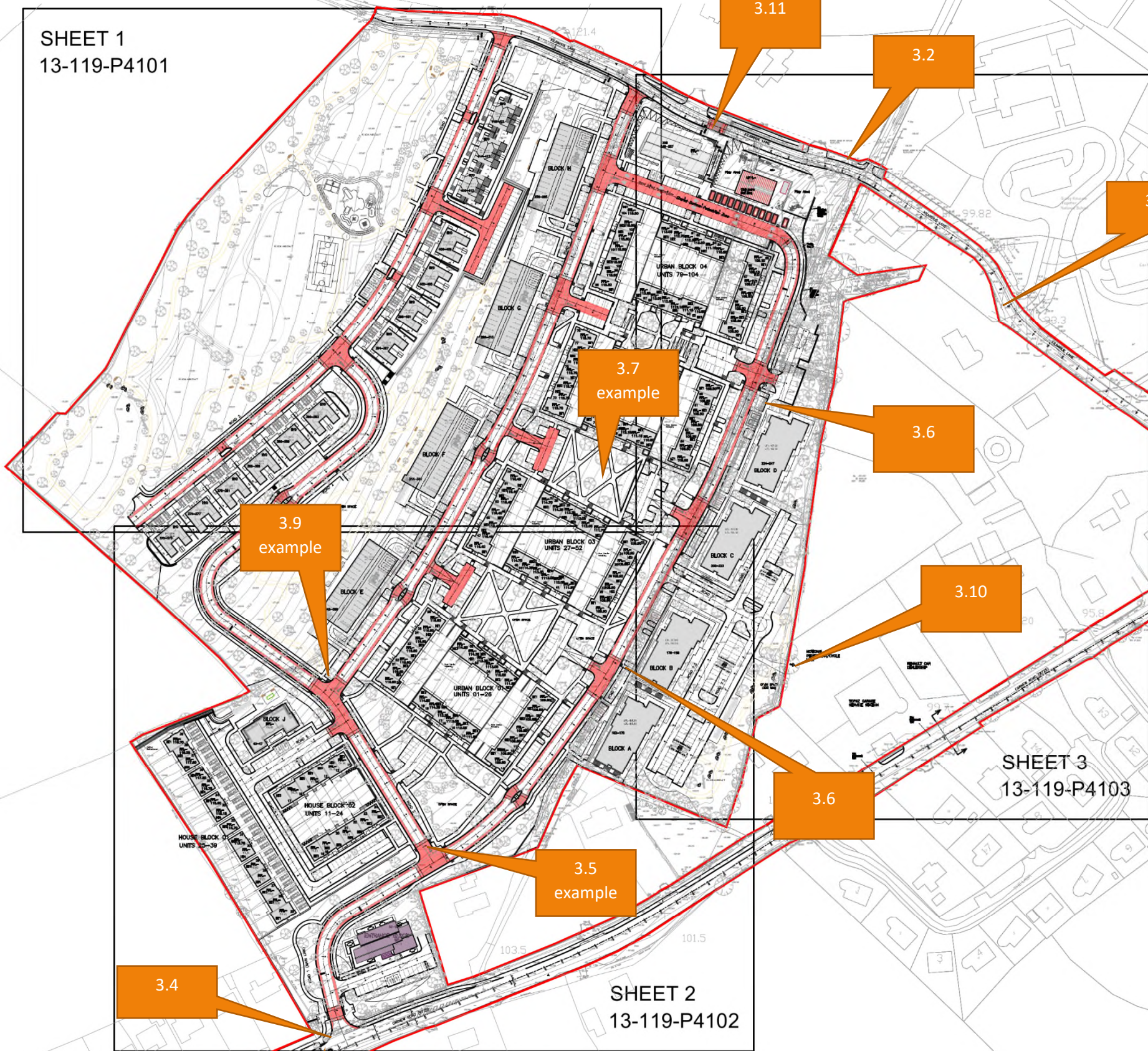
Date:15/11/2021 Audit Team Leader

Appendix C

Problem Location Plan.



SHEET 1
13-119-P4101

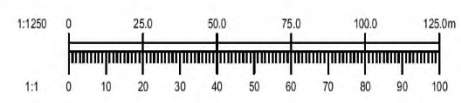


SHEET 2
13-119-P4102

SHEET 3
13-119-P4103

- NOTES:
- DO NOT SCALE. USE FIGURED DIMENSIONS ONLY.
 - THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL OTHER RELEVANT ARCHITECTURAL AND ENGINEERING DRAWINGS.

1 October 2021
 -- DRAFT --
 Nick Smith



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REV.	DATE	AMENDMENT	DRN	APPD

STATUS **FOR PLANNING ONLY
NOT FOR CONSTRUCTION**

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 Email: info@waterman-moylan.ie www.waterman-moylan.ie

CLIENT **GERARD CANNON PROPERTIES**
 ARCHITECT **CONNOLLY ARCHITECTS**
 PROJECT **LANDS AT KILNAHUE & GOREY HILL, GOREY**

TITLE **PROPOSED ROAD LAYOUT GENERAL ARRANGEMENT**

DRAWN	DESIGNED	APPROVED	DATE
PJD	DA		AUG 2021
SCALE	JOB NO.	DRG. NO.	REVISION
1:1250 @A1	13-119	P4100	

UK and Ireland Office Locations

